American River Flood Control District Statement of Operations July 1, 2020 to February 28, 2021 (Eight Months Ending of Fiscal 2021) For Internal Use Only

·	Year to Date July 1, 2020 to February 28, 2021	Budget	Percent of Budget
Revenues	10 1 GM (ually 20, 2021	Buuget	Duuget
Benefit assessment Consolidated capital assessment	\$ 751,485	\$ 1,429,793 980,000	52.56% 0.00%
Interest	73,092	77,267	94.60%
O & M agreements Miscellaneous	26,732	231,801	0.00% Not budgeted
Total Revenues	20,102	-	Not budgeted
	851,309	2,718,861	31.31%
M & O Expenses			
	570.047	202.000	00.040/
Salaries and wages Payroll tax expense	576,917 41,268	833,238 66,659	69.24% 61.91%
Pension expense	127,393	189,428	67.25%
Compensation insurance Medical/dental/vision	13,562 175,747	41,662 216,125	32.55% 81.32%
Fuel/oil reimbursement	16,133	35,000	46.09%
Equipment rental	7,320	20,000	36.60%
Equipment repairs/parts Equipment purchases (< \$5,000)	43,900 1,037	50,000 15,000	87.80% 6.91%
Shop supplies	28,240	20,000	141.20%
Levee maint. (supp. & material)	16,487	20,000	82.44%
Levee maint. chemicals Levee maint. services	20,839 97,224	27,500 80,000	75.78% 121.53%
Rodent abatement (supplies & materials)	6,380	10,000	63.80%
Employee uniforms Staff training	6,227 3,402	7,500 7,500	83.03% 45.36%
Regulation Compliance (OSHA)	10,506	6,000	175.10%
Miscellaneous	1,125	2,000	56.25%
Small tools & equipment Emergency preparedness program	6,118 5,932	7,500 35,000	81.57% 16.95%
Engineering services	11,510	20,000	57.55%
Environmental services/studies	-	5,000	0.00%
Encroachment remediation Urban camp cleanup	11,383	15,000 50,000	0.00% 22.77%
Total M & O Expenses	1,228,650	1,780,112	69.02%
Administration Expenses			
Board of trustees compensation	4,051	7,600	53.30%
Trustee expenses	-	2,400 5,000	0.00% 0.00%
Trustee training Accounting services	12,175	15,000	81.17%
Legal services (general)	17,194	50,000	34.39%
Utilities Telephone	26,538 11,477	40,000 25,000	66.35% 45.91%
Retiree benefits	105,543	143,000	73.81%
Office/shop/yard lease	4,800	7,200	66.67%
Office equipment/furniture Auto allowance	479 4,722	7,500 6,600	6.39% 71.55%
Parking reimbursement	-	500	0.00%
General office expense	8,651 12,380	15,000 10,000	57.67% 123.80%
Technology and software Dues and associations	23,724	25,000	94.90%
Property and liability insurance	28,476	42,000	67.80%
Public relations/information Miscellaneous	2,669	30,000 5,000	0.00% 53.38%
Election expense	145,993	99,723	146.40%
Employee morale/wellness	- 4440	2,000	0.00%
Investment fees Community services	4,412	20,000 1,500	22.06% 0.00%
Bookkeeping services	6,825	14,000	48.75%
Property taxes Building maintenance	1,710 11,077	3,000 10,000	57.00%
County Dtech fees for DLMS	31,669	55,000	110.77% 57.58%
County assessment fees	19,178	-	Not budgeted
Interest expense	402		Not budgeted
Total Administration Expenses  Special Projects Expenses	484,145	642,023	75.41%
Engineering studies/survey studies Levee standards compliance Small capital projects	3,963	170,000 25,000 50,000	2.33% 0.00% 0.00%
Total Special Project Expenses	3,963		1.62%
Capital Outlay			
Equipment purchases (over \$5,000)	212,405	100,000	212.41%
Total Capital Outlay	212,405	100,000	
Capital Outlay: District Headquarters Build-Out			
Building improvements/maintenance La Riviera improvements/maintenance	358,711 54	700,000 2,000	51.24% 2.70%
		702,000	2 0,0
Notes Assessed the second section of the d			

Note: Amounts above are not audited

The above information is current through the last day of the previous month's bank activity.

Data has been verified by the bookkeeper and physical copies of checks have not been reviewed or received and some checks may not have cleared the bank account.

#### AMERICAN RIVER FLOOD CONTROL DISTRICT Cash Flow Report July 2020 through June 2021

#### Cash Flow Report

Jaon Flow Report													
Maintenance and Operations Expens	20-Jul	20-Aug	20-Sep	20-Oct	20-Nov	20-Dec	21-Jan	21-Feb	21-Mar	21-Apr	21-May	21-Jun	TOTAL
500 · Salary/Wages	84,955.85	72,305.42	71,963.98	74,588.44	66,019.98	104,073.57	35,778.71	69,715.98	67,522.54	0.00	0.00	0.00	646,924.47
501 · Payroll Taxes	6,551.57	5,583.83	5,557.69	5,247.26	4,156.05	6,597.80	3,378.64	6,036.87	5,209.15	0.00	0.00	0.00	48,318.86
502 · Pension	17,202.17	15,822.01	21,318.10	16,226.03	9,575.75	19,891.06	10,916.85	15,094.39	9,369.39	0.00	0.00	0.00	135,415.75
503 · Compensation Insurance	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
504 · Medical/Dental/Vision	24,342.88	19,791.24	19,837.24	19,791.24	18,145.44	20,694.56	20,260.56	20,214.56	0.00	0.00	0.00	0.00	163,077.72
508 · Fuel/Oil	2,345.10	4,356.39	2,664.57	2,714.69	0.00	3,215.72	1,797.58	3,135.76	0.00	0.00	0.00	0.00	20,229.81
509 · Equipment Rental	0.00	5,960.25	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	5,960.25
510 · Equipment Purchase(< \$5000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
511 · Equipment Repair/Parts	15,604.93	6,143.91	9,008.02	5,524.43	1,973.22	6,102.41	9,813.15	3,973.02	0.00	0.00	0.00	0.00	58,143.09
512 · Shop Supplies	4,256.28	8,016.10	4,875.31	4,929.78	1,128.15	5,753.11	2,078.35	2,290.45	0.00	0.00	0.00	0.00	33,327.53
514 · Levee Maint(Supplies&Materi	100.38	5,826.24	187.69	2,822.64	1,140.03	3,901.62	2,183.43	425.52	0.00	0.00	0.00	0.00	16,587.55
515 · Levee Maintenance Services	2,200.00	25,393.37	26,643.08	9,097.84	11,407.70	1,955.02	9,552.09	14,619.90	0.00	0.00	0.00	0.00	100,869.00
516 · Employee Uniforms	0.00	0.00	5,768.62	280.37	0.00	503.36	0.00	325.00	0.00	0.00	0.00	0.00	6,877.35
518 · Staff Training	1,529.00	0.00	525.00	1,614.36	0.00	0.00	532.72	0.00	(60.00)	0.00	0.00	0.00	4,141.08
519 · Miscellaneous O&M	0.00	0.00	0.00	0.00	1,125.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1,125.00
521 · Small Tools & Equip	0.00	0.00	273.52	0.00	0.00	4,273.10	688.99	0.00	0.00	0.00	0.00	0.00	5,235.61
523 · Levee Maint. (Chemicals)	0.00	13,414.68	1,344.74	0.00	0.00	0.00	5,009.22	958.01	0.00	0.00	0.00	0.00	20,726.65
525 · Emergency Preparedness Pro	0.00	0.00	0.00	0.00	0.00	1,731.94	0.00	0.00	0.00	0.00	0.00	0.00	1,731.94
530 · Encroachment Remediation	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
532 · Rodent Abatement	0.00	225.24	766.80	4,130.07	1,123.95	0.00	0.00	246.43	0.00	0.00	0.00	0.00	6,492.49
533 · Urban Camp Cleanup	1,380.45	2,421.74	3,622.43	409.50	825.01	1,308.34	513.50	2,172.46	0.00	0.00	0.00	0.00	12,653.43
605 · Engineering Services	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
615 · Survey Services	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
616 · Envionmental Services/Studie	0.00	0.00	0.00	0.00	0.00	0.00	145,993.01	0.00	0.00	0.00	0.00	0.00	145,993.01
Total M&O Expense	160,468.61	185,260.42	174,356.79	147,376.65	116,620.28	180,001.61	248,496.80	139,208.35	82,041.08	0.00	0.00	0.00	1,433,830.59

Administrative Expenses	20-Jul	20-Aug	20-Sep	20-Oct	20-Nov	20-Dec	21-Jan	21-Feb	21-Mar	21-Apr	21-May	21-Jun	TOTAL
505 · Telephone	1,521.70	1,626.92	1,545.83	1,783.83	1,827.13	2,006.12	1,814.41	1,076.12	0.00	0.00	0.00	0.00	13,202.06
506 · Utility Charges	3,362.49	4,354.93	3,882.24	3,785.69	3,680.19	2,926.48	3,681.49	4,095.17	0.00	0.00	0.00	0.00	29,768.68
507 · Office/Shop Lease	600.00	600.00	600.00	0.00	1,200.00	600.00	600.00	600.00	0.00	0.00	0.00	0.00	4,800.00
513 · Office Supplies	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
517 · Auto Allowance	550.00	550.00	550.00	550.00	550.00	825.00	275.00	550.00	550.00	0.00	0.00	0.00	4,950.00
520 · Retiree Benefits	11,542.63	11,542.63	11,542.63	11,542.63	11,542.63	12,095.66	12,095.66	12,095.66	0.00	0.00	0.00	0.00	94,000.13
522 · Office Equipment/Furniture	129.24	0.00	478.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	607.74
526 · Mileage/Parking Reimbursem	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
527 · General Office Expense	1,081.26	1,386.08	951.91	1,723.35	1,309.66	1,097.73	3,406.69	467.61	0.00	0.00	0.00	0.00	11,424.29
529 · Pre-funding Retiree Benefits	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
531 · Technology & Software	467.39	1,139.73	5,407.82	435.38	4,108.69	402.98	683.96	997.07	0.00	0.00	0.00	0.00	13,643.02
600 · Board of Trustees Compensa	1,380.45	2,421.74	3,622.43	409.50	825.01	1,308.34	513.50	2,172.46	0.00	0.00	0.00	0.00	12,653.43
601 · Trustee Expenses	0.00	0.00	0.00	0.00	60.17	4,226.84	5,987.92	231.42	0.00	0.00	0.00	0.00	10,506.35
602 · Accounting Services	475.00	475.00	475.00	475.00	475.00	475.00	475.00	380.00	0.00	0.00	0.00	0.00	3,705.00
603 · Legal Fees (General)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
604 · Flood Litigation	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
606 · Legislative Services	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
607 · Dues and Assoc. Expenes	0.00	700.00	0.00	0.00	0.00	2,175.00	0.00	9,300.00	0.00	0.00	0.00	0.00	12,175.00
608 · Insurance Premiums	4,832.00	11,702.50	3,733.00	4,347.50	373.50	3,800.00	2,750.00	2,189.50	0.00	0.00	0.00	0.00	33,728.00
609 · Conference /Workshops/Sem	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
610 · Public Relations Information	3,591.00	4,090.60	3,294.00	0.00	0.00	941.50	0.00	7,274.50	0.00	0.00	0.00	0.00	19,191.60
611 · Election Expenses	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
612 · District Annexations	0.00	0.00	5,862.00	10,144.00	7,653.00	0.00	12.26	267.74	0.00	0.00	0.00	0.00	23,939.00
613 · Community Services	0.00	12,051.47	0.00	23,586.93	6,374.50	0.00	7,187.68	0.00	0.00	0.00	0.00	0.00	49,200.58
614 · Miscellaneous Admin	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
617 · Investment Fees	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
618 · Property Tax	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
619 · Building Maintenance	3,579.77	238.25	172.36	166.94	79.40	796.35	420.94	196.58	141.75	0.00	0.00	0.00	5,792.34
620 · Bookkeeping Services	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
621 · County Assessment Fees	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
622 · County DTech Fees for DLMS	0.00	0.00	0.00	1,709.68	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1,709.68

#### AMERICAN RIVER FLOOD CONTROL DISTRICT Cash Flow Report July 2020 through June 2021

623 · Employee Morale/Wellness	0.00	4.391.00	0.00	0.00	4,412.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	8,803.00
Total Administrative	33,112.93	57,270.85	42,117.72	60,660.43	44,470.88	33,677.00	39,904.51	41,893.83	691.75	0.00	0.00	0.00	353,799.90
	55,1.2.55	01,210.00	,	50,000.10	, 0.00	30,077.00	00,0001	11,000.00	300	0.00	0.00	0.00	000,, 00.00
Special Projects Expenses	20-Jul	20-Aug	20-Sep	20-Oct	20-Nov	20-Dec	21-Jan	21-Feb	21-Mar	21-Apr	21-May	21-Jun	TOTAL
702 · Engineering/Survey Studies	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
703 · Encroachment Remediation §	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
704 · Vegetation Management	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
705 · Small Capital Projects	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
707 · Levee Standards Compliance	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Total Special Projects	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Capital Outlay: Flood Control	20-Jul	20-Aug	20-Sep	20-Oct	20-Nov	20-Dec	21-Jan	21-Feb	21-Mar	21-Apr	21-May	21-Jun	TOTAL
700 · Bank Protection	0.00	0.00	31,669.50	0.00	0.00	0.00	0.00	0.00	(7,750.00)	0.00	0.00	0.00	23,919.50
701 · Magpie Creek	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
706 · Property Acquisition	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
709 · Equipment Purchase (> \$5000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Total Capital Outlay: Flood Control	0.00	0.00	31,669.50	0.00	0.00	0.00	0.00	0.00	(7,750.00)	0.00	0.00	0.00	23,919.50
Income													
120 · Benefit Assessment	0.00	30,998.97	0.00	0.00	0.00	0.00	761,943.10	0.00	0.00	0.00	0.00	0.00	792,942.07
122 · SAFCA CAD4	980.000.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	980,000.00
123 · Interest	2,388.20	616.69	328.85	1,135.62	42.90	38.95	580.39	95.53	0.00	0.00	0.00	0.00	5,227.13
124 · O&M Agreements	0.00	0.00	0.00	0.00	0.00	274,176.70	0.00	0.00	0.00	0.00	0.00	0.00	274,176.70
126 · Miscellaneous Income	0.00	0.00	0.00	0.00	0.00	10,837.50	19,472.14	0.00	0.00	0.00	0.00	0.00	30,309.64
Total Income	982,388.20	31,615.66	328.85	1,135.62	42.90	285,053.15	781,995.63	95.53	0.00	0.00	0.00	0.00	2,082,655.54
Fund Balance													
District Operations Fund	Jul 20	Aug 20	Sept 20	Oct 20	Nov 20	Dec 20	Jan 21	Feb 21	Mar 21	Apr 21	May 21	Jun 21	
Beginning Balance	1,665,499.72	2,804,306.38	2,593,390.77	2,377,245.11	2,170,343.65	2,009,295.39	2,080,669.93	2,574,264.25	2,393,257.60	0.00	0.00	0.00	
Income	1,332,388.20	31,615.66	328.85	1,135.62	42.90	285,053.15	781,995.63	95.53	0.00	0.00	0.00	0.00	
Expenses	193,581.54	242,531.27	216,474.51	208,037.08	161,091.16	213,678.61	288,401.31	181,102.18	82,732.83	0.00	0.00	72,000.00	
Ending Balance	2,804,306.38	2,593,390.77	2,377,245.11	2,170,343.65	2,009,295.39	2,080,669.93	2,574,264.25	2,393,257.60	2,310,524.77	0.00	0.00	(72,000.00)	
Capital Outlay Reserve Fund													
Beginning Balance	1,270,000.00	920,000.00	920,000.00	920,000.00	920,000.00	920,000.00	920,000.00	920,000.00	920,000.00	0.00	0.00	0.00	
Income	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		
Expenses	350,000.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		
Ending Balance	920,000.00	920,000.00	920,000.00	920,000.00	920,000.00	920,000.00	920,000.00	920,000.00	920,000.00	0.00	0.00	0.00	
Retiree Health Benefit Reserve Fund												<del></del>	
Beginning Balance	3.552.014.00	3.552.014.00	3.552.014.00	3.552.014.00	3.552.014.00	3.552.014.00	3.552.014.00	3.552.014.00	3.552.014.00	0.00	0.00	0.00	
Income	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	72,000.00	
Expenses	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
Ending Balance	3,552,014.00	3,552,014.00	3,552,014.00	3,552,014.00	3,552,014.00	3,552,014.00	3,552,014.00	3,552,014.00	3,552,014.00	0.00	0.00	72,000.00	
Florida Santa Sant	F 1												
Flood Emergency Response Reserve Beginning Balance	1,500,000.00	1,500,000.00	1,500,000.00	1,500,000.00	1,500,000.00	1,500,000.00	1,500,000.00	1,500,000.00	1,500,000.00	0.00	0.00	0.00	
Income	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
Expenses	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
Ending Balance	1,500,000.00	1,500,000.00	1,500,000.00	1,500,000.00	1,500,000.00	1,500,000.00	1,500,000.00	1,500,000.00	1,500,000.00	0.00	0.00	0.00	
<del></del> _													
Emergency Repair Reserve Fund	-		<u>-</u>			-	<u> </u>		<u> </u>	<u> </u>			
Beginning Balance	1,500,000.00	1,500,000.00	1,500,000.00	1,500,000.00	1,500,000.00	1,500,000.00	1,500,000.00	1,500,000.00	1,500,000.00	0.00	0.00	0.00	
Income	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
Expenses Ending Rolenge	0.00	0.00	0.00	0.00	0.00 1,500,000.00	0.00 1,500,000.00	0.00	0.00 1,500,000.00	0.00	0.00	0.00	0.00	
Ending Balance	1,000,000.00	1,500,000.00	1,500,000.00	1,500,000.00	1,500,000.00	1,500,000.00	1,500,000.00	1,500,000.00	1,500,000.00	0.00	0.00	0.00	
Total Balance	10,276,320.38	10,065,404.77	9,849,259.11	9,642,357.65	9,481,309.39	9,552,683.93	10,046,278.25	9,865,271.60	9,782,538.77	0.00	0.00	0.00	
												_	

Item 3

	Acct. #	Paid to	Memo		Amount	Chk. #	
	504	ARFCD General Fund	February Expenses	\$	88,760.36		<b>#</b> 00 040 00
2	504 520	ACWA JPIA ACWA JPIA	Medical/Dental/Vision Retiree Benefits	\$	20,214.56 12,095.66		\$ 32,310.22
3	527	Alhambra/Sierra Springs	General Office Expense	\$	32.85		
4	505	AT&T	Telephone	\$	697.64		
5 6	505 511	AT&T Analog Bar-Hein Company	Telephone Equipment Repair/Parts	\$	144.50 1,063.19		
7	511	Battery Bill	Equipment Repair/Parts	\$	379.82		
8	800	Benson Fence Co. A Corp	Building Improvements/Maint	\$	932.48		
10	527 514	Blue Ribbon Maintenance Capitol Barricade. Inc.	General Office Expense Levee Maint(Supplies&Materials)	\$	700.00 390.85		
11	508	Carquest	Fuel/Oil	\$	9.09		\$ 109.36
12	511	Carquest	Equipment Repair/Parts	\$	88.32		
13 14	512 527	Carquest Clark Pest Control	Shop Supplies General Office Expense	\$	11.95 92.00		
15	508	Contour-Sierra LLC	Fuel/Oil	\$	717.47		\$ 1,759.41
16	511	Contour-Sierra LLC	Equipment Repair/Parts	\$	1,041.94		
17 18	512 603	Del Paso Pipe & Steel  Downey Brand	Shop Supplies Legal Fees (General)	\$	2,214.80 987.50		
19	511	Fastenal	Equipment Repair/Parts	\$	5.57		
20	511	Grainger Inc.	Equipment Repair/Parts	\$	62.24		\$ 919.72
21	512	Grainger Inc.	Shop Supplies	\$	857.48		
22	533 508	Home Depot Hunt & Sons	Urban Camp Cleanup Fuel/Oil	\$	223.86 3,821.78		
24	527	KBA Document Solutions	General Office Expense	\$	186.00		
25	515	Kent Arborist Services	Levee Maintenance Services	\$	6,400.00	-	
26 27	533 511	L and D Landfill Les Schwab Tire Center	Urban Camp Cleanup Equipment Repair/Parts	\$ \$	2,184.13 179.80		
28	902	Lionakis	Architect/Building Design	\$	2,360.00		
29	605	MBK Engineers	Engineering Services	\$	5,628.80		
30	531 511	Muller & Associates, Inc.  Municipal Maintenance Equipment, Inc	Technology & Software Equipment Repair/Parts	\$	390.00 385.86		
32	511	Napa Auto Parts	Equipment Repair/Parts	\$	49.35		
33	507	North Sacramento Land Company	Office/Shop Lease	\$	600.00		
34 35	523 527	Nutrien Ag Solutions, Inc. Pacific Records Management	Levee Maint. (Chemicals) General Office Expense	\$	3,507.30 85.00		
36	620	Robert Merritt, CPA	Bookkeeping Services	\$	712.50		
37	800	Rua & Son Mechanical, Inc.	Building Improvements/Maint	\$	17,606.60		
38	614	Sacramento City Commercial Tax	Miscellaneous Admin	\$	38.00		
40	533 506	Sacramento County MSA Sacramento Utilities	Urban Camp Cleanup Utility Charges	\$	(45.15) 1,215.83		
41	515	Sierra Waste Recycling & Transfer Station	Levee Maintenance Services	\$	1,011.45		
42	506	SMUD	Utility Charges	\$	1,233.16		
43	506 531	Sonitrol Streamline	Utility Charges Technology & Software	\$	1,176.05 200.00		
45	527	TIAA Bank	General Office Expense	\$	183.66		_
46	527	Umpqua Bank	General Office Expense (Pitney Bowes)  Technology & Software (Crashplan, MSFT, GoToMeeting)	\$	49.00		\$ 3,355.64
47	531 506	Umpqua Bank Umpqua Bank	Utility Charges (City of Sacramento Dept of Utilities)	\$	157.64 3,149.00		
49		US Bank	Urban Camp Cleanup (United Site Services)	\$	259.50		
50		Valley Truck & Tractor Co	Equipment Repair/Parts	\$	2,509.89		
51 52	505 800	Verizon Wireless Warehouse Paint	Telephone Building Improvements/Maint	\$	387.26 15.06		
53	506	Waste Management of Sacramento	Utility Charges	\$	539.90		
54	533	Wilson Bohannan Padlock Co.	Urban Camp Cleanup	\$	1,083.29		
			Accounts Payable Subtotal	\$	100,224.43		
			Accounts Payable and General Fund Aggregate	•	100 004 70		
			Total:	Þ	188,984.79		

Invoices Paid	T	DATE	AMOUNT	CHECK #
Clark Pest Control (General Offi	co Evnonco)	2/12/21	\$92.00	8101
Home Depot (Equipment Repair		2/12/21	\$438.99	8102
Quickbooks (Employees)	Truits, Chop Cupplics)	2/16/21	\$35.75	EFT
HSA (Employee)		2/16/21	\$150.00	EFT
HSA (Miscellaneous Expense)		2/16/21	\$2.95	EFT
Lozano, Adrian (Employee Unifo	orms)	2/17/21	\$325.00	8103
Quickbooks (Trustees)		2/19/21	\$13.00	EFT
Quickbooks (Employees)		3/1/21	\$114.75	EFT
HSA (Employee) DMV (Miscellaneous Admin)		3/2/21	\$150.00	EFT
DMV (Miscellaneous Admin)		3/9/21	\$27.00	8104
		Total	\$818.45	
		<u> </u>		
Trustee Compensation	DATE	GROSS	NET	CUK#
2/12/2021 Board Meeting	DATE	GROSS	NET	CHK#
Holloway, Brian F	2/19/21	\$95.00	\$86.59	Direct Dep
Johns, Steven T	2/19/21	\$95.00		Direct Dep
L'Ecluse, Tamika AS	2/19/21	\$95.00	·	Direct Dep
Vander Werf, Rachelanne	2/19/21	\$95.00		Direct Dep
Trustee Taxes				
		DATE	AMOUNT	CHK#
2/12/2021 Board Meeting				<u></u>
Federal Tax Payment		2/19/21	\$58.16	EFT
CA ULL S ETT		2/19/21	\$4.56	EFT
CA UI & ETT		2/19/21	\$6.44	EFT
		Total	\$69.16	
		<u> </u>		
Payroll Summary				
Payroll Summary	DATE	GROSS	NET	CHK#
PP ending 2/15/2021	DAIL	51.000	11=1	<i>□</i>
Malane Chapman	2/16/21	\$3,446.96	\$2,118.98	Direct Dep
David Diaz	2/16/21	\$2,599.52		Direct Dep
Gilberto Gutierrez	2/16/21	\$2,834.48	\$1,728.49	Direct Dep
Ross Kawamura	2/16/21	\$4,360.46	\$2,260.14	Direct Dep
Lucas Kelley	2/16/21	\$2,376.88		Direct Dep
Tim Kerr	2/16/21	\$7,466.41	+-, -	Direct Dep
Adrian Lozano	2/16/21	\$1,936.00		Direct Dep
Victor Palacios	2/16/21	\$2,130.48		Direct Dep
Erich Quiring	2/16/21 2/16/21	\$2,710.40 \$2,781.68		Direct Dep
Jose Ramirez Scott Webb	2/16/21	\$2,781.68		Direct Dep
Scott Webb	2/10/21	ψ3,311.44	Ψ2,141.92	Direct Dep
PP ending 2/28/2021				
Malane Chapman	3/1/21	\$2,820.24		Direct Dep
David Diaz	3/1/21	\$2,126.88		Direct Dep
Gilberto Gutierrez	3/1/21	\$2,319.12		Direct Dep
Ross Kawamura Lucas Kelley	3/1/21	\$4,360.46 \$1,944.72		Direct Dep
Tim Kerr	3/1/21 3/1/21	\$7,944.72		Direct Dep
Adrian Lozano	3/1/21	\$1,584.00		Direct Dep
Victor Palacios	3/1/21	\$1,743.12		Direct Dep
Erich Quiring	3/1/21	\$2,217.60		Direct Dep
Jose Ramirez	3/1/21	\$2,275.92		Direct Dep
Scott Webb	3/1/21	\$2,709.36		Direct Dep
	Tatal	<b>\$67 500 54</b>	\$44,785.72	
	Total	\$67,522.54	<b>Ψ44,103.12</b>	
				_
Employee & Relief GM Taxes		DATE	AMOUNT	CHK#
PP ending 2/15/2021		DAIE	AWIOUNI	CHK#
Federal Tax Payment		2/16/21	\$8,972.98	EFT
CA Withholding & SDI		2/16/21	\$1,802.70	EFT
CA UI & ETT		2/16/21	\$253.54	EFT
DD anding 2/20/2024				
PP ending 2/28/2021 Federal Tax Payment		3/1/21	\$7,730.90	EFT
CA Withholding & SDI		3/1/21	\$1,447.99	EFT
CA UI & ETT		3/1/21	\$43.70	EFT
				_
		Total	\$20,251.81	
<u> </u>		DATE	AMOUNT	CHK#
Employee Pension		_		
PP endin 2/15/2021	Linding de al Linding	0/10/21	<b>#0 500 0</b>	
PERS Retirement Contribution (	Unfunded Liability)	2/16/21	\$6,532.93	EFT
PERS Retirement Contribution 457 Deferred Comp (Employee	L Paid)	2/16/21 2/16/21	\$5,518.63 \$2,935.74	EFT EFT
457 District Contribution	. GIQ)	2/16/21	\$2,935.74	EFT
			,	
DD andin = 0/00/0004				
PP ending 2/28/2021 PERS Retirement Contribution		3/1/21	\$4,899.58	CCT
457 Deferred Comp (Employee	L Paid)	3/1/21	\$4,899.58 \$2,828.34	EFT EFT
457 District Contribution	. 4.4)	3/1/21	\$60.00	EFT
		5, .,1	<del></del>	
		Total	\$22,835.22	_
T-(-1-4) . T.: :-			#00 ==== =	· <del></del>
Total of Invoices Paid and Pay	/roll		\$88,760.36	

# American River Flood Control District Central Valley Flood Protection Board Permit Application American River Bridge Widening (CalTrans)

### **Staff Report**

#### **Discussion:**

The California Department of Transportation submitted an encroachment permit application to widen the existing Business 80 Bridge crossing of the American River. The proposed work includes adding lanes to the east and west bound spans of the bridge and adding an additional pedestrian lane with access ramps to the levees.

The work will include modification to existing bridge piers in the channel and to the abutments. The hydraulic analysis conducted for the proposed modified channel conditions show a negligible impact to the river hydraulics.

The addition of the pedestrian access ramps will require modification to the American River South Levee. Additional fill will be required to create the ramp connection from the levee crown to the bridge deck. The ramp proposed for the American River North Levee indicates connection to a waterside toe access that is not currently developed. This may be for future trails proposed by others.

The work as currently configured will not greatly affect the current operations and maintenance regimen of the District. The inclusion of the pedestrian access ramps will necessitate the expansion of CalTrans' maintenance boundary to extend farther away from the current bridge footprint. The District will work with CalTrans to identify the boundary of their maintenance and any overlap with District responsibilities.

#### Recommendation:

The General Manager recommends that the Board of Trustees endorse the permit application.

#### DEPARTMENT OF TRANSPORTATION

DISTRICT 3 703 B STREET MARYSVILLE, CA 95901 PHONE: (530) 741-4534

December 29, 2020 EA: 03-3F070

Prj. ID: 0312000054 Loc: 03-Sac-51 PM 2.0/3.5

Mr. Michael Wright Chief Engineer Central Valley Flood Protection Board 3310 El Camino Avenue, Suite 170 Sacramento, California 95821

Subject: Draft Central Valley Protection Board (CVFPB)/ Section 408 United States Army Corps of Engineers (USACE) Permit Application regarding project EA. 03-3F070

Dear Michael Wright:

Enclosed are two (2) copies of the Encroachment Permit Application (DWR 3615) and Environment Questionnaire (DWR 3615a) with supporting documentation.

In addition, the following below include background information, scope of work, project alternatives, and project vicinity to show where work is going to occur:

### **Background & History**

An original Project Scope Summary Report (PSSR) was completed in November 2011 for Structure Rehabilitation of three bridges including 21<sup>st</sup> Avenue Undercrossing, Sawmill Undercrossing, and American River Bridge. A Supplemental PSSR was completed in June 2015 to separate the American River Bridge from the other two structures, to replace the deck and widen the bridge to accommodate traffic handling during construction. In October 2015, the project was programmed as an amendment to the 2016 SHOPP as a Long Lead project. The project is currently programmed in the 2020 SHOPP as a Contingency (G-13) Project.

### Scope of work

Project EA. 03-3F070 proposes to rehabilitate the American River Bridge (Br. No. 24-0003) by removing and replacing the existing concrete deck, removing and replacing the steel girder post-tensioning systems in spans 1 and 2, modify existing soundwall, install sheet piling around piers for scour mitigation, construct concrete catcher blocks, widen the bridge to accommodate traffic during construction, add a Class I bike/pedestrian path, and plan for future transportation needs on State Route (SR) 51.

#### **Proposed Alternatives**

Due to the large volume of traffic that uses SR 51, the Traffic Management Plan (TMP) recommends keeping 3 lanes of traffic open in each direction of travel during construction. In order to accommodate this recommendation, the bridge must be widened permanently to keep three lanes open for traffic during construction and to allow the space for the contractor to work.

#### **Alternative 1:**

The project scope for Alternative 1 includes the following elements:

- Remove and replace the existing concrete bridge deck (Bridge number 24-0003), with a 1<sup>1</sup>/<sub>4</sub>" thicker deck than existing.
- ➤ Widen the American River Bridge (Br. No. 24-0003) to maintain 3 lanes of traffic in each direction during construction.
- Provide a 14' bike/pedestrian path on the northbound side of the bridge separated from the traffic by a concrete barrier.
- ➤ Widen the substructure and superstructure by 54'-11"± on the northbound side of the structure.
- ➤ Widen the approaches of SR 51 to accommodate the widening of the American River Bridge.
- ➤ Modification of an existing soundwall on the southeast side of the American River bridge.
- ➤ Construct 30' approach slabs.
- > Strengthen existing girders
- Lengthen a box culvert to the East, North of the American River Bridge
- ➤ Widen bridge abutments, footings, bents, and piers supported by piles.
- ➤ Install permanent sheet piles at piers 4-6 for scour mitigation.
- Construct temporary construction access trestles and cofferdams to facilitate construction on in-water piers.
- Install lighting on the proposed bike/pedestrian path.
- Create a temporary construction access road across a wetland area or/and use existing dirt road to access the construction site
- Construct median barrier (Type 60) and bridge barrier (Type 842).
- Replace steel girder post-tensioning system at spans 1 & 2.
- ➤ Construct concrete catcher blocks underneath existing girders.
- > Install new joint seals.
- Near abutment 1, construct a retaining wall and soundwall from the modified soundwall along the Northbound side of the highway, near the Southeast quadrant of the American River Bridge and extend the retaining wall down the bike/pedestrian path.
- Remove vegetation and trees to accommodate widening of SR 51 (CapCity) for bridge deck construction staging.
- ➤ Widen Cal Expo Undercrossing (Br. No. 24-0133) on the Northbound side
- Modify the Exposition Boulevard Off-ramp in the Northbound direction

### **Alternative 2:**

In addition to the project scope common to Alternative 1, this alternative adds the following elements:

- Widen the substructure to the ultimate width by 38'-11"± on the southbound side to accommodate the future widening of SR 51.
- Alternatives 2 is contingent on obtaining additional construction capital funding (SHOPP & Non-SHOPP) prior to RTL.

#### **Alternative 3:**

In addition to the project scope common to Alternative 1, this alternative adds the following elements:

- Widen superstructure and substructure by 38'-11"± on the southbound side to accommodate the future widening of SR 51.
- > Requires no girder strengthening
- Alternative 3 is contingent on obtaining additional construction capital funding (Non-SHOPP) prior to RTL.
- Re-align the portion of the American River bicycle trail, which runs below and parallel to the bridge to be further from the edge of deck.

### **Project Vicinity**

### VICINITY MAP EA 3F0700 BRIDGE REHABILITATION

American River Bridge Br. No. 24-0003, SAC-51 PM 2.0/3.5



The following items are included in the application package:

Item Number	Document
1	Transmittal Letter
2	3615 Form
3	3615a Form
4	Environmental Document
5	HPSR Signed
6	401 WQC Application
7	404 Application
8	Standard Specifications - Earthwork
9	Standard Specifications - Aggregate Base
10	Standard Specifications - Asphalt Concrete
11	Hazardous Waste ISA
12	Standard Specifications - Treated Woodwaste
13	Project Title Sheet
14	American River Bridge Photo Summary & Index
15	Typical Cross Sections
16	Overview of Proposed Work
17	Barge Alternative Method of Construction (Instead of Trestle)
18	Layouts
19	Proposed Modification to Levee Exhibit
20	Profile & Superelevation Diagram
21	Structures General Plan
22	Parcels within project vicinity
23	Draft Preliminary Geotechnical Report
24	Draft Final Hydraulic Report
25	Riparian Planting Map
26	Riparian Planting Plan Summary
27	Preliminary Foundation Report
28	Project Schedule

Should the (CVFPB) or the (USACE) staff have any questions regarding this permit application submission or required additional information, please contact me at (530) 741-4534 or by email at Andrew.Huang@dot.ca.gov.

Sincerely,

ANDREW HUANG, P.E., Design M7 Caltrans District 3

Application No.

### DEPARTMENT OF WATER RESOURCES CENTRAL VALLEY FLOOD PROTECTION BOARD

### APPLICATION FOR A CENTRAL VALLEY FLOOD PROTECTION BOARD ENCROACHMENT PERMIT

					(For Office Use Only)
1 1	Description (	of proposed work being speci	fic to include	all items that will be cover	ed under the issued nermit
	·				003) by removing and replacing the
					ng systems in spans 1 and 2, install
		und piers for scour mitigat			ks, and widen the bridge
supe	erstructure	permanently to accommod	ate traffic d	uring construction.	
2.	Project	_			
	Location:	Sacramento		County, in Section	Sacramento
	T	TON	(N)	Dec	(E)
	Township:	T9N	(S), Range:	K5E	(W), M. D. B. & M.
	Latitude:	38° 35' 12.12" N	Longitude:	121° 26' 52.04" W	
					Designated
	Stream :	American River (29.3 mil)	, Levee :	U04(10.86)&U03(2.86)	Floodway: 115000 cfs
	APN:				
	01 : 4 =				
3.	Chris A F	Rockey / District 3 CVFPB liai		of 703 B St	
		Name of Applicant / Land Own	er		Address
Mary	ysville	California		95901	(530) 741-4517
	City	;	State	Zip Code	Telephone Number
					chris.rockey@dot.ca.gov
					E-mail
4.	Jason Mo	comber / District 3 CVFPB lia	son	of 703 B St	
٦.	-	Name of Applicant's Representa	itive	OI 703 B St	Company
Mon	ysville	California		95901	(530) 741-4480
iviai	City	· · · · · · · · · · · · · · · · · · ·	State	Zip Code	Telephone Number
					jason.mcomber@dot.ca.gov
					E-mail
5.	Endorseme	ent of the proposed project fro	om the Local	Maintaining Agency (LMA)	١.
٥.	LIIUUISEIII	ent of the proposed project in	on the Local	Walitaliling Agency (LIVIA)	<i>y</i> .
We, t	the Trustees	of <u>American River Flood Cor</u>	ntrol District (l	NA0001) approve this	s plan, subject to the following conditions
		P. 4 1 1		LO Pro Attack	The Configura
	☐ Condition	ons listed on back of this form	n <u>√</u>	Conditions Attached	☐ No Conditions
	-1			Touch	
Tru	stee		Date	Trustee	Date
				<del></del>	
I ru:	stee		Date	Trustee	Date

### APPLICATION FOR A CENTRAL VALLEY FLOOD PROTECTION BOARD ENCROACHMENT PERMIT

6. Names and addresses of adjacent property owners sharing a common boundary with the land upon which the contents of this application apply. If additional space is required, list names and addresses on back of the application form or an attached sheet.

Name	Address	Zip Code
See parcels within vicinity exhibit		
_		
Act of 1970?	en made of the proposed work under the Califo ☑ No ☐ Pending s of the lead agency and State Clearinghouse	·
SCH No.	-	
8. When is the project scheduled for constru	uction? <u>07/2022</u>	
Please check exhibits accompanying this	s application.	
A.  Regional and vicinity maps showi	ing the location of the proposed work.	
B.	f the proposed work to include map scale.	
C.  Drawings showing the cross section banks, flood plain,	ion dimensions and elevations (vertical datum	n?) of levees, berms, stream
D.	vations (vertical datum?) of levees, berms, flo	od plain, low flow, etc.
E. A minimum of four photographs d	epicting the project site.	
	Signature of Ap	pplicant Date
Include any additional information:	- '	

### ENVIRONMENTAL ASSESSMENT QUESTIONNAIRE FOR APPLICATIONS FOR CENTRAL VALLEY FLOOD PROTECTION BOARD ENCROACHMENT PERMITS

This environmental assessment questionnaire must be completed for all Central Valley Flood Protection Board applications. Please provide an explanation where requested. Incomplete answers may result in delays in processing permit applications. Failure to complete the questionnaire may result in rejection of the application.

1.	Has an environmental assessment or initial study been made or is one being made by a local or State permitting agency in accordance with the California Environmental Quality Act? ✓ Yes ☐ No
	If yes, identify the Lead Agency, type of document prepared or which will be prepared, and the State Clearinghouse Number:
	An Initial Study with a Mitigated Negative Declaration (IS-MND), in compliance with the California Environmental Quality Act (CEQA), was prepared for the project.
2.	Will the project require certification, authorization or issuance of a permit by any local, State or federal environmental control agency? ✓ Yes □ No
	List all other governmental permits or approvals necessary for this project or use, including U.S. Army Corps of Engineer' 404and Section 10 permits, State Water Quality Certification, Department of Fish and Game 1600 agreement, etc. Attach copies of all applicable permits.
	The project will adhere to the conditions of the Statewide National Pollutant Discharge Elimination System (NPDES) permit issued by the State Water Resources Control Board (Order No. 2012-0011-DWQ), NPDES Permit No CAS000003 along with the NPDES General Permit No. CAS000002 (Order No. 2009-0009-DWQ). The
	contractor will be required to prepare a Storm Water Pollution Prevention Plan (SWPPP) or a Water Pollution Control Plan (WPCP), 408 Permit, Clean Water Act Section 404
3.	Give the name and address of the owner of the property on which the project or use is located. Please submit a copy of your current Title Report (Grant Deed), if your proposed project includes a private residence. See Parcel Exhibit for property owner information.
4.	Will the project or use require issuance of a variance or conditional use permit by a city or county?  ✓ Yes □ No
	Explain: Due to the high traffic volumes on SR 51 and commercial truck traffic, work will be limited to nighttime hours and no lane or shoulder closure will be allowed during daytime and peak commute hours on weekdays until K-Rails are installed permitting for daytime work
5.	Is the project or use currently operating under an existing use permit issued by a local agency?  Yes No  Explain:

### ENVIRONMENTAL ASSESSMENT QUESTIONNAIRE FOR APPLICATIONS $_{\mbox{\scriptsize ltem 4}}$ FOR CENTRAL VALLEY FLOOD PROTECTION BOARD ENCROACHMENT PERMITS

6.	Describe all types of vegetation growing on the project site, including trees, brush, grass, etc. The project limits contains common vegetation communities and natural communities of special concern. The common vegetation community within the project limits are Ruderal/Developed communities. The natural vegetation communities in the project area include Riparian Forest/Shrub and Oak Woodland Savanna. Other areas included in the project are Riverine, consisting of the American River and Linda Creek which flows outside the project area.
7.	Describe what type of wildlife or fish may use the project site or adjoining areas for habitat, food source, nesting sites, source of water, etc.  The following fish and wildlife within the project sites and adjoining areas are listed as follows: Valley Elderberry Longhorn Beetle (Desmocerus californicus dimorphus), Green Sturgeon (Acipenser medirostris), California Central Valley Steelhead (Oncorhynchus mykiss), Central Valley Spring-Run and Winter-Run Chinook Salmon (Oncorhynchus tshawytsha), Brewer's Blackbird (Euphagus cyanocephalus), House Finch (Haemorhous mexicanus), European Starling (Sturnus vulgaris), Fox squirrel (Sciurus niger), Striped Skunk (Mephitis mephitis), Pacific Chorus Frog (Pseudacris regilla), common bullfrog (Lithobates catesbeianus), and raccoon (Procyon lotor)
8.	Has the Department of Fish and Game, U.S. Fish and Wildlife Service, or National Marine Fisheries Service been consulted relative to the existence of, or impacts to, threatened or endangered species on or near the project site?  Yes No  Explain: Section 7 formal consultation with NMFS and USFWS has been initiated and is currently ongoing.
9.	Will the project or use significantly change present uses of the project area?  ☐ Yes ☑ No  Explain: Biological habitat use will not significantly change in the project area. Visual cultural etc.
10.	Will the project result in changes to scenic views or existing recreational opportunities?  ☐ Yes ☐ No  Explain:  The project will not result in changes to scenic view or changes to existing recreational opportunities in the final conditions.
11.	Will the project result in the discharge of silt or other materials into a body of water?  Yes  No  Explain: There will be no discharge of silt or other materials during construction in to a body of water.

3615a (Rev. 10/11) Page 10<sub>Page 2 of 5</sub>

### ENVIRONMENTAL ASSESSMENT QUESTIONNAIRE FOR APPLICATIONS $_{\mbox{\scriptsize ltem 4}}$ FOR CENTRAL VALLEY FLOOD PROTECTION BOARD ENCROACHMENT PERMITS

12.	Will the project involve the application, use, or disposal of hazardous materials? ✓ Yes ☐ No
	If yes, list the types of materials, proposed use, and disposal plan. Provide copies of all applicable hazardous material handling plans.  See SSP 14-11.14 – Treated Wood Waste.
	See Hazardous Waste Site Investigation (ISA)
13.	Will construction activities or the completed project generate significant amounts of noise?  ☐ Yes
	Explain: No adverse noise impacts from construction are anticipated because construction would be conducted in accordance with Caltrans Standard Specifications Section 14.8-02. Construction noise would be short-term and intermittent.
14.	Will construction activities or the completed project generate significant amounts of dust, ash, smoke, fumes, or odors?  Yes  No
	Explain: The proposed project anticipates temporary short term air quality impacts during construction; however, these impacts will be reduced with incorporation of minimization methods using 2018 Caltrans Standards Specifications This project is not a traffic capacity increasing project therefore, air quality impacts will not be substantial.
15.	Will the project activities or uses involve the burning of brush, trees, or construction materials, etc?  ☐ Yes ☑ No
	Explain, and identify safety and air pollution control measures:  The proposed project does not include activities that involve burning of brush, trees, or construction materials.
10	Will the president existing a grieviture location and a continuous production of existing a grieviture location
10.	Will the project affect existing agricultural uses or result in the loss of existing agricultural lands?  Yes  No  Explain:
	The project limits do not encroach on any agricultural use lands.

3615a (Rev. 10/11) Page 11<sub>Page 3 of 5</sub>

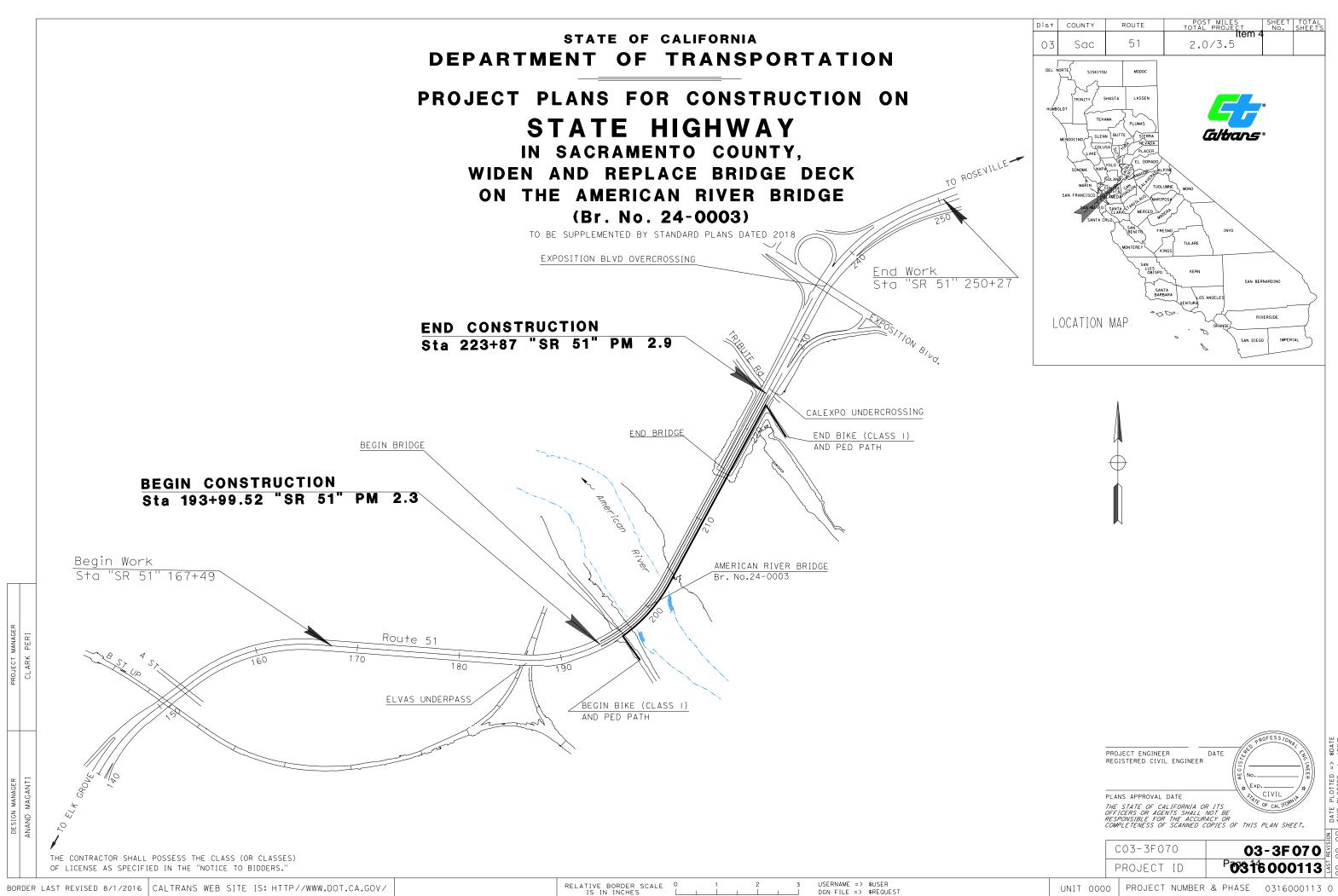
### ENVIRONMENTAL ASSESSMENT QUESTIONNAIRE FOR APPLICATIONS $_{\mbox{ltem }4}$ FOR CENTRAL VALLEY FLOOD PROTECTION BOARD ENCROACHMENT PERMITS

17.		ve any other projects similar to the propose posed project?	ed proje	ect been planned or completed in the same general area as the
	✓ ,	Yes No		
	Two Stat	te Route 51 from E Street to Arden there is	nave si enue to a worl	imilar scope. o add managed lanes and auxillary lanes in each direction ker safety proejct, adding Maintenance Vehicle Pullouts acing Metal Beam Guardrail (MBGR) with Midwest Guardrail.
18.	Will	II the project have the potential to encourag	e, facil	litate, or allow additional or new growth or development?
	<b>✓</b>	Yes No		-
	Exp	plain:		
	Rep brid	olacement of the American River Bridge de	ento Ci	idge No. 24-0003) would allow for a longer service life of the ity to Roseville. Improving the service life of the bridge will bunties.
19.	Will	ll materials be excavated from the floodplai	n? 🗌 `	Yes ☐ No If yes, please answer the remaining questions.
		THE BEMAINING OUESTIONS MUST	ONI V	BE ANSWERED IF THE ANSWER TO QUESTION
		NO. 19 WAS "YES". IF THE ANSV	VER TO	O QUESTION NO. 19 WAS "NO", YOU DO NOT THE REMAINING QUESTIONS.
	A.	What is the volume of material to be excar	vated?	
		Annually 7000 CY	Total _	14000 CY
	В.	What types of materials will be excavated Material to be excavated will be existing g		earthen material
	C.	Will the project site include processing an ✓ Yes ☐ No	d stock	kpiling of material on site?
		Explain:		
				ring June 1 to October 15 and all stock piling will be done not within the said duration.
	D.	What method and equipment will be used Excavator or similar equipment.	to exc	cavate material?

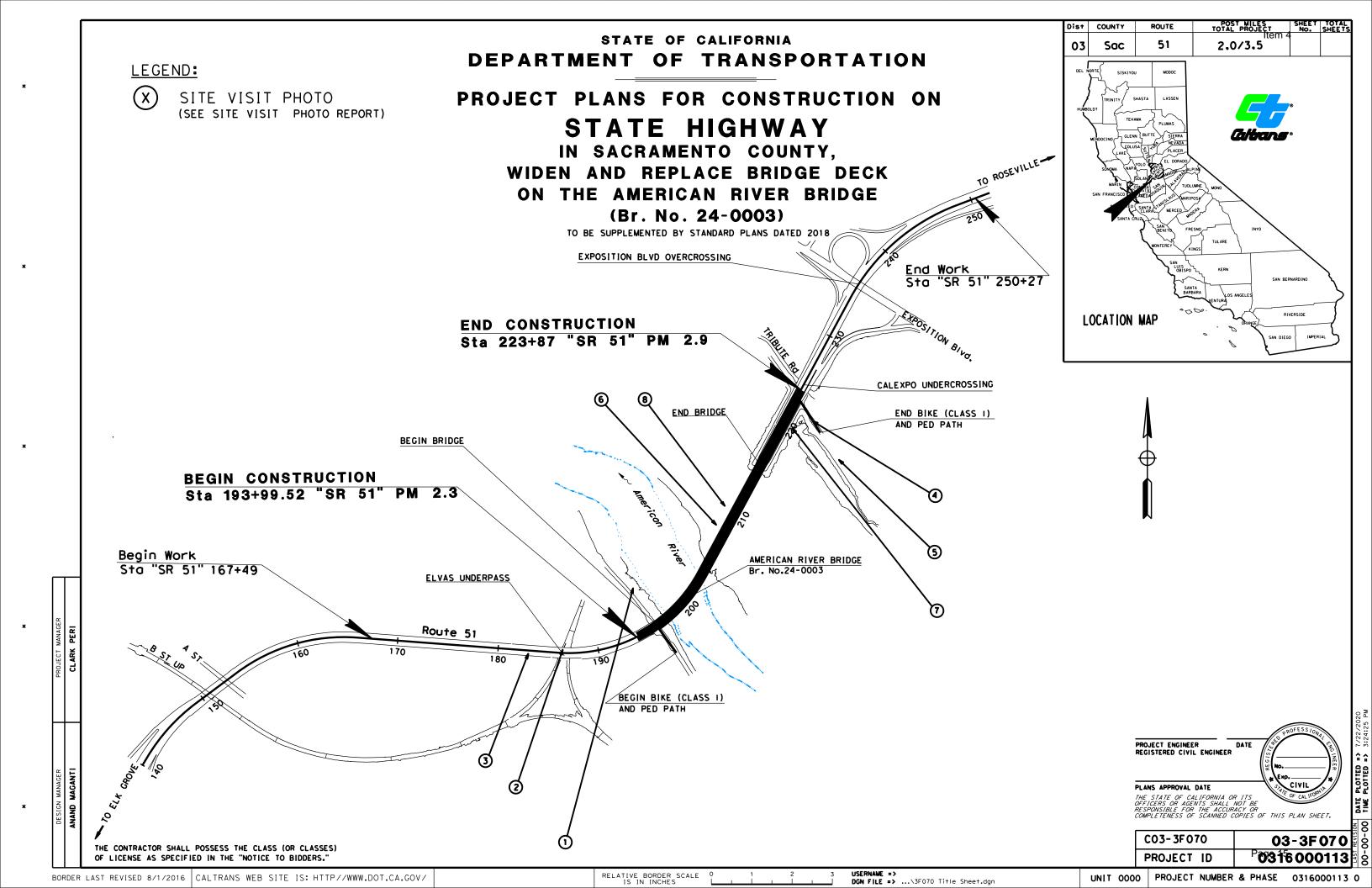
3615a (Rev. 10/11) Page 12 Page 4 of 5

### ENVIRONMENTAL ASSESSMENT QUESTIONNAIRE FOR APPLICATIONS $_{\mbox{\scriptsize ltem 4}}$ FOR CENTRAL VALLEY FLOOD PROTECTION BOARD ENCROACHMENT PERMITS

E.	What is the water source for the project?
F.	How will waste materials wash water, debris, and sediment be disposed of?
G.	What is the proposed end land use for the project site?
Н.	Has a reclamation plan been prepared for this site in accordance with the Surface Mining and Reclamation Act of 1975?
	☐ Yes ☐ No If yes, please attach a copy.



DGN FILE => \$REQUEST



### **Sac 51 American River Bridge Deck Widening**



Site Visit Photo Report – 4/26/2017 to 10/19/2017



1: GROUND LEVEL PHOTO LOOKING AT AMERICAN RIVER BRIDGE FROM THE RIVER LEVEE.



2: GROUND LEVEL PHOTO LOOKING TOWARDS SR 51 FROM UNION PACIFIC RAILROAD UNDERCROSSING.



3: GROUND LEVEL PHOTO LOOKING AT MCKINLEY SOUNDWALL AND NB SR 51.



4: GROUND LEVEL PHOTO LOOKING TOWARDS TRIBUTE ROAD OVERCROSSING FROM THE RIVER LEVEE.

### **Sac 51 American River Bridge Deck Widening**



Site Visit Photo Report – 4/26/2017 to 10/19/2017



5: GROUND LEVEL PHOTO LOOKING AT CALIFORNIA EXPOSITION CENTER LOT FROM THE RIVER LEVEE.



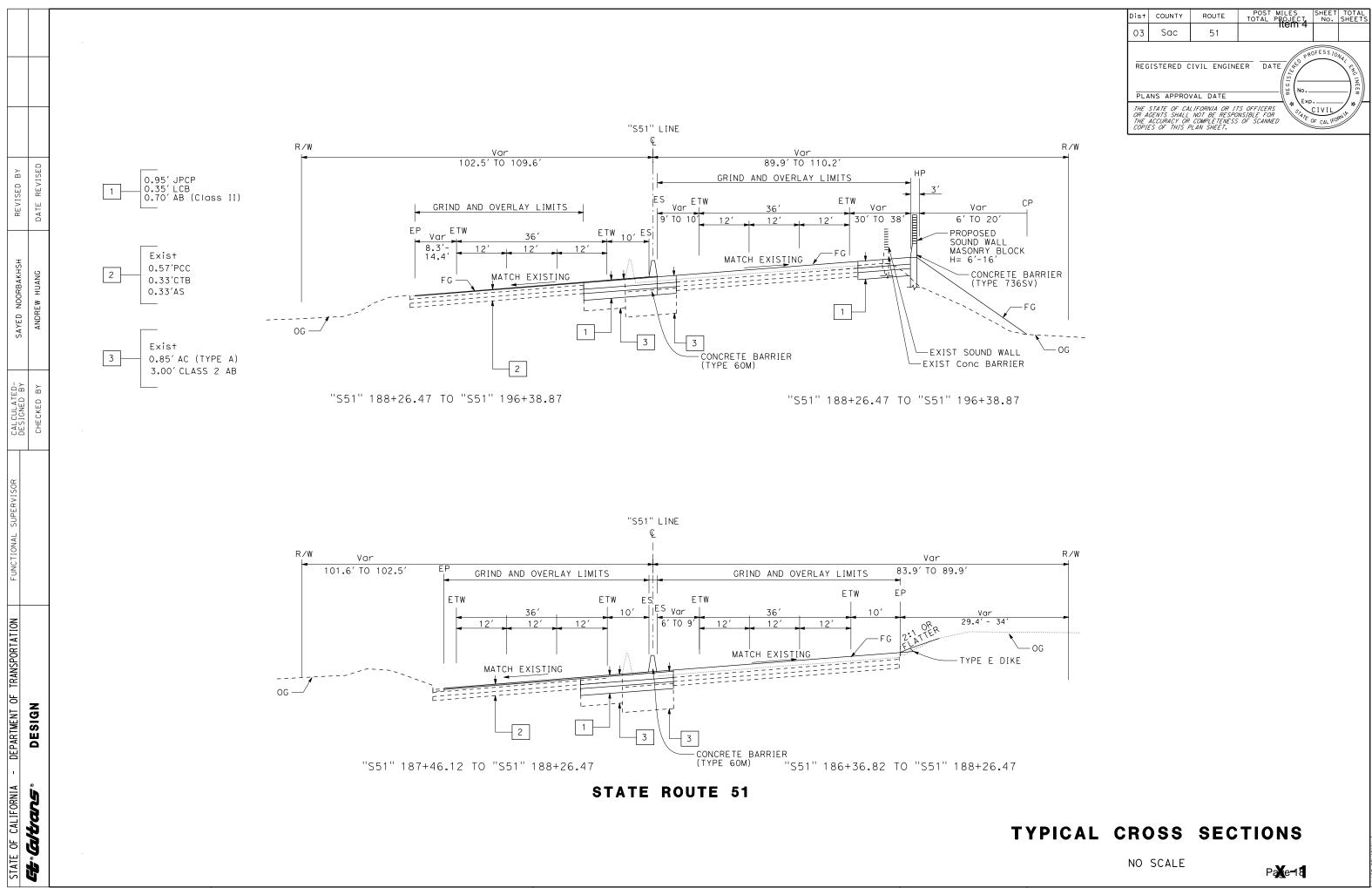
6: GROUND LEVEL PHOTO LOOKING AT EXISTING BIKE PATH UNDER SR 51.



7: GROUND LEVEL PHOTO LOOKING AT DRAINAGE BASIN EAST OF NB SR 51.



8: GROUND LEVEL PHOTO LOOKING TOWARDS AMERICAN RIVER BRIDGE FROM THE EXISTING BIKE TRAIL



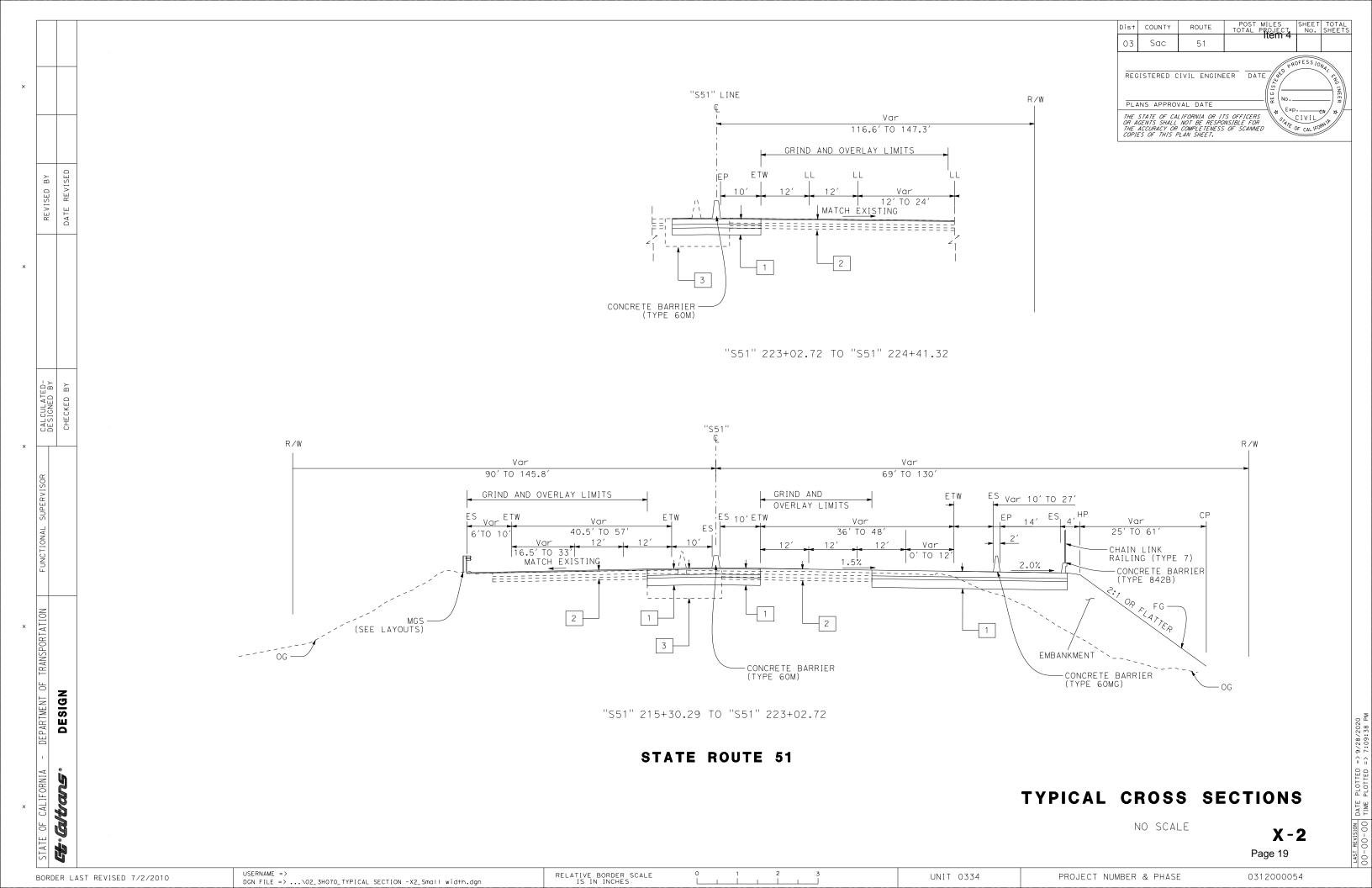
BORDER LAST REVISED 7/2/2010

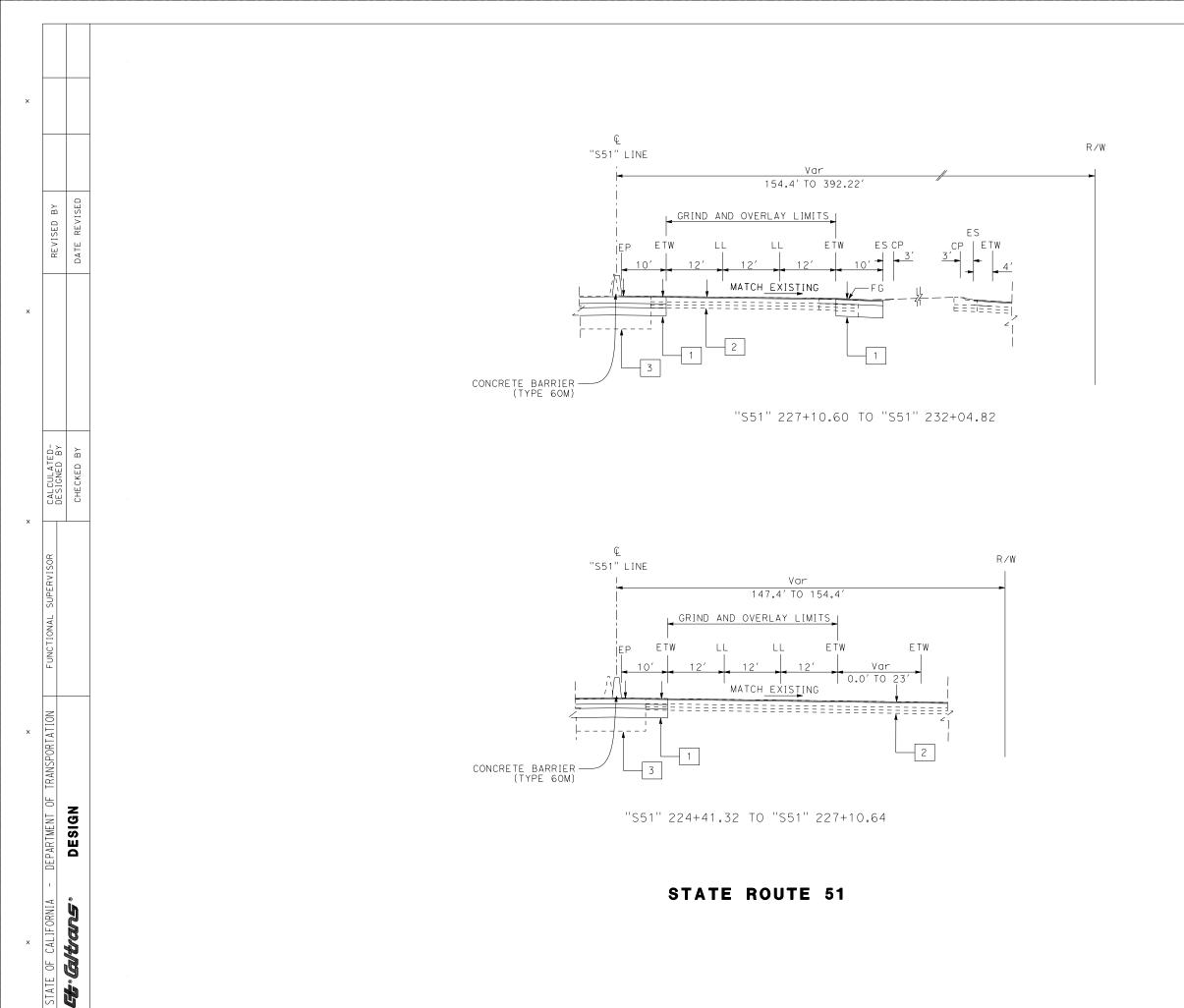
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UNIT 0334

PROJECT NUMBER & PHASE

0312000054





Dist COUNTY 03 Sac REGISTERED CIVIL ENGINEER DATE PLANS APPROVAL DATE THE STATE OF CALIFORNIA OR ITS OFFICERS OR AGENTS HALL NOT BE RESPONSIBLE FOR THE ACCURACY OR COMPLETENESS OF SCANNED COPIES OF THIS PLAN SHEET.

TYPICAL CROSS SECTIONS

NO SCALE

X-3

Page 20

BORDER LAST REVISED 7/2/2010

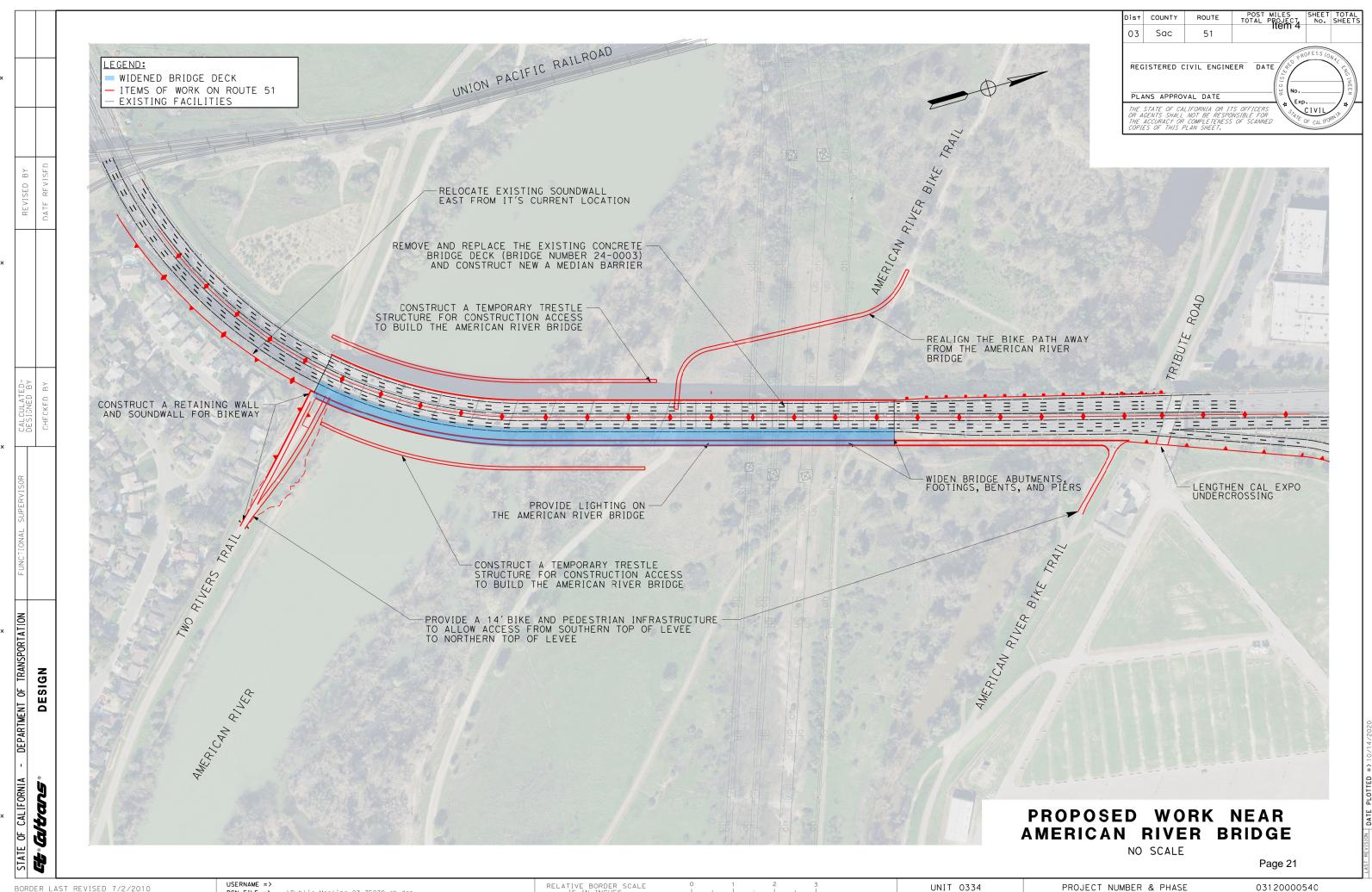
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RELATIVE BORDER SCALE IS IN INCHES

UNIT 0334

PROJECT NUMBER & PHASE

0312000054



RELATIVE BORDER SCALE
IS IN INCHES UNIT 0334 BORDER LAST REVISED 7/2/2010 DGN FILE => ...\Public Meeting 03-3F070\_ah.dgn

03120000540

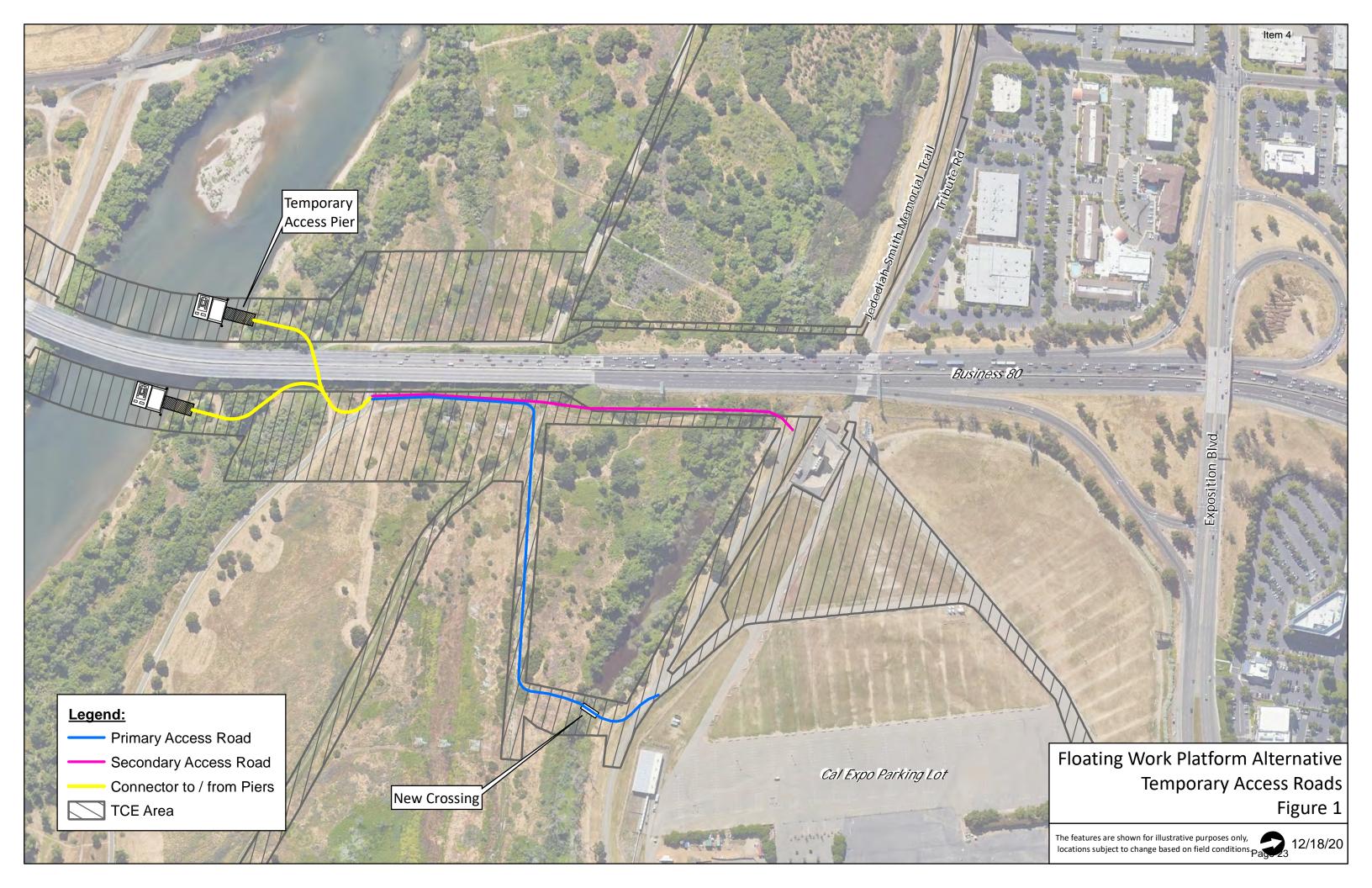
#### FLOATING WORK PLATFORM ALTERNATIVE

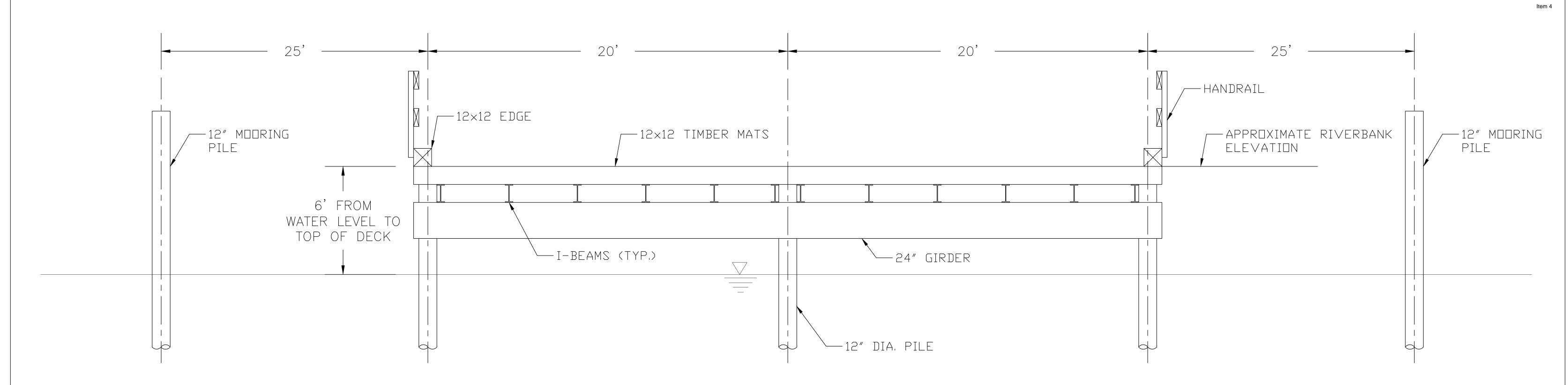
As an alternative to a trestle, floating work platforms (barges) would be used to facilitate construction activities within the American River. Use of barges would eliminate the need for a trestle along the entire width of the American River (700 piles spanning approximately 3,200') at this location for the duration of the project. In addition, use of barges would eliminate approximately two construction seasons associated with installation and removal of the trestle.

In order to facilitate the use of barges, a number of preparatory steps would be necessary:

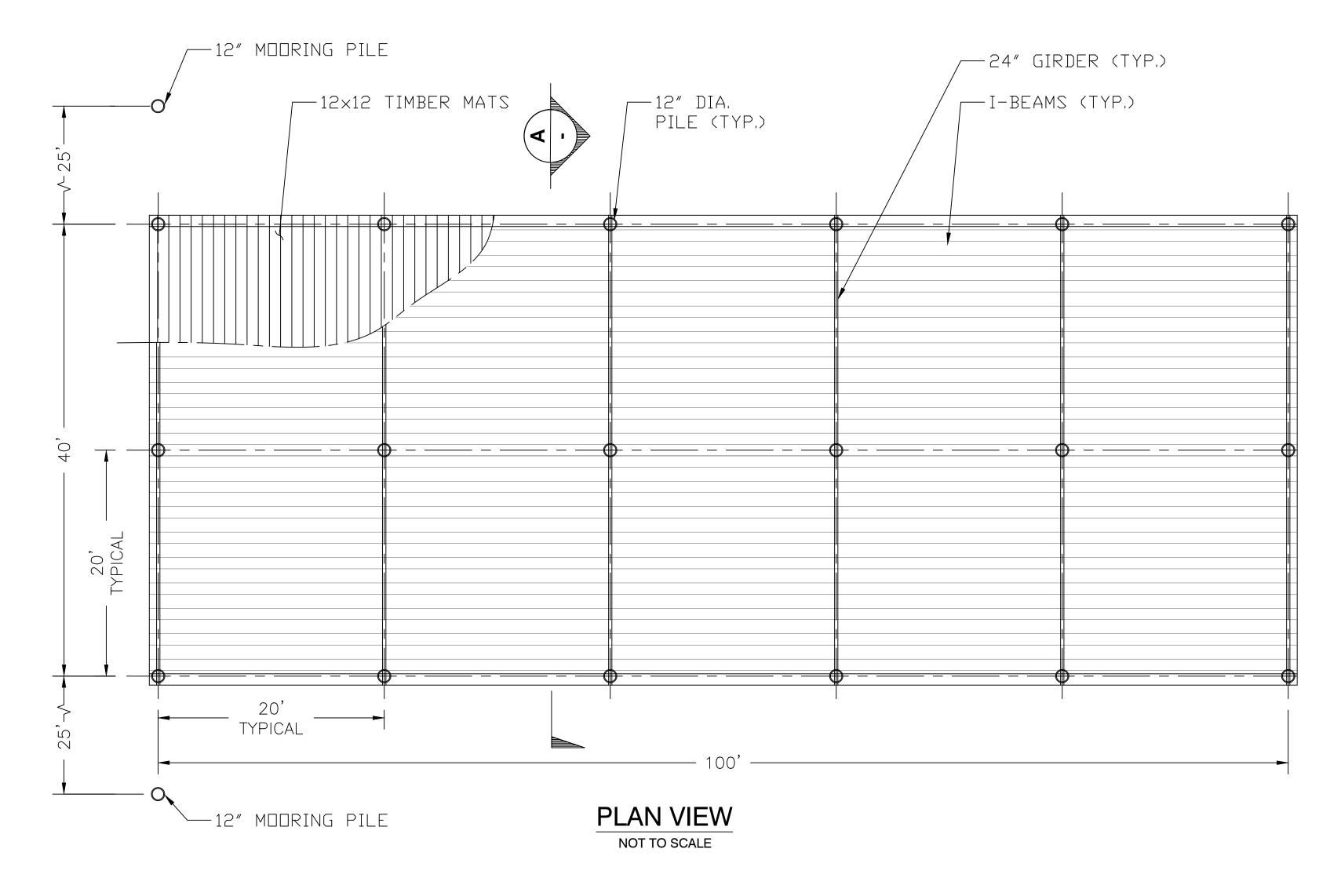
- Construct access roads on the north side of the American River from CalExpo to the temporary access pier locations on the east and west sides of the bridge. See Figure 1, Temporary Access Roads.
- 2. Construct temporary access piers. Each pier would require 20 piles 12" in diameter, which would be driven using vibratory or impact hammers. 18 piles would support the temporary access piers and the two (2) additional piles would serve as mooring points. For each pier, 9 piles will be placed in water and 9 piles will be placed on land in the floodplain. Incidental fill may be placed on land within the floodplain to enable the access road to match the grade of the access piers. See Figure 2, Temporary Access Piers and Barge Mooring Points.
- 3. The barges generally require 2' of clearance between the bottom of the barge and the riverbed for safe operation. Based on a recent bathymetric survey, approximately 23,800 cubic yards of material would be dredged in the work zone (225' from the extents of the bridge widening both upstream and downstream) to create adequate vertical clearance. See Figure 3, Dredge Work Zone. Dredging activities would take place from the temporary access piers and barges using an excavator. Assuming use of a single excavator, approximately 600 cubic yards of material would be dredged per day. With the use of small boats, barges would transport the dredged material to the access pier, where it would be directly loaded into trucks, using an excavator located on the pier, and hauled either off-site or to a temporary storage location within the project limits. The temporary storage location would be determined in coordination with the regulatory agencies. Periodic maintenance dredging may be performed in subsequent seasons to maintain adequate clearance.

The barges would support heavy equipment and construction materials for the purposes of pier installation and associated bridge widening activities. Barges would be tied to the mooring points during periods of inactivity, and would remain in the American River through the duration of the work. Water quality protection measures will be implemented, which may include a turbidity curtain and a skirted oil boom, subject to input from the regulatory agencies.





## TYPICAL SECTION NOT TO SCALE

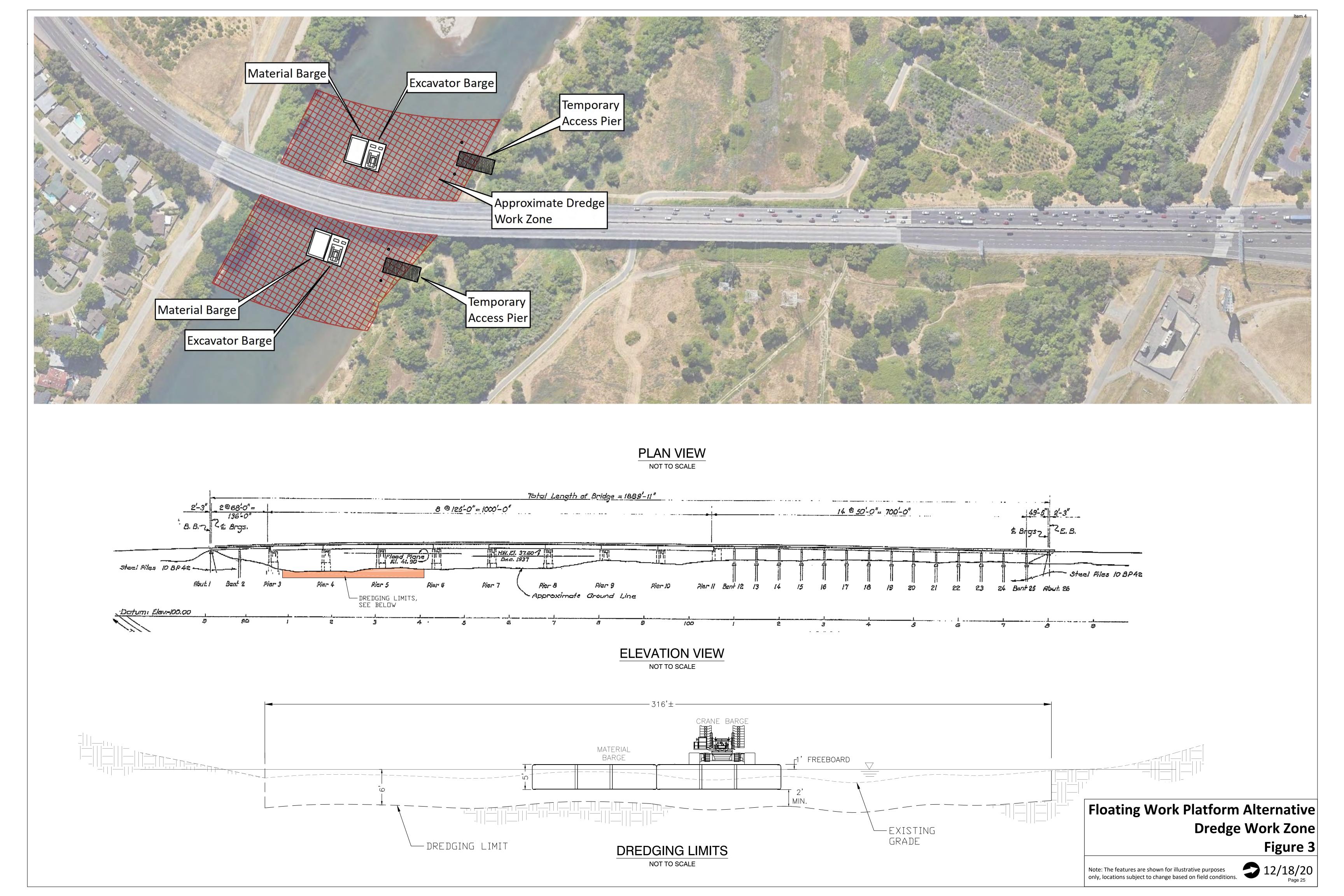


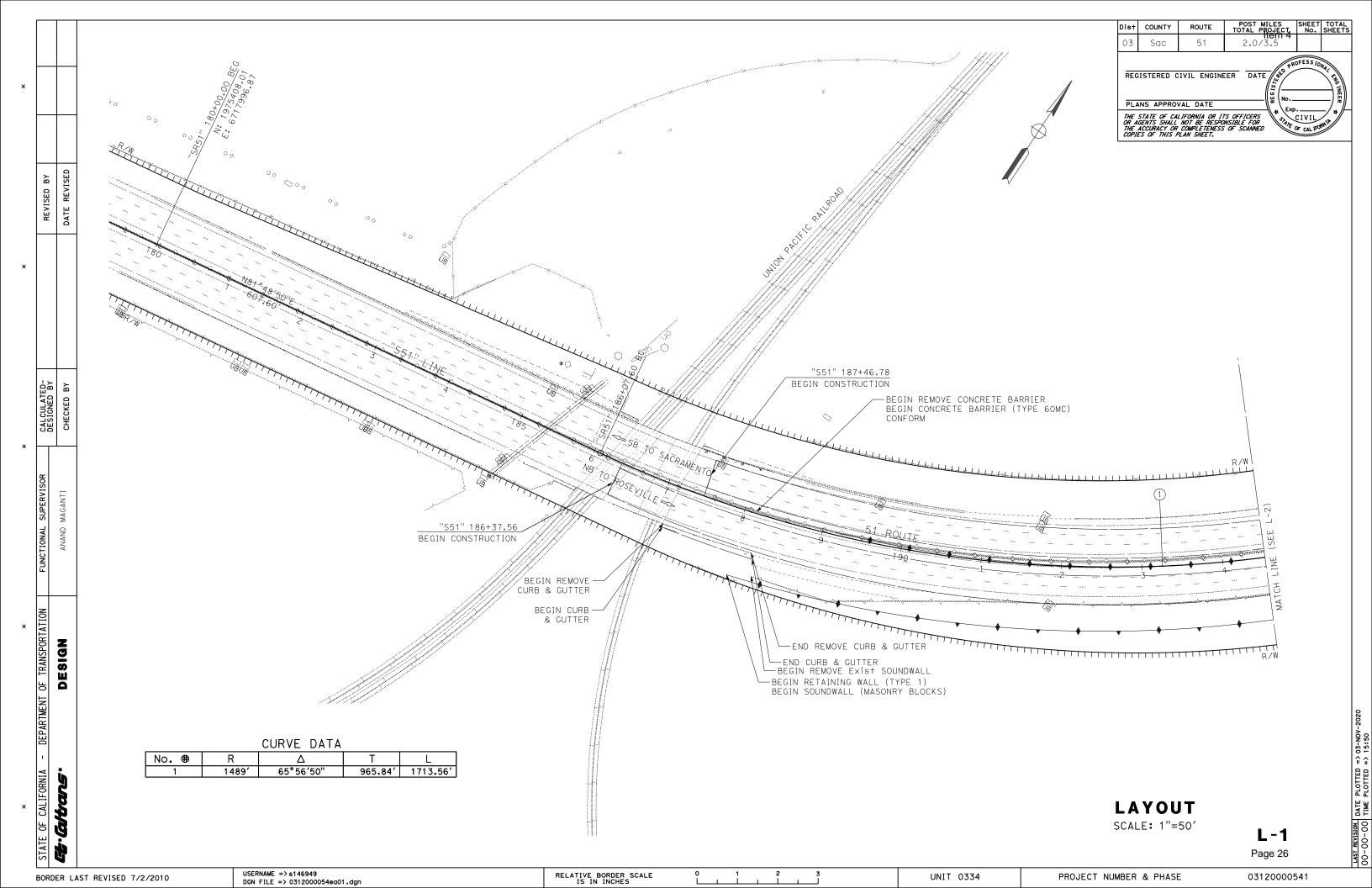
# PIER (APPROXIMATELY 40' x 100')

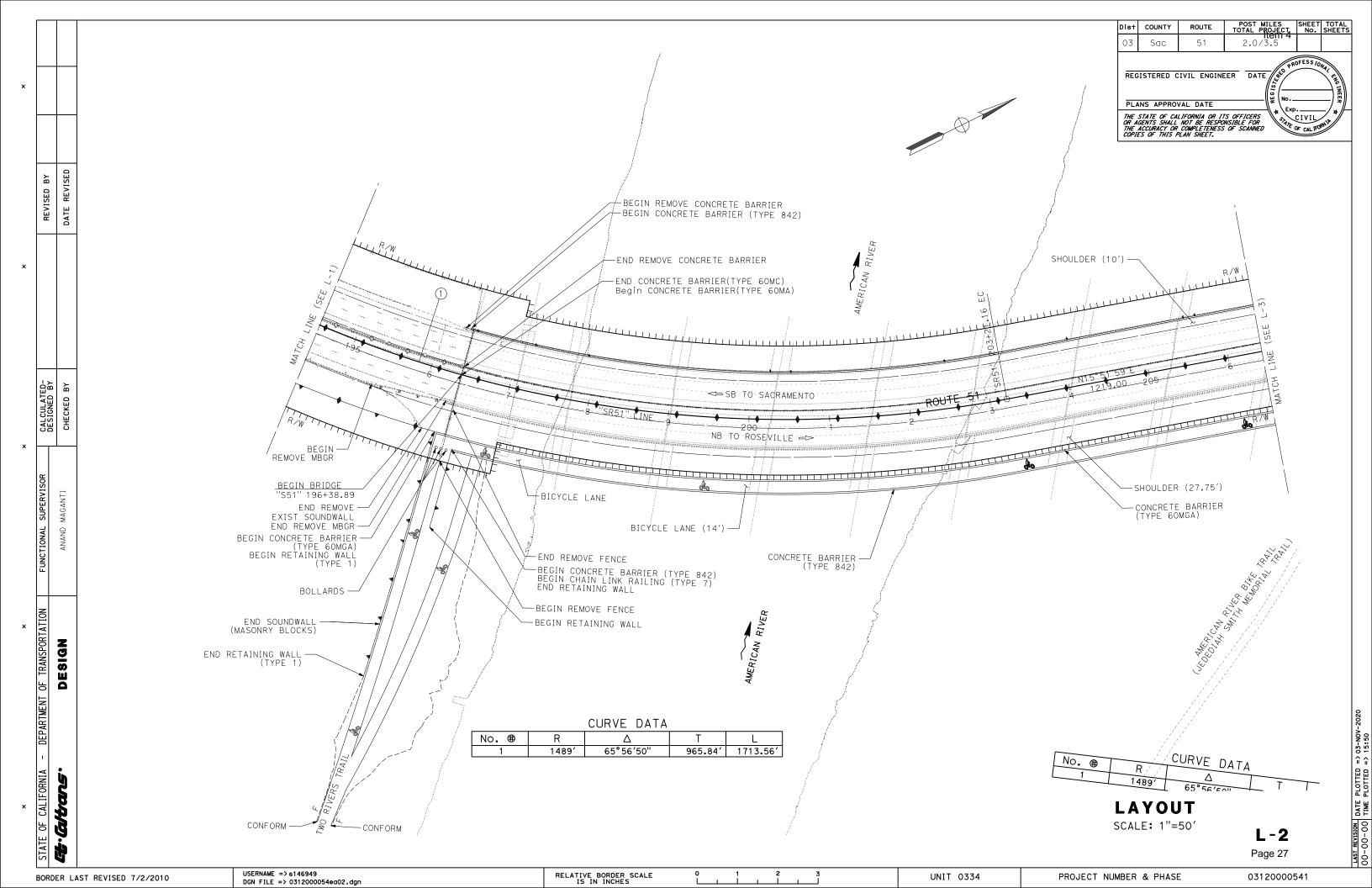
Floating Work Platform Alternative
Temporary Access Piers and Barge Mooring Points
Figure 2

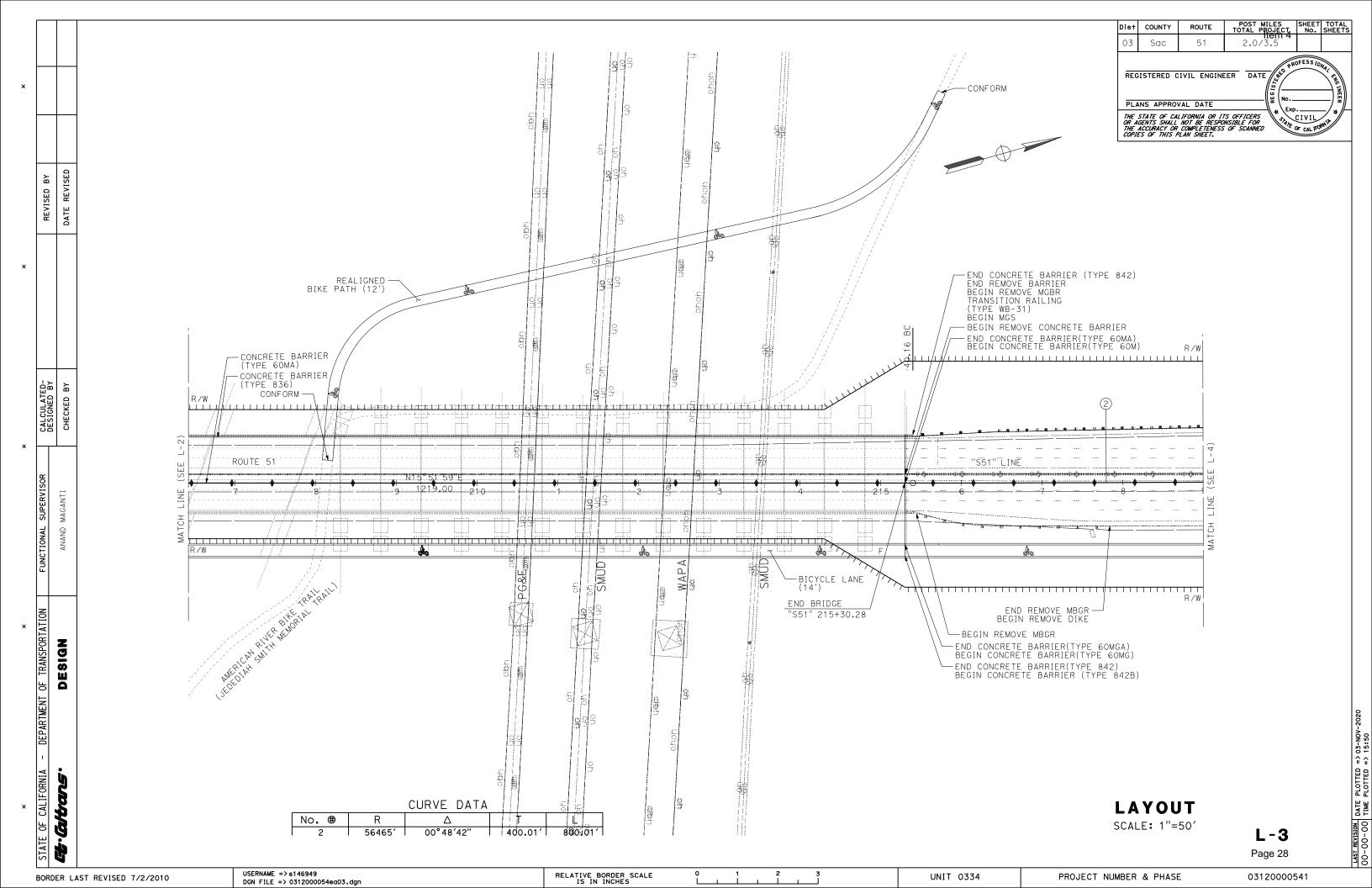
Note: The features are shown for illustrative purposes only, locations subject to change based on field conditions.

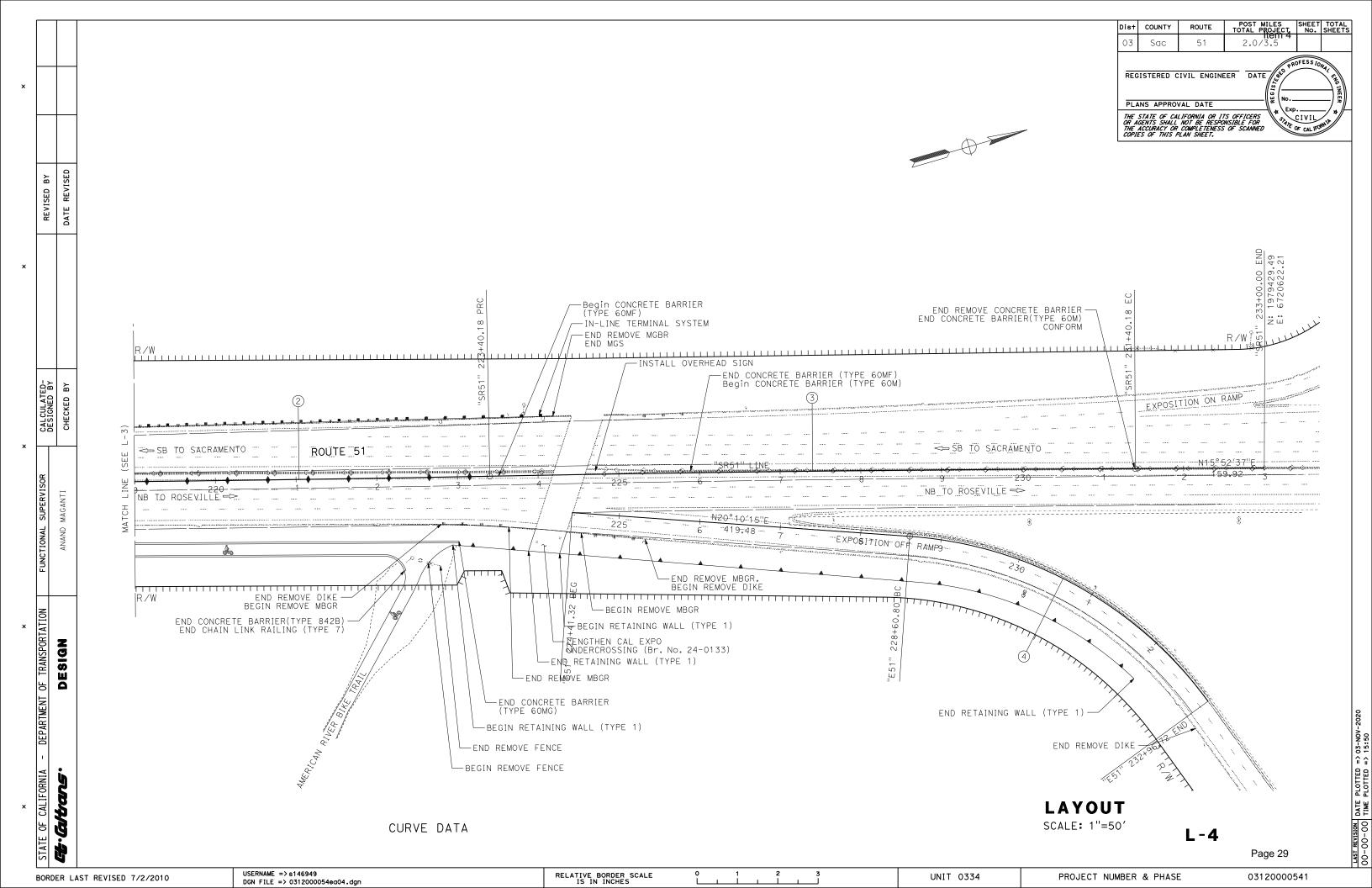
12/18/20 Page 24

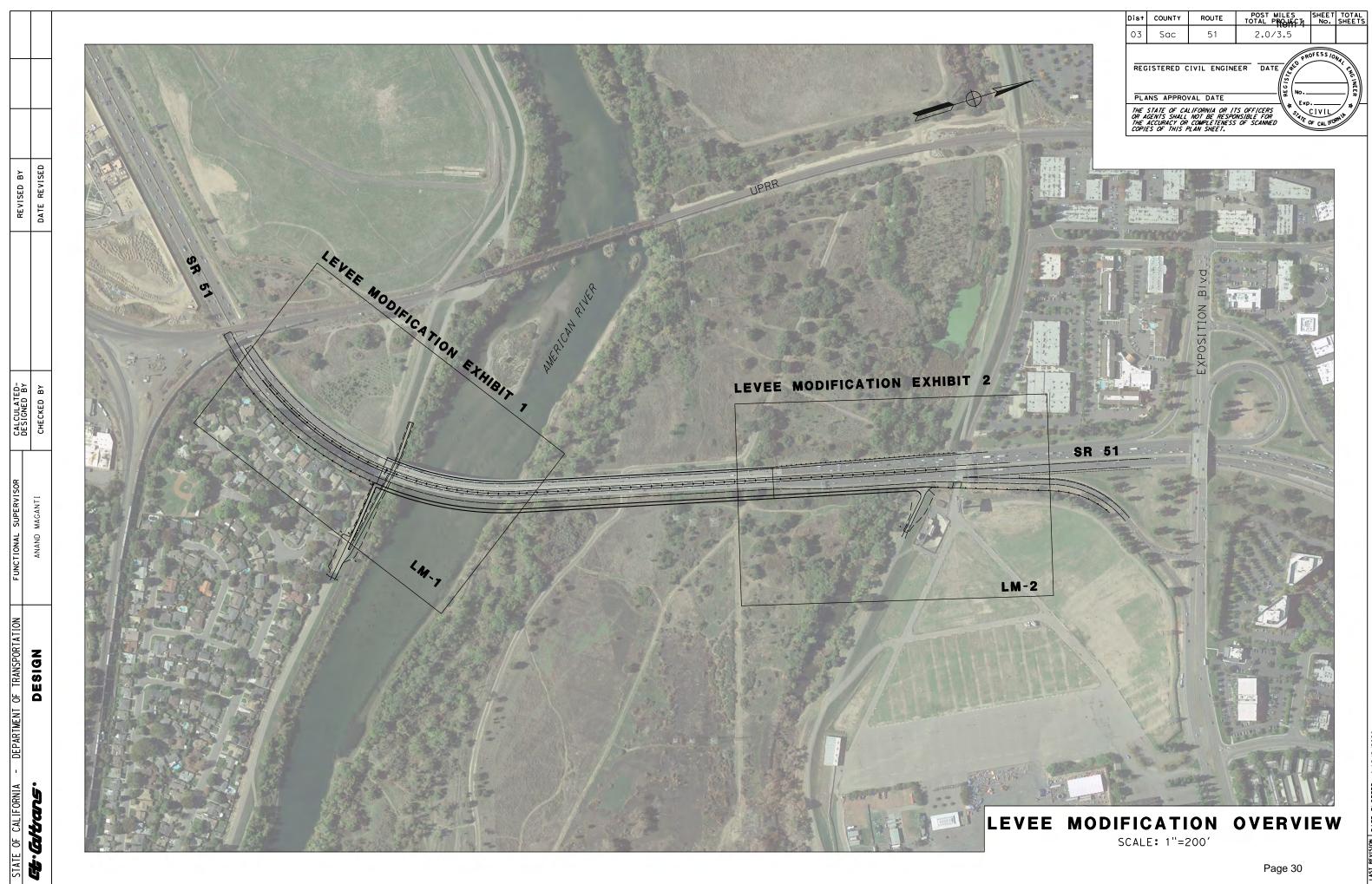




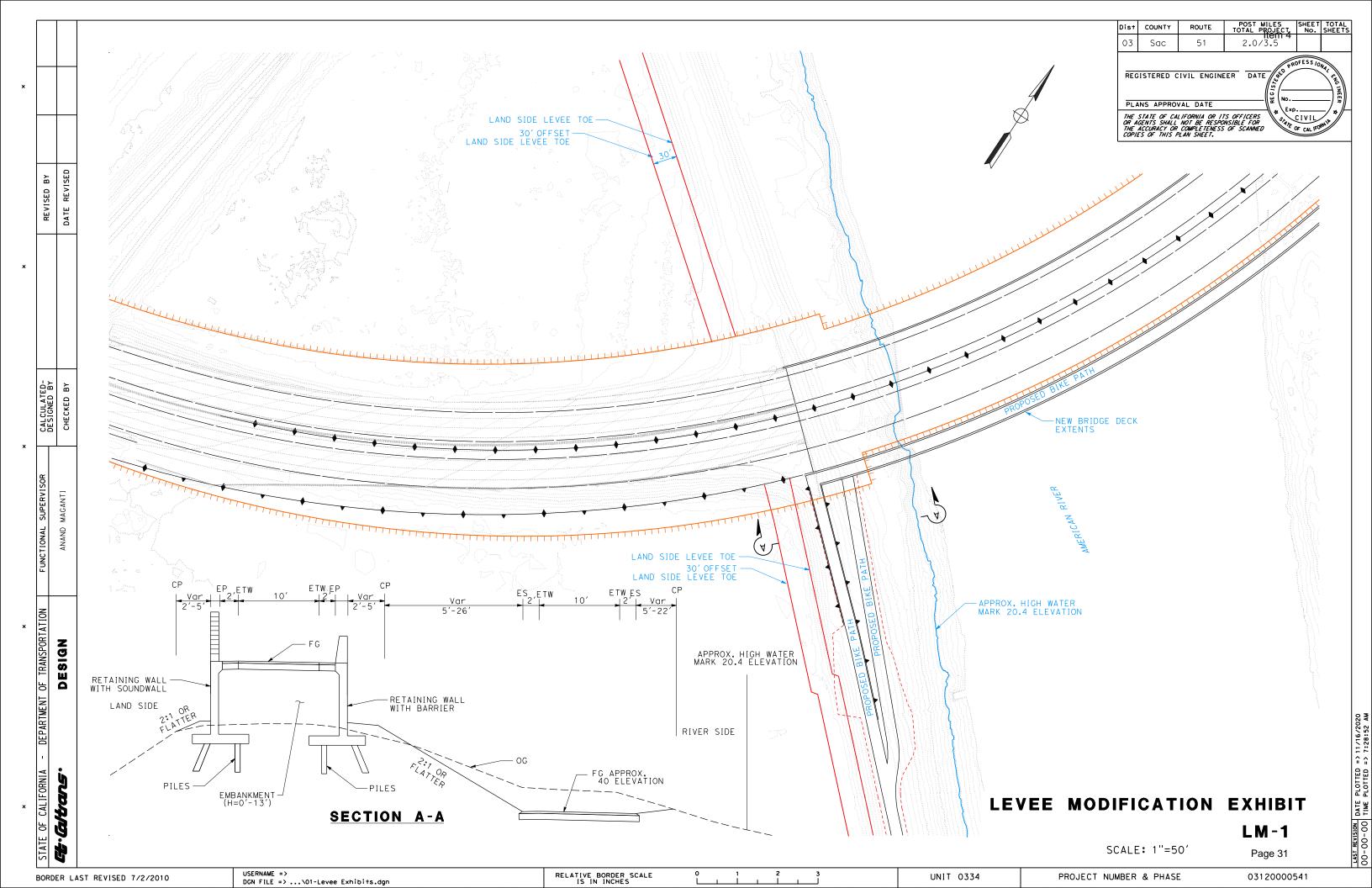


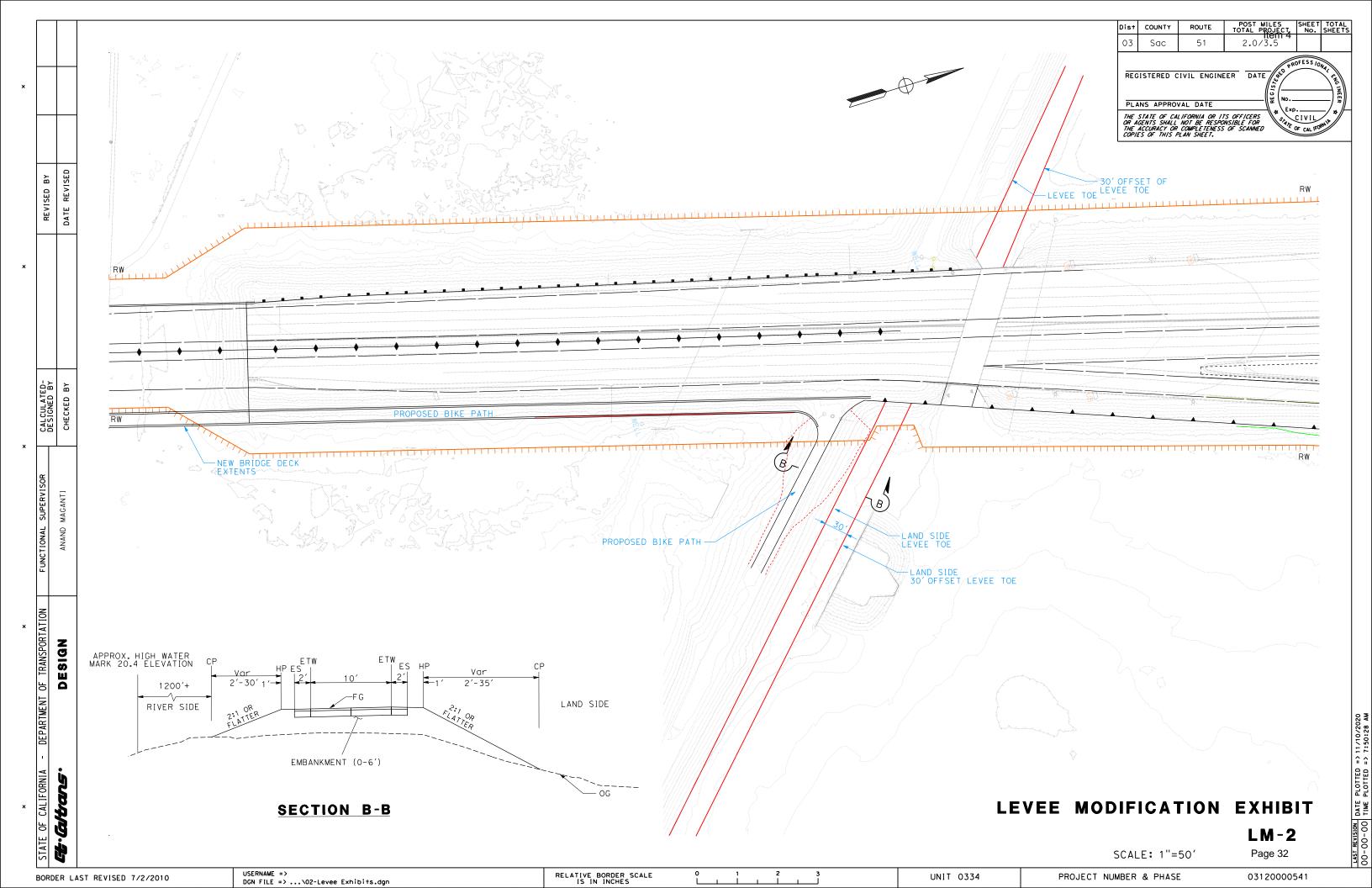


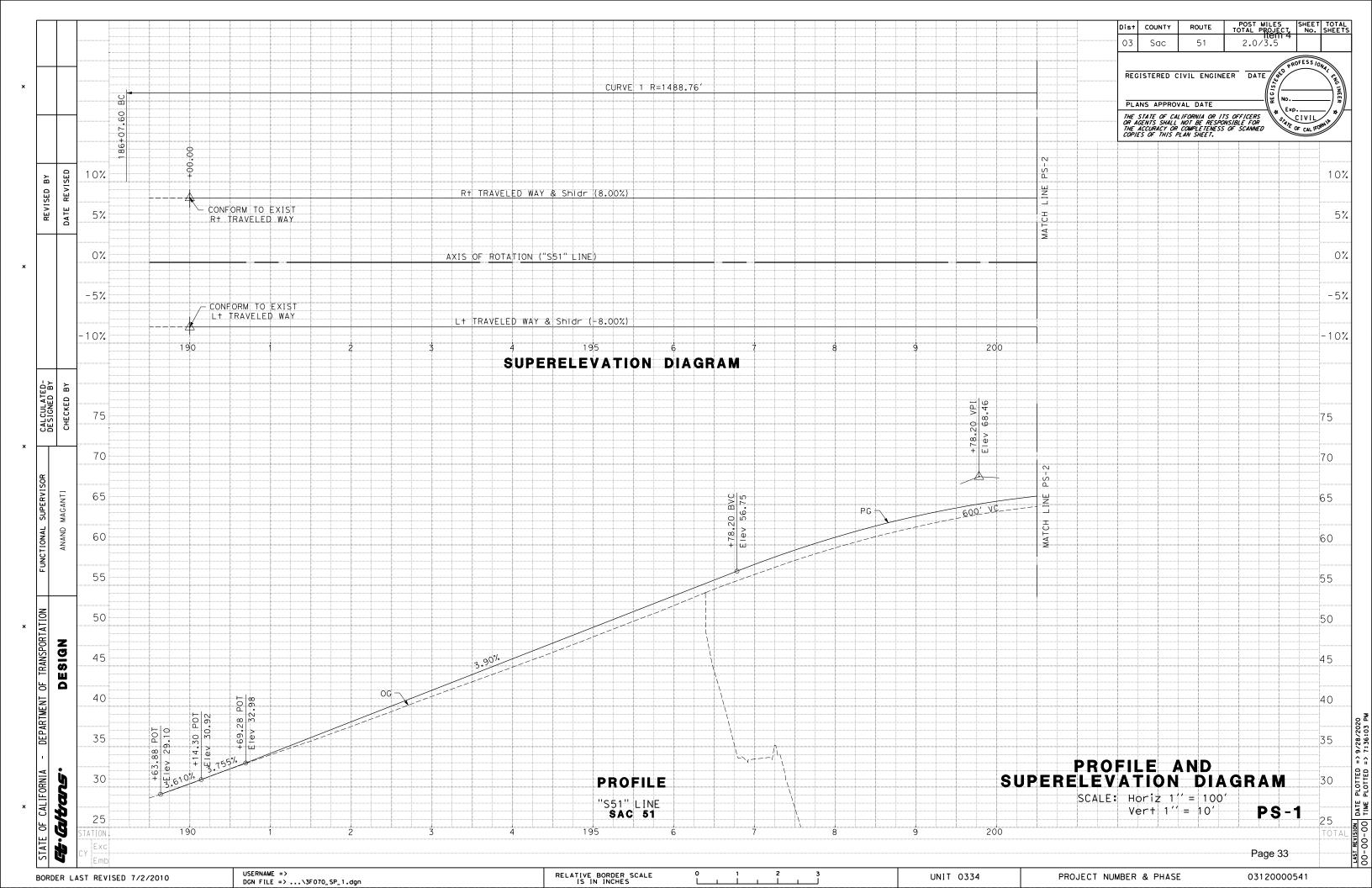


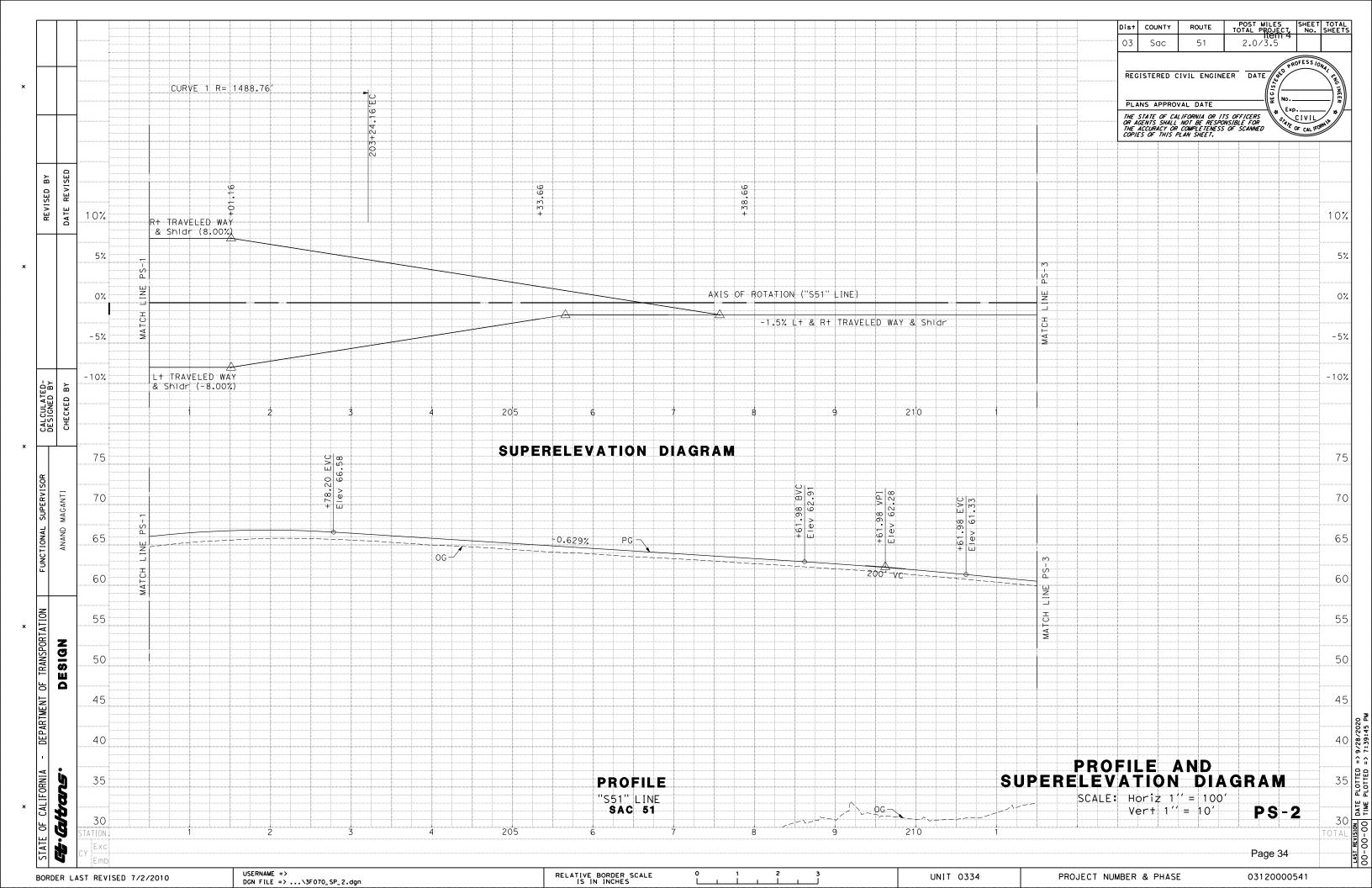


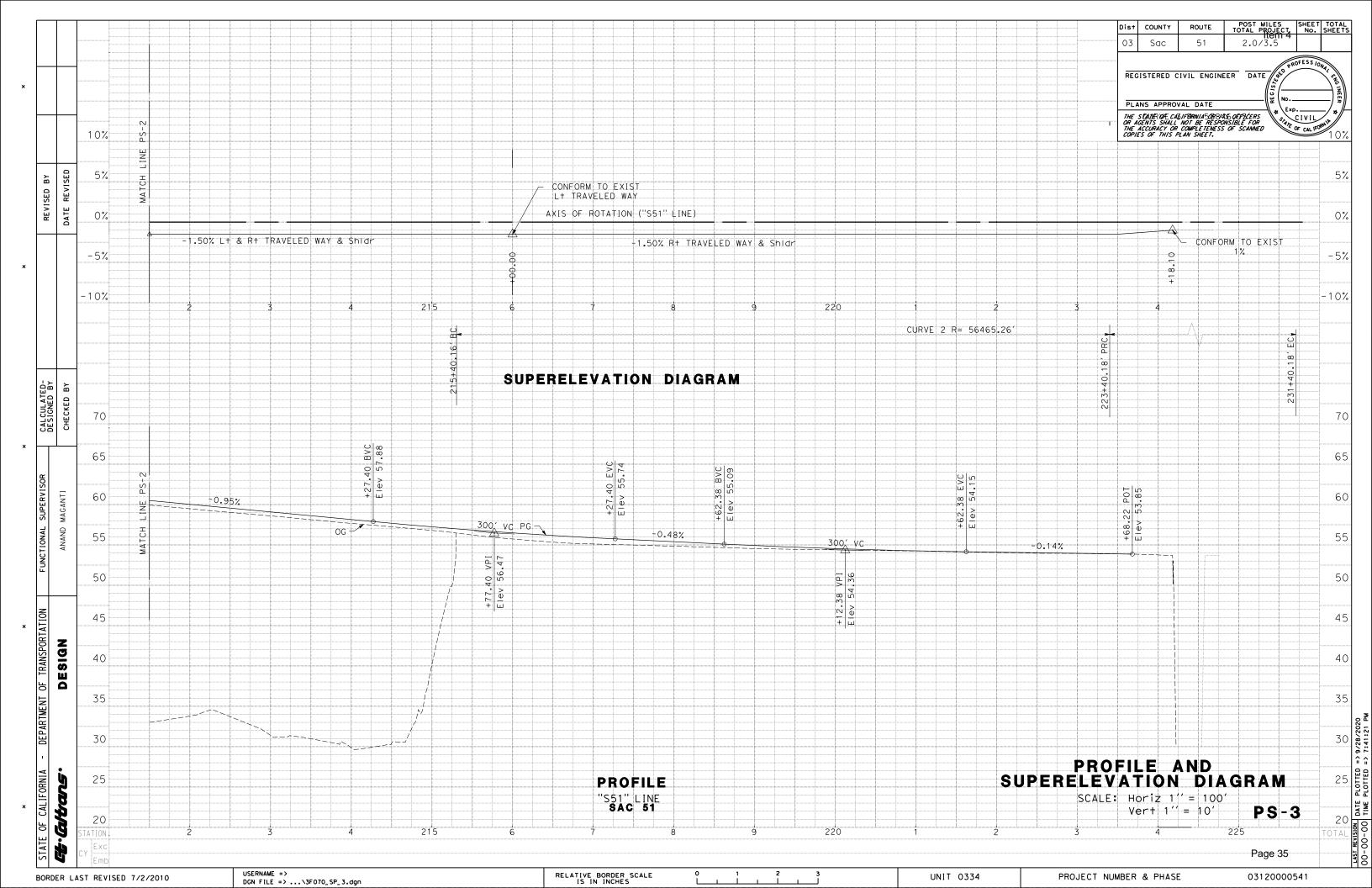
UNIT 0334 03120000541 PROJECT NUMBER & PHASE

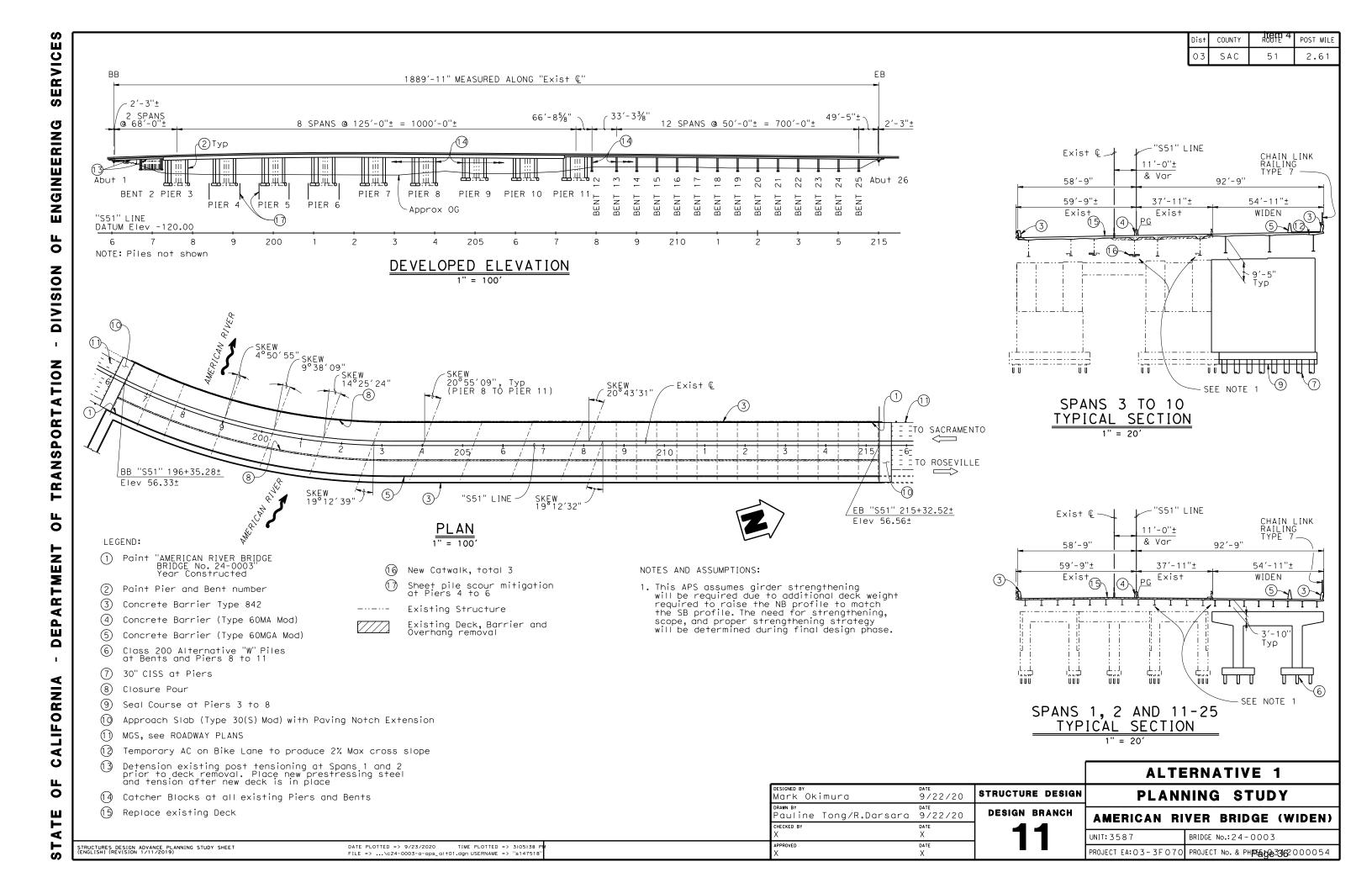


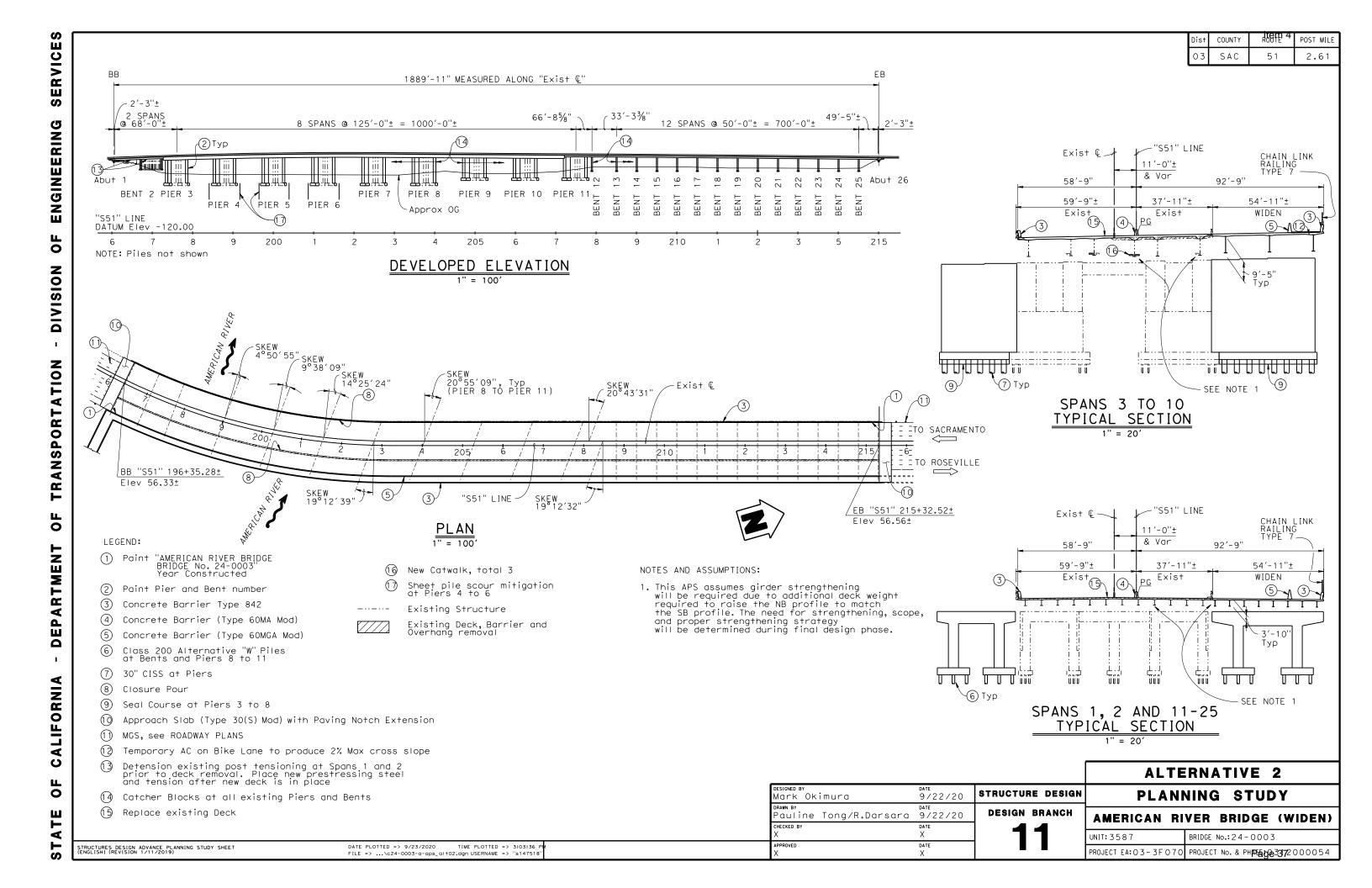


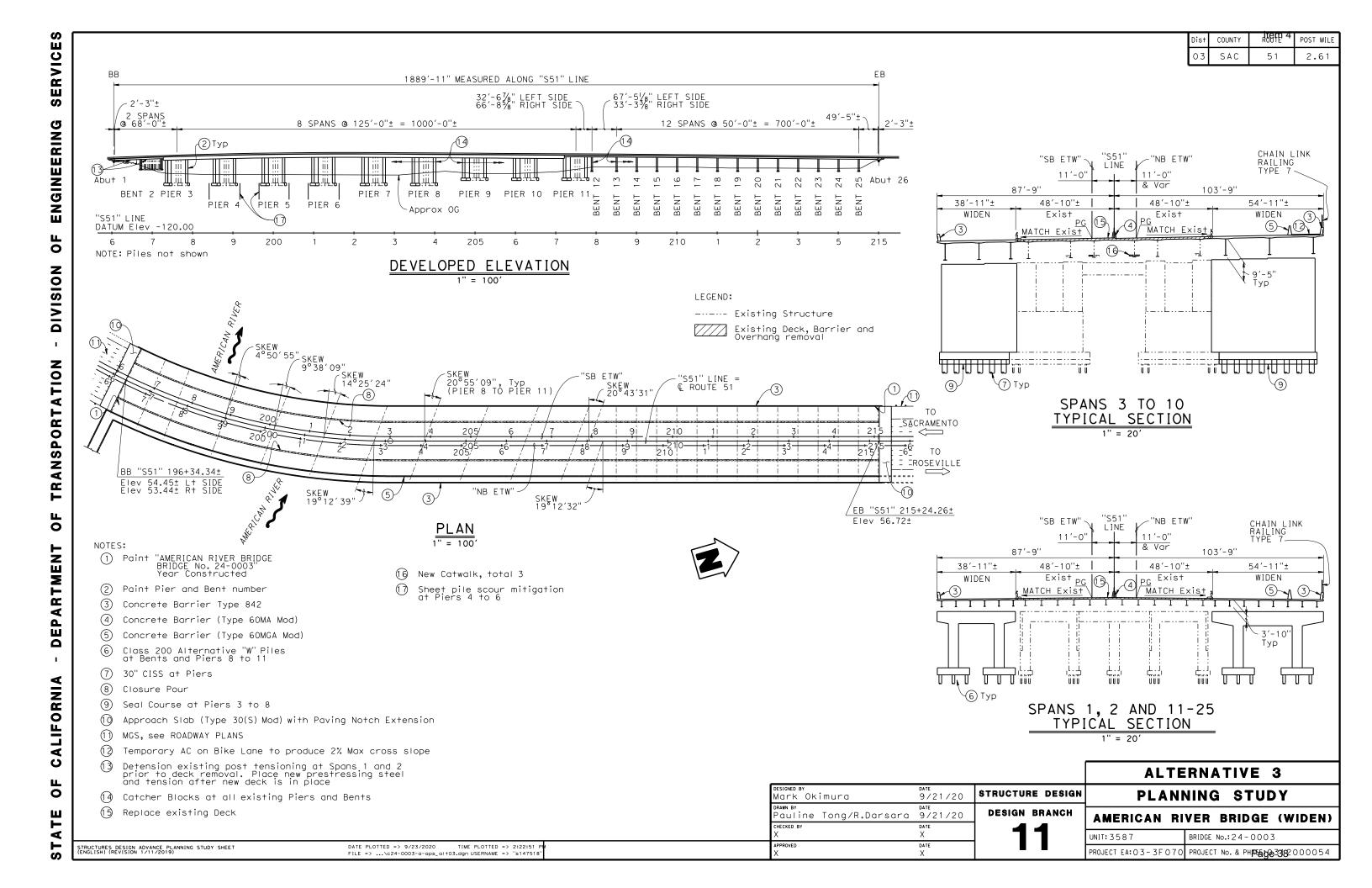












⋖

STRUCTURES DESIGN ADVANCE PLANNING STUDY SHEET (ENGLISH) (REVISION 3/17/2017)

39'-5<sup>1</sup>/<sub>4</sub>"±

Abut 2

<u>ELEVATION</u>
1" = 20'-0"

Approx OG=FG

225

"Exist Q"

N15°51′59"E

ORIGINAL SCALE IN INCHES

225

\EB Sta 224+57.53±

Elev =  $53.70 \pm$ 

TO ROSEVILLE

**①**, Typ

N18°26′23"E

F

Abut 1

224

 $\frac{BB \text{ S+a } 224+18.09\pm}{E \text{ Iev} = 53.76\pm}$ 

"SR51" LINE

# 22 # 25 # CONTINUE

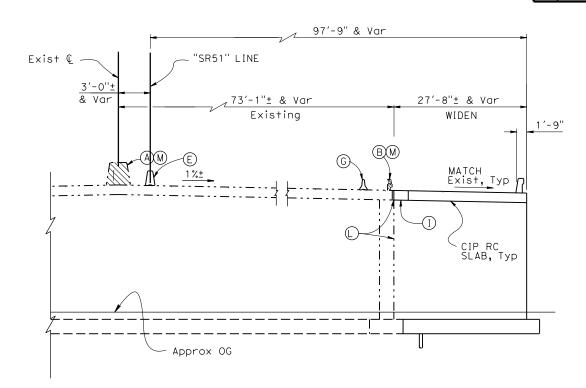
€ TRIBUTE Rd

=====

DATUM Elev 00.0

oist COUNTY ROUTE 4 POST MILE

3 Sac 51 3.14



NOTE:Not all piles shown

# $\frac{\text{TYPICAL SECTION}}{1" = 10'-0"}$

### LEGEND

- $\begin{tabular}{ll} \hline \end{tabular} A)$  Remove Exist conc barrier Type 60G modified for overhead sign support.
- B Remove Exist conc barrier Type 9.
- (C) Remove Exist barrier and wingwalls 3' min below FG
- D Remove Exist walls and footings as needed
- (E) Conc Barrier Type 60MA Mod
- (F) Concrete Barrier Type 836
- (G) Temporary Rail Type K
- (H) Retaining Wall, see "ROADWAY PLANS"
- (I) 3'-0" Closure Pour
- ① Piles, Class 90 Pipes. CIDH may be used to minimize impact to sewer lines in front of abutments.
- (K) Exist 30" RCP, Location approximate
- (L) Drill and Bond Dowel
- (M) Refinish Deck



Indicates Removal

lacksquare

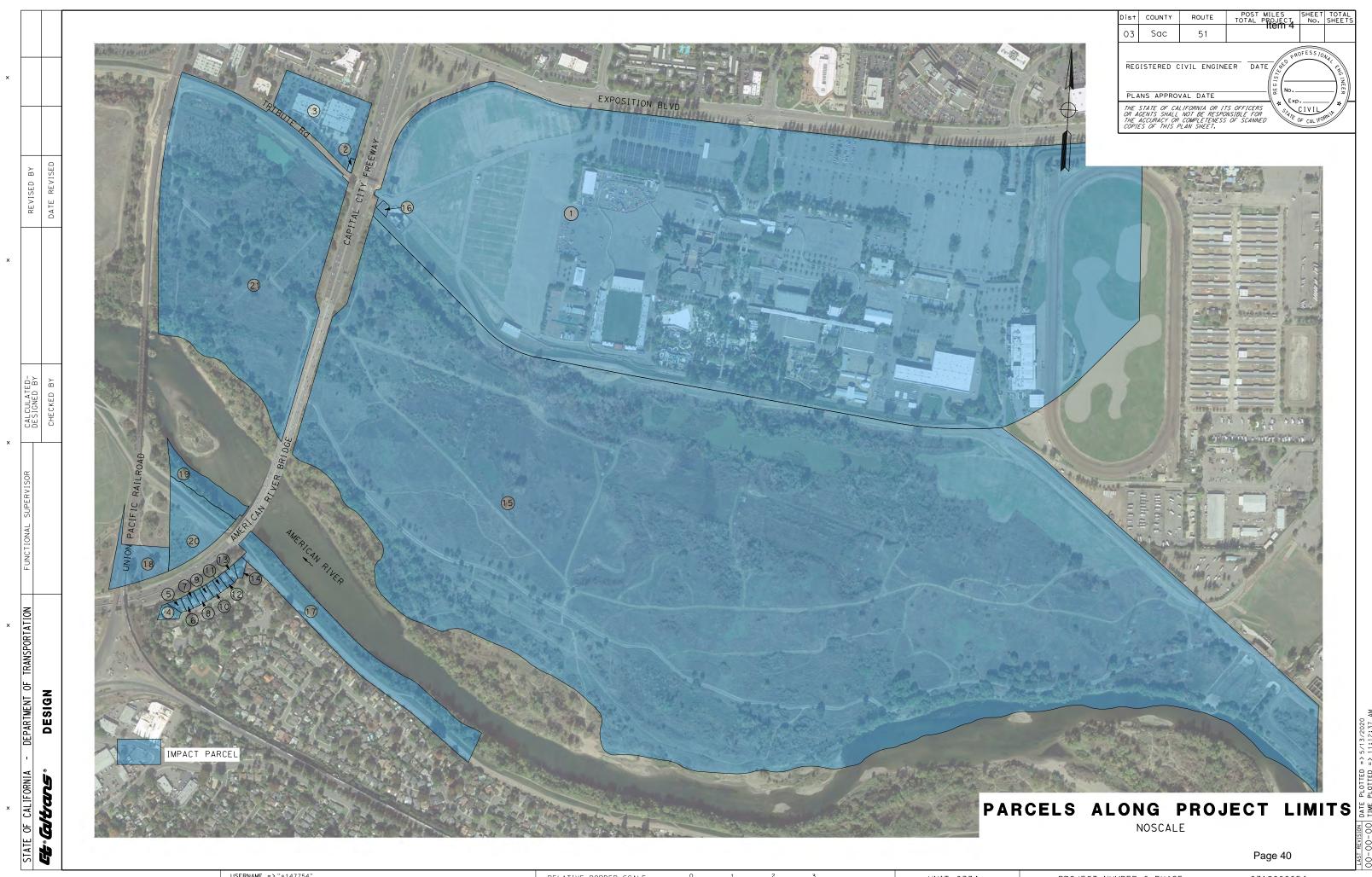
Indicates Point of Minimum Vertical Clearance

	DESIGNED BY Mark Okimura	DATE 9/25/20	STRUCTURE DESIGN
	DRAWN BY Loren Goldthwait	DATE 9/25/20	DESIGN BRANCH
	CHECKED BY	date X	11
3	APPROVED X	date X	

	AL	TERN	ATIV	E 1	<b>&amp; 2</b>	
1	P	LANN	IING	STUI	ΟY	
	CAL	EXPO	UC	WID	ENING	
	UNIT: 3587		BRIDGE No.:	24-133		

UNIT: 358 / BRIDGE NO.: 24 - 1 3 3

CONTRACT NO.: 03-3F070 PROJECT NO. & PHPAGE 3392 000054



BORDER LAST REVISED 7/2/2010

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RELATIVE BORDER SCALE 1 2 3 UNIT 0334

PROJECT NUMBER & PHASE 0312000054

No.	APN	OWNER NAME	OWNER_ ADDRESS	CITY, STATE	ZIPCODE
1	277-0250-018-0000	STATE OF CALIFORNIA	PO BOX 15649	SACRAMENTO, CA	95852
2	277-0285-002-0000	STATE OF CALIFORNIA	PO BOX 911	MARYSVILLE, CA	95901
3	277-0285-007-0000	UA 393 A HOLDINGS LLC	2450 CABRILLO HWY S STE 200	HALF MOON BAY, CA	94019
4	005-0251-028-0000	SUSAN C GORSUCH	3743 ERLEWINE CIR	SACRAMENTO, CA	95819
5	005-0251-027-0000	MARTIN J & JOAN M AROZ REVOCAB	3749 ERLEWINE CIR	SACRAMENTO, CA	95819
6	005-0251-026-0000	RUSSELL HOCKING	3751 ERLEWINE CIR	SACRAMENTO, CA	95819
7	005-0251-025-0000	BOBBY ELINOR OLWELL	3755 ERLEWINE CIR	SACRAMENTO, CA	95819
8	005-0251-024-0000	CARLA SUE DUCRAY	3759 ERLEWINE CIR	SACRAMENTO, CA	95819
9	005-0251-023-0000	JASON M BROWN	3763 ERLEWINE CIR	SACRAMENTO, CA	95819
10	005-0251-022-0000	ANTHONY F MORA	3767 ERLEWINE CIR	SACRAMENTO, CA	95819
11	005-0251-021-0000	CARMELA RAY	3771 ERLEWINE CIR	SACRAMENTO, CA	95819
12	005-0251-020-0000	MARK L STREGE	10086 CRISTO DR	SACRAMENTO, CA	95829
13	005-0251-019-0000	JEANNIE C LITTLE	3779 ERLEWINE CIR	SACRAMENTO, CA	95819
14	005-0251-018-0000	CHRISTINA ESPINOSA	4971 QUONSET DR	SACRAMENTO, CA	95820
15	277-0250-024-0000	STATE OF CALIFORNIA	PO BOX 15649	SACRAMENTO, CA	95852
16	277-0250-017-0000	SACRAMENTO REGIONAL COUNTY SAN	10060 GOETHE RD	SACRAMENTO, CA	95827
17	005-0010-026-0000	COUNTY OF SACRAMENTO	10361 ROCKINGHAM DR STE 100	SACRAMENTO, CA	95827
18	001-0170-029-0000	SOUTHERN PACIFIC TRANSPORTATIO	1400 DOUGLAS ST # 1640	OMAHA, NE	68179
19	001-0170-005-0000	COUNTY OF SACRAMENTO	10361 ROCKINGHAM DR STE 100	SACRAMENTO, CA	95827
20	001-0170-006-0000	CITY OF SACRAMENTO	915 I ST	SACRAMENTO, CA	95814
21	277-0250-019-0000	STATE OF CALIFORNIA	PO BOX 15649	SACRAMENTO, CA	95852

# PARCELS ALONG PROJECT LIMITS

NOSCALE

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REVISED BY

CALCULATED-DESIGNED BY

DEPARTMENT OF TRANSPORTATION

DESIGN

Page 41

STATE OF CALIFORNIA -RELATIVE BORDER SCALE IS IN INCHES UNIT 0334 PROJECT NUMBER & PHASE 0312000054 BORDER LAST REVISED 7/2/2010 DGN FILE => ...\Form Army\apn - TABLE.dgn

## Memorandum

Making Conservation a California Way of Life

To: MR. ANAND MAGANTI – D3

**Branch Chief** 

Office Design Branch M7

North Region Project Development

Date: February 20, 2020

File: 03-SAC-51-PM2.0/3.5

Project ID: 0312000054

EA: 03-3F070

AMERICAN RIVER BRIDGE #24-0003 (Widen and Deck Replacement)

Attention: Mr. Andrew Huang

From: DEPARTMENT OF TRANSPORTATION

Division of engineering services

Geotechnical Services

Office of Geotechnical Design - North

Design Branch D

Subject: DISTRICT PRELIMINARY GEOTECHNICAL REPORT FOR AMERICAN RIVER BRIDGE (WIDEN AND DECK REPLACEMENT)

#### Introduction

The Office of Geotechnical Design North has prepared a District Preliminary Geotechnical Report (DPGR) for the proposed American River Bridge (Widen and Deck Rehabilitation) project. In a request letter dated September 6, 2019, District North Region Division of Project Development, Office of Design B requested a DPGR for the proposed American River Bridge (Widen and Deck Rehabilitation). The following recommendations are based on the 2019 subsurface investigation performed at the site and the design information provided by the District Office.

With regards to the current geotechnical recommendations, all elevations referenced within this report and shown on the draft Log of Test Boring sheets are based on the NAVD 1988 vertical datum, unless otherwise noted.

#### **Project Description**

The American River Bridge (Widen and Deck Replacement) project proposes to add one travel lane at each side and a bike lane on the right side of the bridge. The district requested to provide a DPGR for four fill slopes and one overhead sign.

Anand Maganti February 20, 2020 033F070 03-SAC-51-PM -2.d<sup>1</sup>/<sub>2</sub>3.5 0312000054 Page 2 of 15

Based on the information provided, roadway improvements are proposed south of Abutment 1 and north of Abutment 26. The existing two post overhead sign-truss, located on northbound near STA 224+70, is planned to be replaced.

#### **Geotechnical Investigation**

A geotechnical investigation was conducted in 2019 for the Capital City Project in which included various bridges south and north of the American River Bridge (24-0003). Soil borings drilled within the project limits include five mud rotary borings (RW-19-020, RW-19-024, RW-19-025, RW-19-036, RW-19-037, RW-19-038 and RW-19-040) and one auger boring (A-19-042). Also, there is an existing soil boring from the Levee program from the Department of Water Resources, WCSBAR\_003B.

There is sufficient subsurface soil information available from the above mentioned soil investigation and **NO** additional soil borings are needed for this request. The Log of Test Borings (LOTBs) are being prepared during the preparation of this report.

#### **Geotechnical Conditions**

#### Geology

According to the Preliminary Geologic Map of the Sacramento Quadrangle, the materials that underlie the project site are mapped as Holocene aged alluvium deposits (Qha). Materials associated with alluvium typically consist of silt, clay, sand, gravels and cobbles deposited by river currents. North of Exposition Blvd (approximate) the project site is mapped as Holocene aged basin deposits (Qhb). Materials associated with basin deposits typically consist of fine-grained sediments with horizontal stratification deposited by standing or slow-moving water in topographic lows.

#### **Surface Conditions**

The existing highway within the project area generally trends north/south along a relatively flat valley floor. The elevation along the current alignment is approximately 55 feet. The elevation of native ground along the toe of the embankments are approximately 30 feet in elevation. The project site spans the American River which flows east-west. Within the project limits, local drainage is generally south towards the American River which flows west.

Anand Maganti February 20, 2020 033F070 03-SAC-51-PM -2.0<sup>1</sup>/<sub>2</sub>3.5 0312000054 Page 3 of 15

The American River Levees cross underneath the highway at about STA 196+00, on the south and STA 223+00, on the north.

South of Abutment 1, the north slope appears to have a 2H:1V grade or flatter. The south slope appeared to have 1H:1V grade, having a soundwall at the hinge. Vegetation consists mainly of weeds and grass. There are medium and large threes near toe of slope. There is a drain outlet at toe of each slope.

North of Abutment 26, the slopes appeared to be 1H:1V. Vegetation consists mainly of weeds and grass. There are few small and large size trees near toe of slope. There are light post fixtures along the southbound shoulder. There are few small trees near toe of slope.

On northbound, there is a One Post Overhead Sign-Truss (about STA 217+50) that it is planned to be removed. Further north, there is a two post Overhead sign-truss (about STA 224+70) that is planned to be replaced.

Based on our review our Office has identified an abandoned sewer line that possibly runs underneath parallel to the existing embankment, north of the project.

## **Subsurface Conditions**

Based on Soil Boring WCSBAR\_003B, Abutment 1 is supported on the American River levee. The levee fill consists of very stiff Fat Clay (CH) to elevation 44.0 feet overlaying a dense Silty Clayey Sand (SC-SM) to elevation 42.0 feet. Below the Silty Clayey Sand, Poorly-Graded medium dense Sand with Silt (SP-SM) extends to about elevation 33.0 feet. Then, medium dense Silty Sand (SM), Poorly-Graded Sand with Silt (SP-SM), Silty Clayey Sand (SC-SM) and Silty Sand extend to elevation 0.0 feet. Dense to very dense Well-Graded Gravel (extended to the maximum explored depth of elevation -18.0 feet.

The south and north embankment fills (about elevations 55.0 to 30.0 feet) consist mainly of medium dense to very dense Poorly-Graded Sand with Silt (SP-SM), Silty Sand (SM), Poorly-Graded Sand (SP), Poorly-Graded Sand with Clay (SP-SC) and Clayey Sand (SC).

Below the embankment fills, the subsurface soils predominately consist of alluvial deposits generally interbedded layers of gravels, sand, silty sand, sandy silts, silts, and clays. Alternating layers of loose to very dense Silty Sand (SM), Poorly-Graded Sand (SP) and Sandy Silt (ML) were encountered to about elevation -5.0 feet. Then, very dense Poorly-Graded Gravels were predominately encountered to about elevation -25.0 feet. Below the gravels, dense to very dense Poorly-Graded Sand (SP), Poorly-Graded Sand with Silt (SP-SM), Silt (ML) and Sandy Silt were

encountered to the maximum explored depth of elevation -144.0 feet. Bedrock was not encountered in any of the borings. The LOTBs are been drafted during the preparation of this report. Please referred to the attached draft boring records for more details.

### **Groundwater**

The 2019 subsurface investigation showed that groundwater is typically encountered at elevations between 14.0 to 11.0 feet. The American River surface water was at about elevation 10.0 feet. Groundwater elevations will fluctuate through the year due to variations in seasonal rainfall.

### **Geotechnical Design Evaluation**

#### Corrosion

Corrosion tests were conducted on soil samples taken from soil borings. Test results indicate the soil sample is considered **non-corrosive** by current Caltrans standards.

Location	SIC Number	рН	Minimum Resistivity (Ohm-cm)	Sulfate Content (ppm)	Chloride Content (ppm)
Water	CR20190498	5.98	30326	4	4
RW-19-026 85' -120'	CR20190493	7.26	1781	N/A	N/A
RW-19-029 35' - 60'	CR20190494	6.99	4196	N/A	N/A
RW-19-031 45' - 100'	CR20190495	7.03	4083	N/A	N/A
RW-19-034 0' - 30'	CR20190496	7.68	5655	N/A	N/A
RW-19-034 30' - 80'	CR20190497	7.15	5296	N/A	N/A

03-SAC-51-PM -2.073.5 0312000054 Page 5 of 15

#### **Preliminary Recommendations and Conclusions**

#### **Embankments (Fill Slopes)**

Based on our review, portions of this project will require widening existing fills. At the time of this report, no information was available from the District regarding the volume of fills to be constructed or slope ratio to be utilized for the proposed fill construction.

Based on our site reconnaissance, most of the existing fills throughout the project limits were noted to be 1H:1V. The Abutment 1 north slope appeared to be 2H:1V and flatter. The existing fills range in vertical height up to approximately 25ft. During our field reconnaissance, it did not appear that there were any slope instabilities on or below the existing fill areas reviewed. The new slopes are recommended to have a 2H:1V grade. All earthwork shall be in conformance with Section 19 of the 2018 Standard Specifications.

The proposed earthwork for the road widening may extend near Caltrans property line. If right of way is a constrain, Type 1 Retaining Wall or MSE wall may be considered.

### **Excavations**

Based on our review of provided layouts and proposed cross-sections, no excavation work is identified in the documents. However, it is anticipated that some excavation work will be required for the proposed widening and preparing the existing fills and native ground for fill placement. The excavations can be completed utilizing conventional earthwork equipment.

### Overhead Sign

The proposed foundation will be mainly embedded on the compacted granular dense to very dense embankment fills. Therefore, the proposed two post sign-truss may be supported by a standard plan foundation, presented on Sheets \$15 or \$116 of the 2018 Standard Plans.

03-SAC-51-PM -2.0 199.5 0312000054 Page 6 of 15

This DPGR is based on specific project information regarding proposed work and location that have been provided by the Office of North Region Division Project Development, Design Branch M7. Once the project plans are available, the Office of Geotechnical Design North, Design Branch D should review the information to determine if this DPGR is still applicable. Any questions regarding the above recommendations should be directed to the attention of Shawn Wei, (916) 227-1079 or Fernando De Haro, (916) 227-1069, at the Office of Geotechnical Design North, Branch D.

Prepared by:

Prepared by:

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Office of Geotechnical Design-North
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Reviewed by:

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cc: Clark Peri – District 3 (Project Manager)
Steve Culley – District 3 (District Materials Engineer)
Deline Hunter – Project Liaison
Ruth Fernandes – Structures Office Engineer
Geotechnical Archive

Attachment I Vicinity Map
Attachment II Draft Boring Records

Yusuf Zaka
Engineering Geologist
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Design-North
Design Branch DAL

MARK
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WILSON

No.8164

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Mark Wilson, P.G. Engineering Geologist Office of Geotechnical Design-North Design Branch D

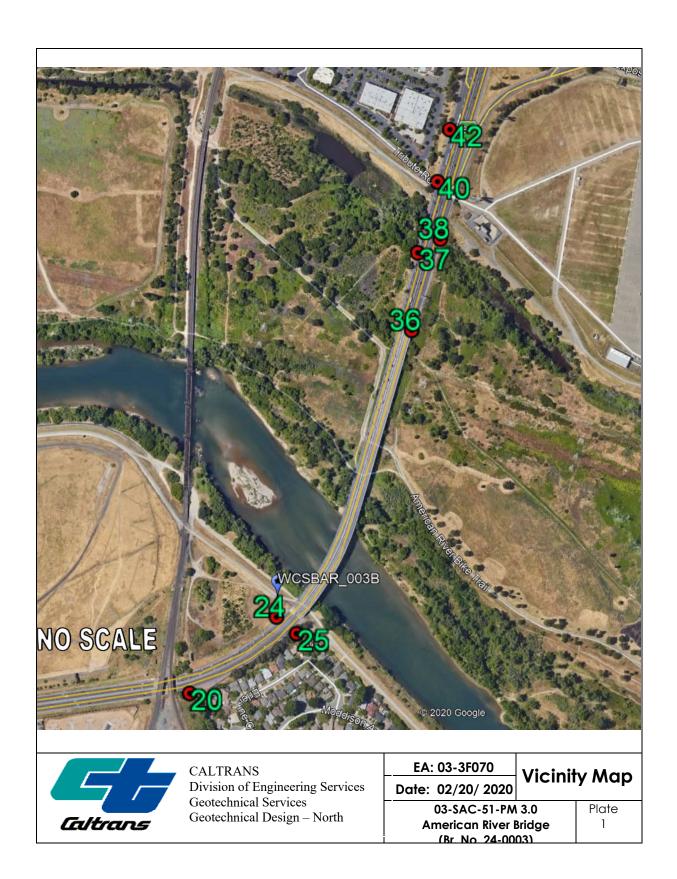
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Anand Maganti February 20, 2020 033F070

# Attachment I

**Vicinity Map** 



# **Attachment II**

# **Draft Boring Records**

OGGED BY BEGIN DATE COMPLETION DAT						g or N	orth/E	East a	nd Dat	um)		HOLE IC		
B. Rousseau 3-26-19 3-28-19 PRILLING CONTRACTOR	<b>38.5853</b> BOREHOL					Station	n, Lin	e)					<b>19-020</b> CE ELEVATIO	N
Gregg Drilling  DRILLING METHOD	DRILL RIG	i											ft NAVD88	
Mud Rotary	MARL	/110 X										4.63 i	n	
SAMPLER TYPE(S) AND SIZE(S) (ID) SPT (1.4")/CAL (2.5")/Punch Core (2.5")	SPT HAMM			nch	dro	р						87%	R EFFICIENC	Y, ERi
OREHOLE BACKFILL AND COMPLETION  Neat cement grout	GROUND\ READINGS			ING I			AF	TER	DRILLI	NG (E	DATE)	TOTAL <b>161.5</b>	DEPTH OF BO	ORING
DEPTH (ft) Material Graphics NOITHIES		Sample Location Sample Number	Blows per 6 in.	Blows per foot	Recovery (%)	RQD (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Shear Strength (tsf)	Drilling Method	casing Depin		Remarks	
0.00 SILTY SAND (SM); yellow; moist; fine SAN non-plastic.	D; some fines;									A		d Auger t	o 5 feet	
										X				
										M				
5 SANDY SILT (ML); loose; olive brown; mois	st; some fine	801	2 2 3	5	66						Swi WA	tch to Mud	d Rotary	
			3		24					100				
		C02												
10 SILTY SAND (SM); medium dense; brown;	wet; fine	803	4 5 5	10	66					100	WA			
SAND; some fines; non-plastic.		\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	5	╀	19					100				
		C05								000				
15 SILT with Sand (ML); brown; moist; little fin	e SAND	/ <sub>(0</sub>	2	6	100					100	WA			
3.00		806	2 3 3	<del> </del>	28					100				
bluish gray; wet.		C07												
20			2	7	100						WA			
0.00 SANDY SILT (ML)/SILTY SAND (SM); med bluish gray; fine SAND; non-plastic.	num dense,	808	2 2 5	<u>,                                    </u>	NR					200	***			
		600			INIX					000				
25														
5.00 SILTY SAND (SM); medium dense; bluish medium to fine SAND; some fines; non-plas	gray; moist; stic.	\$30	5 5 5	10						100	WA			
laminated organic matter.		_			28					000				
		57								20				
0.00 POORLY GRADED SAND with Silt (SP-SN dense; bluish gray; moist; medium to fine S		S12	7 11 9	20	77						WA			
POORLY GRADED GRAVEL (GP).			9_	$\lceil$	NR					200				
		C13								200	Rig	chatter		
35 35 very dense.		S14	16 15	37	NR					100				
		\ \sigma \omega	15 22	+	NR						Rig	chatter		
		C15								3000				
(continued)														
(comment)			REPOR			COP	D.					HOLE IC	-19-020	
		-	DIST.	CC	UNT			R0	DUTE		STMII .05-2	.E	EA 03-1600	)-0113.
KLEINFELDER										1 1				

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BRIDGE NUMBER 83 C-57 SR51 PREPARED BY D. Ross DATE SHEET 7-15-19 51 1 of 4

													T
ELEVATION (ft)	р ОЕРТН (ft)	Material Graphics	DESCRIPTION	Sample Location Sample Number	Blows per 6 in.	Blows per foot	Recovery (%)	RQD (%)	Moisture Content (%)	(pcf)	(tsf)	Drilling Method Casing Depth	Remarks
-10.00	40	0000	POORLY GRADED GRAVEL (GP); dense.	S16	8 11 12	23	NR					000	
		0000000		C17			NR					00000	Rig chatter
-15.00	45	0000	POORLY GRADED GRAVEL with Silt and Sand (GP-GM); very dense; gray; moist; fine to coarse GRAVEL, 1.5 in. max. dia.; some medium to fine SAND;	S18	26 50 50	100	33					000	PA
		000000	GRAVEL, 1.5 in. max. dia.; some medium to fine SAND; few fines; non-plastic.	C19	30		NR					<u> </u>	Rig chatter
-20.00	50		7 inch thick lens of SANDY SILT (ML).	S20	20 33 32	65	39					000	WA
					32		NR					000	Rig chatter
	55 -	0000		C21								000	
-25.00		00000		822	30 38 50	88	NR NR					000	Light rig chatter
	-			C23								000000000000000000000000000000000000000	
-30.00	60	- (A)	POORLY GRADED SAND (SP); very dense; light gray; moist; fine SAND.	S24	7 38 50	88	100			>		3000	
	-	- - - -		C25	00		NR					000000	
-35.00	65 -		LEAN CLAY (CL); mottled olive and yellow; moist; trace fine SAND; medium plasticity.	826	11 21 24	45	66 NR				——/>	$\sim$	
	-			C27								00000000000	
-40.00	70		olive; few fine SAND.	828	13 18 26	44	100				}	0000	
				C29			NR					000000	
-45.00	75			830	21 30 36	66	72				}	00	
	-			C31	00		NR					000000	
-50.00	80		SILTY SAND (SM); very dense; multicolored red and olive; moist; fine SAND; little fines; low plasticity.	S32	22 50/5"	50/5	100					000	
			POORLY GRADED SAND (SP); olive; medium to fine SAND.	C33								000000000000000000000000000000000000000	Light rig chatter
-55.00	85		SANDY LEAN CLAY (CL); hard; yellowish brown; moist; some fine SAND; medium plasticity.	S34	13 21 21	42	100			PP		00000	
		1.7.7	(continued)	C35								0	
					REPOR BOR	NG	REC		D				HOLE ID <b>RW-19-020</b>
(	K	(LE	INFELDER		DIST. <b>03</b> PROJE	S		ame		ROU <b>51</b> Æ	TE		ETMILE EA 03-1600-0113-0
			Bright People. Right Solutions.		Caltr	ans	TOS	461	83 C- PREF			ac	DATE SHEET <b>7-15-19</b> 50 <b>2 of 4</b>

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-90.00 120 -90.00 120 -90.00 120 -90.00 120 -90.00 125																	2022
## SANDY LEAN CLAY (CL); red; moist fine SAND; medium plasticity.  ## POORLY GRADED SAND (SP); dense; yellowish brown; moist, fine SAND.  ## POORLY GRADED SAND with Sitt (SP-SM); olive gray;  ## POORLY GRADED SAND with Sitt (SP-SM); olive gray;  ## POORLY GRADED SAND with Sitt (SP-SM); very dense; olive gray;  ## POORLY GRADED SAND with Sitt (SP-SM); very dense; olive gray;  ## POORLY GRADED SAND with Sitt (SP-SM); very dense; olive gray;  ## POORLY GRADED SAND with Sitt (SP-SM); very dense; olive gray;  ## POORLY GRADED SAND with Sitt (SP-SM); very dense; olive gray;  ## POORLY GRADED SAND with Sitt (SP-SM); very dense; olive gray;  ## POORLY GRADED SAND with Sitt (SP-SM); very dense; olive gray;  ## POORLY GRADED SAND with Sitt (SP-SM); very dense; olive gray;  ## POORLY GRADED SAND with Sitt (SP-SM); very dense; olive gray;  ## POORLY GRADED SAND with Sitt (SP-SM); very dense; olive gray; moist, fine SAND; non-plastic.  ## POORLY GRADED SAND with Sitt (SP-SM); very dense; olive gray; moist, fine SAND; one plastic.  ## POORLY GRADED SAND with Sitt (SP-SM); very dense; olive gray; moist, fine SAND; one plastic.  ## POORLY GRADED SAND with Sitt (SP-SM); olive gray;  ## POORLY GRADED SAND with Sitt (SP-SM); olive gray;  ## POORLY GRADED SAND with Sitt (SP-SM); olive gray;  ## POORLY GRADED SAND with Sitt (SP-SM); olive gray;  ## POORLY GRADED SAND with Sitt (SP-SM); olive gray;  ## POORLY GRADED SAND with Sitt (SP-SM); olive gray;  ## POORLY GRADED SAND with Sitt (SP-SM); olive gray;  ## POORLY GRADED SAND with Sitt (SP-SM); olive gray;  ## POORLY GRADED SAND with Sitt (SP-SM); olive gray;  ## POORLY GRADED SAND with Sitt (SP-SM); olive gray;  ## POORLY GRADED SAND with Sitt (SP-SM); olive gray;  ## POORLY GRADED SAND with Sitt (SP-SM); olive gray;  ## POORLY GRADED SAND with Sitt (SP-SM); olive gray;  ## POORLY GRADED SAND with Sitt (SP-SM); olive gray;  ## POORLY GRADED SAND with Sitt (SP-SM); olive gray;  ## POORLY GRADED SAND with Sitt (SP-SM); olive gray;  ## POORLY GRADED SAND with Sitt (SP-SM); olive gray	s	Rema		Casing Depth	(tst) Drilling Method	Shear Strength (tsf)	Dry Unit Weight (pcf)	Moisture Content (%)	RQD (%)	Recovery (%)	Blows per foot	Blows per 6 in.	Sample Number	acitoo Lolamo	DEPTH (ft) Material Graphics Craphics	ELEVATION (ft)	2019 U7:U7 AM DT. D
SANDY LEAN CLAY (CL); rest, moist, fine SAND, medium   SAND   S				5	$\sim$					100			35	ND;	CLAYEY SAND (SC); yellowish brown; moist; fine SAND; some fines.		8/21/2
SANDY LEAN CLAY (CL); rest, moist, fine SAND, medium   SAND   S				0000							50	25 22 28		y;	90 POORLY GRADED SAND (SP); very dense; olive gray; moist; medium to fine SAND.		-6
-70.00  -70.00	-			0000	XXXXX					100	52	15		ium .	/ / plasticity		
100   100					$\sim$						J2	12 40		wn;	POORLY GRADED SAND (SP); dense; vellowish brown;	5.00	-6
100   SANDY LEAN CLAY (CL.); hard; clive; moist; some fine   SAND; modium plasicity.   SAND; modium plasicity.   POCRLY GRADED SAND with Silt (SP-SM); clive gray; moist; fine SAND.   SILTY SAND (SM); very dense; vellowish brown; moist; fine SAND; some fines; non-plasic.   SILTY SAND (SM); very dense; vellowish brown; moist; fine SAND; some fines; non-plasic.   SILTY SAND (SM); very dense; vellowish brown; moist; fine SAND; some fines; non-plasic.   SAND; little fines; non-plasic.   SAND; non-plasic.   S	-			0000	XXXX					89	57	21					
SANDY LEAN CLAY (CL); hard; olive; moist; some fine SAND; medium plasticity.   SAND; medium plasticity.   SAND; medium plasticity.   SAND; medium plasticity.   SAND; most; fine SAND; olive gray;   SAND; some fines; non-plastic.   SAND; some fines; non-plastic.   SAND; moist; fine SAND; SAND;				0000						NR		32					
POORLY GRAND SAND with Silt (SP-SM); olive gray.   100   25   26   26   26   26   26   26   26				0000	4.0	PP=4.0				100	57	10 20		e	/ / CAND, madium planticity		-7
Section   110   Silty Sand (SM); very dense; yellowish brown; moist;   Silty Sand (SM); very dense; yellowish brown; moist;   Silty Sand (SM); very dense; yellowish brown; moist;   Silty Sand (SM); very dense;   Silty Sand (SM);				0000	XXXX					100		_ 31		ıy;	POORLY GRADED SAND with Silt (SP-SM); olive gray; moist; fine SAND.		
SILTY SAND (SM); very dense; yellowish brown; moist;   Silty SAND; some fines; non-plastic.   Silty SAND; some fines; non-plastic.   POORLY GRADED SAND; wery dense; olive gray; moist; fine SAND; non-plastic.   Silty SAND; moist; fine SAND; non-plastic.   Silty SAND; mon-plastic.   Silty SAND; mon-plastic.   Silty SAND; mon-plastic.   Silty SAND; ittle fines; non-plastic.   Silty SAND; ittle fines; non-plastic.   Silty SAND; mon-plastic.   Silty SA	-			0000	XXX							15 22 28	S44		0.00		-8
BS.00 115   SILTY SAND (SM); very dense; yellowish brown; moist; fine SAND; some fines; non-plastic.   Q				0000	(XXXX)					100			C45		Olive.		
-90.00 120   -90.00   SILTY SAND (SM); very dense; olive gray; moist; fine SAND; little fines; non-plastic.   -95.00   125   -95.00   125   -95.00   125   -95.00   125   -95.00   125   -95.00   130   SILTY (ML); hard; bluish gray; moist; few fine SAND; low plasticity.   SILT (ML); hard; bluish gray; moist; few fine SAND; low plasticity.   SILT (ML); hard; bluish gray; moist; few fine SAND; low plasticity.   -95.00   100				$\supset$	-							12 19 25	S46	t;	115   SILTY SAND (SM); very dense; yellowish brown; moist; fine SAND; some fines; non-plastic.		3- K
LEAN CLAY with Sand (CL); hard; yellow; moist; little fine SAND; medium plasticity.  SILT (ML); hard; bluish gray; moist; few fine SAND; low plasticity.  PP=>4.5  PP=>4.5  PP=>4.5  PP=>4.5  PP=>4.5  PP=>4.5  REPORT TITLE  BORING RECORD  PP=>4.5				0	$\gtrsim$								C47	ise;	olive gray: moist: fine SAND: non-plastic		⊼ Ε Σ Σ
LEAN CLAY with Sand (CL); hard; yellow; moist; little fine SAND; medium plasticity.  SILT (ML); hard; bluish gray; moist; few fine SAND; low plasticity.  PP=>4.5  PP=>4.5  PP=>4.5  PP=>4.5  PP=>4.5  PP=>4.5  REPORT TITLE  BORING RECORD  PP=>4.5	-			) )							40	18 19 21			0.00		2 -8
LEAN CLAY with Sand (CL); hard; yellow; moist; little fine SAND; medium plasticity.  SILT (ML); hard; bluish gray; moist; few fine SAND; low plasticity.  PP=>4.5  PP=>4.5  PP=>4.5  PP=>4.5  PP=>4.5  PP=>4.5  REPORT TITLE  BORING RECORD  PP=>4.5	-			$\supset$	$-\!$					66	92	24			125 — ( ) ; ; ;		-CALIRAI
	-			0		DD-: 1						42 50				5.00	
	-			00000	$\mathcal{L}$					100	31	10			SAND; medium plasticity.  130 SILT (ML); hard; bluish gray; moist; few fine SAND; low		Y_2017.51
				0 0 0						100		12 19		low;	POORLY GRADED SAND with Silt (SP-SM); olive yellow.	.0.00	רואיזפוט_וו
				0	$\gtrsim$					100	52				135		NDAKU_G
		HOLEID	<del> </del>							F1 F	T T1-		15		(continued)		<u>-</u>
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ELEVATION (ft)	DЕРТН (ft)	Material Graphics	DESCRIPTION	Sample Location Sample Number	Blows per 6 in.	Blows per foot	Recovery (%)	RQD (%)	Aoisture Sontent (%)	Dry Unit Weight (pcf)	Shear Strength (tsf)	Drilling Method Casing Depth	Remarks
	Ī	20	SILTY SAND (SM); very dense; yellow; moist; fine SAND; some fines; non-plastic.		19 20 32		57	-	20		0, 5	<sub>1</sub> /	
	140		POORLY GRADED SAND with Silt (SP-SM); very dense; olive yellow; moist; medium to fine SAND; non-plastic.	C55								<u> </u>	
-110.00	_		3 inch thick lens of SILTY SAND (SM).	S56	22 36 41	77	77 64					0000	
				C57								DODDO	
-115.00	145		olive gray.	S58	15 28 33	61	77					0000	
				C59			9					0000	
-120.00	150			Se0	25 32 39	71	77					0000	
				C61	39		24					0000	
-125.00	155			S62 C	23 28 35	63	66					<u>orbonondonbonnonbonnondon</u>	
120.00					35							3000	
	160		LEAN CLAY with Sand (CL); yellow; moist; fine SAND; medium plasticity; calcite veins.	C63	24	92						2000	
-130.00			Bottom of borehole at 161.5 ft bgs Borehole was terminated at proposed depth. Borehole was backfilled with neat cement grout via tremie pipe and topped with native soil.	₩ 88	24 42 50							0	
	165		Borehole was backfilled with neat cement grout via tremie pipe and topped with native soil.										
-135.00													
	170												
-140.00	170												
-145.00	175												
	L	1											
-150.00	180												
-150.00	180												
-150.00	180			F	REPOR	RT TI	TLE						HOLE ID
-150.00					BOR	NG CO	REC	Υ			OUTE	POS	HOLE ID <b>RW-19-020</b> STMILE EA 03-1600-0113
-150.00			EINFELDER Bright People. Right Solutions.	C F	BORI DIST. 03 PROJE	CT C	REC OUNT Cacra OR BI	Y <b>ame</b> RIDG	ento SE NA	5 AME		1.0	HOLE ID <b>RW-19-020</b> STMILE EA 03-1600-0113

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Greg	g D	rilli	ing	ACTOR			REHOLE	ELO	CAT	ΓΙΟΝ	(Offs	et, S	tatio	n, Line	e)				45.50	ft NAVI	<b>088</b>
ORILLII <b>Holl</b> o				O Nuger/Mud Rotary		<b>I</b>	ILL RIG <b>obile E</b>	3-80											1	OLE DIAN <b>/4.63 in</b>	METER
SAMPL	ER 1	ГҮР	E(S	) AND SIZE(S) (ID) ach Core (2.5")			T HAMM uto; 14				ach	dro	n						95.5%		ENCY, ERI
BOREH	HOLE	B/	\CK	FILL AND COMPLETIO	DN	GR	OUNDW ADINGS	/ATE			NG [			AF	TER	DRILLI	NG (E	DATE	TOTAL	DEPTH C	F BORING
Neat	cen	ner	nt g	rout		1,42	1011100		ī.	21.5	π.				±				42.51	τ	
ELEVATION (ft)	ОЕРТН (#)	A 4 - 4 - 12 - 1	Matenal Graphics	ı	DESCRIPTION			Sample Location	Sample Number	Blows per 6 in.	Blows per foot	Recovery (%)	RQD (%)	Moisture Content (%)	Dry Unit Weigh (pcf)	Shear Strength (tsf)	Drilling Method	Casing Deptn		Remarks	
45.00	0			SILTY SAND (SM); b non-plastic.	rown; moist; fine SA	AND; some	fines;												low Stem	Auger to	10 feet
		-																			
40.00	5	<b>–</b>	200	POORLY GRADED ( subrounded to round	GRAVEL (SP); mois ed GRAVEL; few fin	t; fine to co ne SAND.	arse			5	11	33									
40.00	•	-		POORLY GRADED S moist; fine SAND.	SAND (SP); medium	n dense; br	own;	3	00	5 5 6	<u> </u>										
		-[:																			
35.00	10			SILTY SAND (SM); m SAND; little fines; nor	nedium dense; brow	n; moist; fi	ne	X	7	6 4 3	7	44						Sw	tch to Mu	d Rotary	
				no GRAVEL.	n-piasuc; iew iine, ro	ounaea GR	KAVEL.	/\ 0	กั	3_		89					100				
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25.00		4		wet; some fines.				X g	2	2 5 8	13	100									
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20.00	25	_							١								000				
		_		very loose.				\\	200	1 0 3	3	100									
		-		SILT (ML); soft; reddi	ish brown; wet; few f	fine SAND.						100				PP=0.2	$_{\rm I}$				
	30			POORLY GRADED S		own; wet;		Š	3								200				
15.00							t·			6	17	100									
		-		medium to fine SAND		2.0,	•,	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	2	8 9		14									
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	35	ŀ	·]· ·		(continued)												Ø				
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PREPARED BY **D. Ross** DATE SHEET 10-9-19 55 1 of 2 BRIDGE NUMBER

KLEINFELDER Bright People. Right Solutions.

	T TITLE NG RECOR	RD.			LE ID RW-19	9-02	24							
DIST. <b>03</b>	COUNTY Sacrame	nto	ROUTE <b>51</b>	POSTMILE <b>1.05-2.6</b>		EA <b>03-</b> 1	1600-0113-0							
	PROJECT OR BRIDGE NAME Caltrans TO946183 C-57 SR51 Sac													
BRIDGE	NUMBER	PREP	PARED BY		DATE		SHEET							

10-9-19

2 of 2

D. Ross

LOGGE			BE	GIN DATE		OMPLETIC	ON DATE	BOREHOL	E LOC	ATION	(Lat/	Long	or N	orth/	East a	ind Datu	ım)		Item 4
E Sa		NITO	ACTOR	3-18-19	;	3-22-19		38.5863											RW-19-025 SURFACE ELEVATION
Greg								BOREHOL	E LOC	ATION	(Olis	ei, S	lalioi	II, LII	ie)				32.30 ft NAVD88
DRILLII				lud Rota	rv			DRILL RIG											BOREHOLE DIAMETER  6.0 in/4.63 in
SAMPL	ER T	YPE(S	) AND SI	ZE(S) (ID)				SPT HAMI	/IER T										HAMMER EFFICIENCY, ERI
				Punch C		.5")		Auto; 14						AF	TER	DRILLIN	IG (	DATE	<b>87%</b> ) TOTAL DEPTH OF BORING
						to surfa	ace	READINGS	3	21.							,		176.0 ft
ELEVATION (ft)	ОБЕРТН (ft)	Material Graphics				CRIPTIO			Sample Location Sample Number	Blows per 6 in.	Blows per foot	Recovery (%)	RQD (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Shear Strength (tsf)	Drilling Method	Casing Depth	Remarks
			POORL moist; f	Y GRADE ine SAND;	D SANI non-pla	O with Silt ( astic.	(SP-SM); ol	ive brown;									$\forall$	На	nd Auger to 5 feet
30.00	5		SANDY fine SA	´SILT (ML ND; low pl	); loose; asticity.	yellowish	brown; mois	st; some	X01	1 2 3	5	83						Sw	itch to Hollow Stem Auger
25.00	10	- - -	mediun	n dense; m	nulticolor	ed olive br	rown and oli	ive.	7 2	4	9	66						PA	
20.00			SILTY	 SAND (SM	 1); loose;	 olive brow	 vn; moist; fir	ne SAND;	802	4 4 5								PA	
	15	- - -	i little fin	es; non-pla	astic.				803	5 2 3	5	44						PA	
15.00			SANDY SAND.	'SILT (ML		olive brow	- — — — vn; moist; so	 ome fine											
10.00	20	- - -	wet.						S04	0 2 4	6	22						PA	
	25	•	SILTY Solive br	SAND (SM own; wet; f	l); mediu fine SAN	ım dense; ID; little fin	multicolored nes; non-pla	d olive and stic.	S05	3 5 8	13	100					700	Sw	itch to Mud Rotary
5.00			gray.						900	3		100					doodood		
0.00	30						807	0 5 7	12	89 100					000000	PA			
	35		:		lo	continued)			C08								0000		
										REPOI				П					HOLE ID <b>RW-19-025</b>
(	K	(LI	EIN	FEL	DE	R				DIST.  03  PROJE	CO	UNT acra	Y ame	nto	5	OUTE I <b>1</b>		05-2	ILE EA

gINT FILE: KIF\_gint\_master\_2017 PROJECT NUMBER: 20178946.183A OFFICE FILTER: SACRAMENTO gINT TEMPLATE: E:KLF\_STANDARD\_GINT\_LIBRARY\_2017.GLB [CLIENT\_CALTRANS BORING RECORD MET/ENG]

PLOTTED: 08/27/2019 07:09 AM BY: DRoss

PREPARED BY
E Santos / D. Ross BRIDGE NUMBER DATE SHEET 7-23-19 57 1 of 5

ELEVATION (ft)	0 0 0 0 0 0 0 0 0	ייים ווי)	Material Graphics	DESCRIPTION	Sample Location Sample Number	Blows per 6 in.	Blows per foot	Recovery (%)	RQD (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Shear Strength (tsf)	Drilling Method	Remarks
	_33			POORLY GRADED SAND with Silt and Gravel (SP-SM); dense; grav; wet; few fine to coarse subrounded GRAVEL:	S08	8 9 14	23	44					100	PA Rig chatter
-5.00			2000000	medium to fine SAND; few fines; non-plastic.  POORLY GRADED GRAVEL with Silt and Sand (GP-GM); very dense; gray; wet; fine to coarse subangular to subrounded GRAVEL, 2 in. max. dia.; some coarse to fine SAND.	$\Pi$	14		NR					doooood	raig Chautei
	40	_	0000000		S11	16 25 18	43	33					0000	WA
-10.00			000000000000000000000000000000000000000		C12			NR					0000	
	45	-	0000		S13	47 50/3"	50/3	44						-
-15.00			00000000000000000000000000000000000000		8	50/3"							11111	
	50		0000										000	
	30		0000		\$ 4 <u>1</u> 8	36 50/5"	50/5	54						
-20.00			0000										0000	
	55			SILT with Sand (ML); very dense; olive; moist; little fine SAND; medium plasticity; some cemented nodules.									000	End of rig chatter
			-	moderate cementation.	\$15	48 50/3"	50/3	NR 100					200	PI _
-25.00			- -		C16								MANNA	
	60	-		POORLY GRADED SAND with Silt (SP-SM); olive; wet; medium to fine SAND.  SILT with Sand (ML); very dense; olive; wet; little fine SAND; non-plastic.	<u></u>	17 32 50/3"	82/9	100					<u> </u>	-
-30.00				SAND; non-plastic.  POORLY GRADED SAND (SP); olive; wet; medium to	S17	50/3"		100				PP=4.5	00	
	0.5			fine SAND; little fines.  ELASTIC SILT (MH); hard; olive; moist; few fine SAND; high plasticity; weak to moderate cementation.	C18								0000	
	65			pale olive.	S19	16 26 27	53	100					0000	PI
-35.00								100				PP=>4.	1000	
	70	_	•	weak cementation.  SILTY SAND (SM); very dense; olive; moist; fine SAND; some fines; low plasticity.	C20	17	58	100					00000	
40.00					821	17 26 32	_	100					200	
-40.00					C22								300000	
	75			LEAN CLAY with Sand (CL); very stiff; pale olive; moist; little fine SAND; low plasticity.	S23	26 31 32	63	83				PP=3.2	1000	
				(continued)		REPOF				_				HOLE ID
		L		EINFELDER		BOR DIST. 03	CO S	UNT <b>acr</b> a	Y ame	nto	5	OUTE	PO: <b>1.</b>	RW-19-025  STMILE EA 03-1600-0113-0
				Bright People. Right Solutions.		PROJE Caltr BRIDG	ans '	TO9	461	83 C	-57 PARI	SR51 ED BY		DATE SHEET SS 7-23-19-58 2 of 5

OFFICE FILTER: SACRAMENTO PROJECT NUMBER: 20178946.183A gINT FILE: KIf\_gint\_master\_2017 gINT TEMPLATE: E:KLF\_STANDAI

	I			T <sub>C</sub> T														_
ELEVATION (#)	DЕРТН (ft)	Material Graphics	DESCRIPTION	Sample Location	Sample Number	Blows per 6 in.	Blows per foot	Recovery (%)	RQD (%)	Moisture Content (%)	Dry Unit weignt (pcf)	Shear Strength (tsf)	Drilling Method	Casing Depth		Remark	6	
-45.00			SILTY SAND (SM); multicolored olive and yellowish brown; moist; medium to fine SAND; some fines; non-plastic.		C24			100				PP=3.2						
	80 -		LEAN CLAY with Sand (CL); hard; pale olive and mottled yellowish brown; moist; little fine SAND; medium plasticity; oxidation.	M	S25	8 28 32	60	83				PP=>4.	000					
-50.00			POORLY GRADED SAND with Silt (SP-SM); medium dense; multicolored yellowish brown and dark gray; moist to wet; fine SAND.  12 inch thick lenses of LEAN CLAY (CL); hard; pale olive; wet; few fine SAND; low plasticity; moderate to strong		C26			100					10000					
	85 -	<b>-</b>	cementation.	X	S27	16 10 6	16	72					000					
-55.00	_		POORLY GRADED SAND (SP); multicolored olive, yellowish brown and dark gray; wet; medium to fine SAND.  SILTY SAND (SM); olive; wet; fine SAND; little fines;		C28			100					100000					
	90		non-plastic; moderate to strong cementation.  SANDY SILT (ML); hard; olive; moist; some fine SAND; low plasticity.	X	S29	26 30 50/5"	80/11					PP=>4.						
-60.00	_	-         	POORLY GRADED SAND with Silt (SP-SM); multicolored olive and olive brown; wet; fine SAND; non-plastic.	1	C30			28					00000					
05.00	95		POORLY GRADED SAND (SP); very dense; olive; wet; medium to fine SAND; mica flakes.	X	S31	20 26 30	56	72 100					0000					
-65.00	100				C32								MANNA					
	100		SILT with Sand (ML); hard; multicolored olive and yellowish brown; moist; little fine SAND; low plasticity.	X	S33	17 28 50	78	100				PP=>4. PP=>4.	3000					
-70.00	-		LEAN CLAY (CL); hard; pale olive and mottled yellowish brown; wet; few fine SAND; low plasticity; weak to moderate cementation.		C34			100					mmin					
	105			X	835	20 20 42	62	100				PP=>4.	0000	PI				
-75.00			SILTY SAND (SM); very dense; multicolored olive brown		C36			00					mone					
	110		and yellowish brown; wet; fine SAND; little fines; non-plastic; weak to moderate cementation.  POORLY GRADED SAND (SP); very dense; multicolored	X	837	29 50/6"	50/6	100					0000					
-80.00			brown, yellowish brown, and olive gray; wet; medium to fine SAND; weak to moderate cementation.		C38								10000					
	115		olive brown.		839	22 24 34	58	77					00000					
-85.00					C40			.00					1111					
			(continued)		T F	EPOR	T TIT	ΓLF							HOLE	D		_
	K	CLI	EINFELDER Bright People. Right Solutions.		E	BORI DIST. 03 PROJE	NG CO S	REC UNT acra R BF	Y <b>ame</b> RIDG	e <b>nto</b> SE NAI	│ <b>5</b> ME	DUTE 61 SR51	1	OSTM . <b>05-2</b>	<u> </u> RW ILE	<u>-19-02</u> EA	2 <b>5</b> 1600-01 <sup>,</sup>	13
			<i>(</i>		В	RIDGE	NUI	MBE	R			ED BY OS / D	. R	oss	D/ <b>7</b>	TE <b>-23-19</b> =	SHEET	5

OFFICE FILTER: SACRAMENTO PROJECT NUMBER: 20178946.183A gINT FILE: KIf\_gint\_master\_2017 gINT TEMPLATE: E:KLF STANDA

ELEVATION (ft)	DEPTH (ft)	Material Graphics	DESCRIPTION	Sample Location Sample Number	Blows per 6 in.	Blows per foot	Recovery (%)	RQD (%)	Moisture Content (%) Dry Unit Weight	(pcf)	Shear Strength (tsf)	Drilling Method Casing Depth	Remarks
	120	•	POORLY GRADED SAND (SP); dense; olive brown; wet; medium to fine SAND; weak to moderate cementation. dense.	S41 C40	13 14 17	31	100 72	_					
-90.00			LEAN CLAY (CL); hard; pale olive mottled black; wet; few fine SAND; medium plasticity; moderate to strong	- C45			100			PF	P=>4.5	00000	
	125		fine SAND; medium plasticity; moderate to strong cementation.	S43	12 22 27	49	66					0000	
-95.00			very stiff to hard; weak cementation.	C44			64			PP 4	°=3.25 4.25, 4.25		
	130		hard; weak to moderate cementation.	S45	16 26 33	59	100			PP	°=4.25	0000	
100.00			SILT with Sand (ML); very dense; vellowish brown; moist;	C46			.30				4.5		
105.00	135	•         •         •	little fine SAND; non-plastic.  POORLY GRADED SAND with Silt (SP-SM); very dense; yellowish brown; wet; fine SAND.	S47	18 27 42	69	100			>		0000000	
	140	-		248									
110.00			POORLY GRADED SAND (SP); very dense; olive brown; wet; medium to fine SAND.	C50 \$49	23 50/5"	50/5	100	1				0000000	
	145			S51 C	12 24 44	68	77					000000	
115.00			multicolored brown and yellowish brown. olive gray.	C52 S	44		100					0000000	
	150		fine SAND.  1 inch thick lenses of LEAN CLAY (CL); olive and pale	S53	14 17 30	47	100					000	
120.00			olive; moist at 151.0' and 151.5'. medium to fine SAND; weak cementation.	C54			100					000000	
	155		coarse to fine SAND; no cementation.	S55	8 14 23	37	50						
125.00	160		fine SAND.	C56								00000	
	160		(continued)	S57		87	77					00	
(			EINFELDER		REPOR BOR DIST. 03	ING CO	REC OUNT Sacra	Y ame	ento	ROU <b>51</b>	JTE		HOLE ID <b>RW-19-025</b> STMILE EA 03-1600-0113
			Bright People. Right Solutions.			ans	TOS	<b>1461</b>	BE NAM 183 C-	57 SI	) BY		DATE SHEET  7-23-19 60 4 of 5

OFFICE FILTER: SACRAMENTO PROJECT NUMBER: 20178946.183A gINT FILE: KIf\_gint\_master\_2017 gINT TEMPLATE: E:KLF\_STANDAI

08/2/72019 07:09 AM BY: DRoss 0.00 ELEVATION (ft)	DEPTH (ft)	Material Graphics	DESCRIPTION		Sample Number	Blows per 6 in.	Blows per foot	Recovery (%)	RQD (%)	Moisture Content (%)	Dry Unit Weignt (pcf)	Shear Strength (tsf)	Drilling Method	Remarks Remarks
-130.00	165		POORLY GRADED SAND (SP); very dense; olive gray; wet; fine SAND.	×		26 41 46			-				00000000	_ _ _
-135.00				X	S58	24 32 41	73	83					DODDODDO	
-140.00	170		SILT (ML); hard; pale olive mottled white and olive yellow; wet; few fine SAND; low plasticity.		S29	28 40 40	80						sacadadadada	
-145.00			weak to moderate cementation.  Bottom of borehole at 176.0 ft bgs Borehole was terminated at proposed depth. Borehole was backfilled with neat cement grout placed via tremie pipe and topped with native soil.		860	23 50/6"	50/6	100			F	PP=>4.		
-150.00	180													
-155.00	185													
-155.000 -15	190													-
GLB	195													-
-165.000 -165.000 -170.000 -170.000	200													
gini iemiPLAIE: E:KLF_STAN	P	< < L E	EINFELDER Bright People. Right Solutions.		D P	EPOR BORI IST. 03 ROJEC Caltra RIDGE	NG F COL Sa CT OI Ins 1	JNT acra R BF FO9	Y <b>IME</b> RIDG <b>461</b>	nto E NAM 83 C	<u>5</u> ME -57 \$	OUTE 1 SR51 ED BY	1	HOLE ID RW-19-025  DSTMILE EA 03-1600-0113-0  C DATE SHEET 7-23-19 61 5 of 5

	BOREHOLE L								Item 4
LOGGED BY BEGIN DATE COMPLETION DATE R Schmidt 8-5-19 8-9-19	HOLE ID								
DRILLING CONTRACTOR	38° 35' 29.					ine)			RW-19-036 SURFACE ELEVATION
Gregg	52.9' Rt St								55.6 ft
DRILLING METHOD	DRILL RIG								BOREHOLE DIAMETER
Rotary Wash SAMPLER TYPE(S) AND SIZE(S) (ID)	Mobile D83	-							4.5 in  HAMMER EFFICIENCY, ERI
SPT (1.4")	AUTO	L							96%
BOREHOLE BACKFILL AND COMPLETION	GROUNDWA <sup>-</sup> READINGS					FTER	DRILLIN	IG (DA	11
8/9/2019			t meas			1			101.0 ft
DEPTH (ft) Material Graphics NOITHIER	Sample Location	Sample Number Blows per 6 in.	Blows per foot	Recovery (%)	RQD (%) Moisture	Dry Unit Weight (pcf)	Shear Strength (tsf)	Drilling Method Casing Depth	Remarks
ASPHALT CONCRETE 5".  CLAYEY SAND (SC); dense; redding brown; r	moist: fine								
SAND; 20% fines.	noist, iine								
50.60 5									
	X		14	100					
		7_	-						
45.60 10									
	M	6 9		89				]}	
		10	-						
40.60 15									
40.00   13   14   17	X	11 13 14	27	78					
		14	-						
Poorly graded SAND with CLAY (SP-SC); den 35.60 20 yellowish brown; moist; medium to find SAND	se; dark ; few fines.								
33.00   20   7   7	X	10 17 23	40	89				000	
		23	4						
20 00 00 00									
30.60 25	X	13 17 25	42	67				000	
		25	4					0000	
25.60 30 SILT (ML); stiff; dark brown; moist; low plastici	ty fines :								
25.60 30   SILT (ML); stiff; dark brown; moist; low plastici PP=2.0tsf.	ty iii los ,	5 4	12	78					
		8	4						
								200	
20.60 35	X	3 5 6	11	67				20	
			-{-	$\neg$					
15 60 40 SILT with SAND (ML); brown; moist; little fine	SAND							200	
15.60 40 SILT WITH SAND (ML); brown; moist, little line.	C, 11 412.							000000000	
10 60 45								20	
10.60 45 SANDY SILT (ML); dense; brown; moist; some SAND.	e tine	5 7	15	89				200	
		8	$-\Box$					000	
5.60 50 SILT with SAND (ML); medium dense; dark ye brown; moist; little fine SAND.	ellowish	4 5 6	11	56					
			-/					000	
I [ ]								20	
(continued)			ı			1	I	الصا	1
		REPO	RT TIT	LE -					HOLE ID
Department of Transportation  Division of Engineering Ser		BOF DIST.	RING F	REC DUNT		ROUTE	: PO	STMIL	RW-19-036 LE PROJECT ID
Division of Engineering Ser	VICE2	03		AC		51		6/2.9	
Geotechnical Services									
Geotechnical Services Office of Geotechnical Desi	ian - North				IDGE N		Widen)	)	

ELEVATION (ft)	را PDEPTH (#)		Material Graphics	DESCRIPTION	Sample Location	_	Blows per 6 in.	Blows per foot	Recovery (%)	RQD (%)	Moisture Content (%) Dry Unit Weight	Shear Strength (tsf)	Drilling Method	Remarks
				SILT with SAND (ML) (continued).	>		2 3 5	8	100				0000	
-4.40	60		3 12	Poorly graded SAND (SP); dense; dark grayish brown; moist.			6 8 9	17	89				00000	
-9.40	65			Poorly graded GRAVEL (GP).	Σ			50/4	0				00000	
-14.40	70	H		SILTY SAND (SM); very dense; moist; medium to fine SAND; little fines.			17 22 33	55					MANDANA	
-19.40	75			SILT (ML); hard; olive; moist; PP>4.5tsf.	_		36 \50/5"	50/5	91				<u> </u>	
-24.40	80				Σ		22 29 50/2"	79/8	100				<u> </u>	
-29.40	85	_			>		14 - 23 \ 19	42	100				00000	
-34.40	90			Poorly graded SAND with SILT (SP-SM); very dense; yellowish brown; moist; fine SAND; few fines.	Σ		22 31 50	81	89				0000000	
-39.40	95				>		15 - 23 - 32	55	89				DODDODDOD	
-44.40	100			Bottom of borehole at 101.0 ft bgs			20 33 37	70	0				2000	
-49.40 <sub>00</sub>	105	_												
3 2013).GLB 2/20 -54.40 04.45	110	_												
-59.40 -59.40	115	_												
-64.40	120													
5 BR - STANDARD AR. GPJ CALTRANS LIBRARY (FEB 2013). GLB 2/20/20  - 6 GP	L		_/	Department of Transportation Division of Engineering Services Geotechnical Services		[	REPORI BORI DIST. 03	NG I	REC DUN BAC	ΓΥ	ROUTI <b>51</b>	PC 2	STM . <b>6/2</b> .	HOLE ID <b>RW-19-036</b> ILE PROJECT ID <b>0312000054</b>
BR - SI				Office of Geotechnical Design - Nort	:h		PROJEO Amer BRIDGE	ican	ı Riv	er E	E NAME <b>Bridge (</b> PREPAI		)	DATE SHEET
2							<b>24-0</b> (	003	اعاص	`	YZAŁ	A		9-18-19 <sub>-63</sub> 2 of 2

							l = · ·											Item 4
LOGGE R Scl				N DATE <b>6-19</b>	COMPL <b>8-16-</b>	ETION DATE		DLE LOC					orth/Ea	st and	Datui	m)		HOLE ID <b>A-19-037</b>
DRILLIN	NG CC		ACTOR			-	BOREH	DLE LOC	ATION	(Offs	et, S	tation	, Line)					SURFACE ELEVATION
Greg							_	_t Sta 2	20+28	3.6 S	R51	l						53.7 ft
DRILLIN Hollo							DRILL R											BOREHOLE DIAMETER <b>6 in</b>
			) AND SIZE	(S) (ID)				MMER TY	PE									HAMMER EFFICIENCY, ERI
SPT (	(1.4")	)					AUTO											87%
8/16/2			FILL AND C	OMPLETIC	ON		GROUN READIN	DWATER GS	Not					ER DRI	LLIN	G (E	DATE)	TOTAL DEPTH OF BORING 41.5 ft
ELEVATION (ft)	'DЕРТН (ft)	Material Graphics			DESCRIP	TION		Sample Location Sample Number	Blows per 6 in.	Blows per foot	Recovery (%)	RQD (%)	Moisture Content (%) Dry Unit Weight	(pcf) Shear Strength	(tsf)	Drilling Method	Casing Deptin	Remarks
48.70	5		ASPHALT AGGREG	ATE BASE	11".	(SP-SM); very e SAND ; few fi	dense; nes.		2 20 28	48	78					<b>}</b>		
43.70	10								9 12 18	30	100					     		
38.70	15							X	32 19 22	41	89							
33.70	20		SILTY SA moist; fine	ND (SM); v e SAND ; so	very dense; ome fines.	; dark yellowish	brown;		7 12 17	29	89	-						
28.70	25							X	11 19 20	39	100	-				}  		
23.70	30							X	6 15 24	39	100	-						
18.70	35								10 9 9	18	100	-				} } }		
13.70	40		Bottom of	borehole a	at 41.5 ft bg	ıs			4 6 9	15	100	_						
8.70	45																	
3.70	50																	
								1.	DEDOD	ייד דו								L HOLE ID
				-		Transportatio			BORI	NG I	REC			'	D0.1	· · ·		HOLE ID A-19-037
		7		Geote	chnical S	ineering Services chnical Desi		F	DIST. <b>03</b> PROJE <b>Ame</b> r	S CT O	SAC R BI	RIDGI	ROU 51 E NAM			6/2.		PROJECT ID <b>0312000054</b>
				Onice	oi Geore	oriinoai D <del>e</del> Si	911 <b>-</b> 1101		BRIDGE 24-0	E NUI				ARED				DATE SHEET 9-25-19, 64 1 of 1

LOGGE	D RV		REGIN	N DATE	E	COM	DI ETIC	ON DATE	BOREHO	IELO	ΑΤΙΟΙ	VI (I at	/Long	or N	orth/	East a	nd Dati	ım)		Item 4
	hmidt		8-8-		_	8-9		NI DATE	38° 35						orul/	_asi a	iiu Dall	a111)		A-19-038
DRILLIN		NTRA	CTOR						BOREHO						n, Lin	e)				SURFACE ELEVATION
Greg		FLIOD							66.3' F		221+	50.2	SR5	1						53.4 ft
DRILLIN <b>Hollo</b>	w-Ste								DRILL RI Mobile											BOREHOLE DIAMETER 6 in
SAMPL	ER TYF		AND SIZE(	(S) (ID)	)				SPT HAN		YPE									HAMMER EFFICIENCY, ER
SPT (		101/5		014515					AUTO			211.10						10 (	D 4 T E \	96%
8/9/2		ACKF	ILL AND C	OMPLE	=1 ION	l			GROUNI READING			t mea		ed				NG (I	DATE)	TOTAL DEPTH OF BORING 41.5 ft
ELEVATION (ft)	рБРТН (ft)	Material Graphics			DI	ESCR	IPTION	N		Sample Location	Blows per 6 in.	Blows per foot	Recovery (%)	RQD (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Shear Strength (tsf)	Drilling Method	Casing Depth	Remarks
48.40	5		ASPHALT AGGREGA SANDY lea SAND; so	ATE BA	ASE 1	9".	; dark b	orown; moi 25.	st; fine	<i></i>								<i>{</i> }		
<del>-1</del> 0.40			CLAYEY S	SAND (	 (SC)· (		stiff: da	. — — — - ark vellowi	 sh brown:	-	5 9 \ 15		67							
43.40	10		CLAYEY S moist; fine								6 10 12	22	78							
38.40	15		Poorly gra brown; mo	ded SA pist; fine	AND (S	SP); ve edium	ery den: sand S	se; dark ye SAND ; trad	ellowish ce fines.		12 14 14	28	67	_						
33.40	20										13 17 20	37	78	-						
28.40	25										16 25 28	53	78							
23.40	30					<u>.</u>	<u> </u>	· <del></del>			10 14 16	30	67	-						
18.40	35		SILT (ML); fines ; 3.1.	; mediu	um stif	ff; dark	( brown	; moist; lov	w plasticity		7 5 6	11	100					- - - - - - -		
13.40	40		Bottom of I	boreho	ole at 4	11.5 ft l	bgs				3 2 3	5	100							
8.40	45 -																			
3.40	50 -																			
	-၁၁										REPC	RT TI	TIF							HOLE ID
				Divi	ision	of En		nsportation ring Ser ces			DIST.	RING C	OUN SAC	TY ;	R0 <b>5</b>			STN .6/2	/ILE .9	A-19-038 PROJECT ID 0312000054
									gn - Nort	h	PROJ <b>Am</b> e	ect ( Ecta	JR B <b>n Ri</b>	RIDG <b>ver l</b>	E NA <b>Brid</b>	ME ( )	Widen	)		
				•						Ī	BRIDO		IMBE		PRE	PARI <b>ZAK</b>	ED BY			DATE SHEET  9-18-19-65 1 of 1

															Item	1 4
Yusuf	GGED BY  SEGIN DATE  SUBSTITUTE  SEGIN DATE  COMPLETION DATE  SEGIN DATE  SEGI												ım)		HOLE ID <b>RW-19-0</b> 4	
Greg	3			60.0' Rt			•			, Line	<del>:</del> )				52.8 ft NAVE	
DRILLIN				DRILL RIG	02										BOREHOLE DIA	METER
Rotar	-		ne AND SIZE(S) (ID)	Mobile B		DE									4.6 in HAMMER EFFIC	IENICY FD:
SAMPLE SPT	_r: I )	i F ⊑(5	I AND SIZE(S) (ID)	Auto	∟r: IY	rc									96%	ILINOT, EKI
	OLE	BACK	FILL AND COMPLETION	GROUNDW	ATER	DUR	NG D	RILL	ING	AF1	ΓER D	RILLIN	IG (E	DATE)	TOTAL DEPTH	OF BORING
	ill N	eat C	ement	READINGS	_										141.5 ft	
ELEVATION (ft)	<sup>2</sup> DEРТН (ft)	Material Graphics	DESCRIPTION		Sample Location Sample Number	Blows per 6 in.	Blows per foot	Recovery (%)	RQD (%)	Content (%)	Dry Unit weignt (pcf)	Shear Strength (tsf)	Drilling Method	Casing Depin	Remark	S
		- K-d	ASPHALT CONCRETE (4"). CONCRETE (8").	f									}			
	H		Poorly graded SAND (SP); medium dense; oliv moist; fine to medium, subangular SAND; few	re brown; fines.	X 1	-	14	28								
			, ,		1	5 5 9	14	_20								
42.80	10		Little GRAVEL.		≥ 2		18 A	0 /								
	-				كا	8 9 9		ر ت								
		2,7	Coarse GRAVEL.		X 3		6	0		1				PA		
		000	Poorly graded GRAVEL with SAND (GP); gray mostly fine GRAVEL; some fine to coarse SAN	ID.		3 3 3							200	^		
32.80	20 -	000		ļ	X 4			0		_	$\dashv$		000			
	+	0000		ľ	7					$\top$						
	t	000		}	5					+						
	F	000											200			
22.80	30 -	000	Poorly graded SAND (SP): loose: brown: moist		X 6	2	6	39					000			
	$\vdash$		Poorly graded SAND (SP); loose; brown; moist medium SAND; trace fines.			2 3 3				$\top$						
		1//	Lean CLAY (CL); stiff; gray; moist; high plastici PP = 1.5 tsf.	ıy πnes ;	X 7	3	14	100		+				PI		
	-	1//		ľ	Ť	3 5 9							000			
12.80	40 -	HH	SILT (ML); very dense; yellowish brown; moist;		8	12	73	100		_+						
	t	]	plasticity fines; strong cementation.			12 26 47				$\top$			200			
	F	₩	SANDY lean CLAY (CL); very dense; yellowish	brownish	9	16	74	100		$\pm$			000			
	-	1//	gray; moist; some fine to medium SAND.			16 31 43				T	T					
2.80	50 -	'nπ	SANDY SILT (ML); very dense; grayish green; some fine SAND; mostly nonplastic fines.	moist;	X 10	14	34	100		22			0000	PA		
			\some fine SAND ; mostly nonplastic fines Poorly graded SAND with SILT (SP-SM): grav:	moist; fine		14 17 17	$\sqrt{1}$			$\neg$			000			
	F		Poorly graded SAND with SILT (SP-SM); gray; to medium SAND; little fines. SILTY SAND (SM); very dense; gray; moist; fin	e SAND	11	14	46	100								
	-		some fines.	O, 4 VL ,		14 22 24	1									
-7.20	60 -				12	10 16 26	42	100					200			
						26							000			
	-		SILT with SAND (ML); very dense; brownish gr	ay; moist;	13	17 27 39	66	100								
	_	$\prod$	\little fine SAND SILT (ML); very dense; brownish gray; moist; ti	ace fine		39	4									
-17.20	70	<u> </u>	SAND.	ļ	14	23 50/5"	50/5	109,		+			000			
						100/0										
	-		Low plasticity fines.		15	20 33 50/4"	83/10	75								
	_		Hard; medium plasticity fines; PP = + 4.5 tsf.			50/4"	4						000			
	80-		(continued)			I							IX )	1		
			Department of Transportation	on		REPOR			, DDI	$\overline{}$					HOLE ID	040
	_		Division of Engineering Serv			BORI DIST.	CC	DUN <sup>-</sup>		RO	UTE		STM		RW-19-	U4U
		7	Geotechnical Services			03 PROJE	_	R RE	SID כי	51 NAM		2.	5/4.	3	0H931	
			Office of Geotechnical Desi	gn - North		SR 5	1 Ca	pita	I Cit	y Co	orrido					
						BRIDGI	E NUN	MBEI	R		PARE	D BY <b>eve R</b>	- مامرر	_	DATE 9-5-69 <sub>GE</sub> 6	SHEET

ELEVATION (ft)	Эрертн (#)	(11)	Material Graphics	DESCRIPTION	Sample Location	Sample Number	Blows per 6 in.	Blows per foot	Recovery (%)	RQD (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Shear Strength (tsf)	Drilling Method	Remarks
	-80-	П	Ш	SILT (ML) (continued).	X	16	20 35 40	75	100					<u> </u>	
				SANDY SILT (ML); dark brown; moist; some fine SAND; mostly fines.	×	17		F0/F	440		25			000	PA
			$\prod$			11/	31 (50/5")	<u>50/5</u>	(110)		25			000	
-37.20	90	Н		SILT (ML); very dense; yellowish brown; moist; few fine SAND; moderate cementation; alternating layers of SILT (ML) and SILTY SAND (SM).	X	18	23	70	100					2000	
				()			23 31 39							$\bowtie$	
		H		SILTY SAND (SM); very dense; brown; moist; little fine SAND.	X	19	15 47 47	94	100					000	
-47.20	100													000	
		Н		SANDY SILT (ML); very dense; yellow brown; moist; some fine SAND; mostly nonplastic fines.	X	20	15 21 25	46	100		23			0000	PA
				SILTY SAND (SM); very dense; moist; medium SAND; medium plasticity fines.	·    X	21		53	100						
		H		medium plasticity lines.			18 26 27							000	
-57.20	110				X	22	15 23 24	47	100						
				Fet OLAY (OLD), projek high plantists force			24							000	
		H		Fat CLAY (CH); moist; high plasticity fines.	X	23	10 14 27	41	100					000	
-67.20	120					0.4			400						
		H				24	17 27 30	57	100					000	
				SILTY SAND (SM); very dense; brown; moist; some fine	X	25	15	70	100					200	
		Н		SAND.			15 25 45								
-77.20	130			Gray.	X	26	19 40 33	73	100					000	
		H													
					X	27	12 26 32	58	100		$\vdash$				
-87.20	140			Fat CLAY (CH): hard: gray: moist: high plasticity fines:	X	28		59	100					000	
			<i>// //</i>	Fat CLAY (CH); hard; gray; moist; high plasticity fines;  PP = + 4.5 tsf.  Bottom of borehole at 141.5 ft bgs	<u> </u>		12 28 31	<u> </u>	.00					,	
-97.20	150			This Boring Record was developed in accordance with the Caltrans Soil & Rock Logging, Classification, and											
	130	Ά		Presentation Manual (2010) except as noted on the Soil or Rock Legend or below.											
				Ç											
-107.20	160	H													H
		$\mathbb{H}$													
2 -117.20	170														
20		$\mathbb{H}$													
5						_		_						_	
-107.20 -117.20						1 -	DEDOD	T 71							HOLE ID
			7	Department of Transportation			BORI	NG	REC				1=-	0	HOLE ID RW-19-040
				Division of Engineering Services Geotechnical Services			DIST. <b>03</b>	5	SAC		51			STM <b>5/4.</b>	
				Office of Geotechnical Design - North	1		PROJEC SR 51	l Ca	pita	I Cit	ty Co	orrid			
				-		E	BRIDGE	NU	MBE	₹			ED BY <b>eve R</b>	yde	DATE SHEET 9-5-69 2 of 2

LOGGE	ח פע		BEGIN DATE COMPLETION DATE	BOREHO	EL	OC ^	TION	/I a+/	ore	or N	orth/	Eact c	nd Dat	ım\		Item 4	
Gene				38° 35'				`	_				nd Dall	ann)		A-19-042	
DRILLIN				BOREHO												SURFACE ELEVATION	
Greg				50.2' Lt	St			•							48.4 ft NAVD88		
DRILLIN				DRILL RIG		•										BOREHOLE DIAMETER	
Hollo SAMPLE			AND SIZE(S) (ID)	Mobile SPT HAM			PF									6 in HAMMER EFFICIENCY, ERI	
SPT	、	(0)		Auto	· • · L I \											87%	
			ILL AND COMPLETION	GROUND READING		ΓER	DUR <b>50.0</b>		RILI	ING	AF	TER [	DRILLIN	VG (I	DATE)		
	till Ne	eat C	ement	READING		. 1	50.0	π			T					51.5 ft	
ELEVATION (ft)	оертн (#)	Material Graphics	DESCRIPTION		Sample Location	Sample Number	Blows per 6 in.	Blows per foot	Recovery (%)	RQD (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Shear Strength (tsf)	Drilling Method	Casing Depth	Remarks	
	F		ASPHALT CONCRETE (4"). CONCRETE (8.5").		4									$ \lambda $			
			GONCRETE (8.5"). AGGREGATE BASE (18").		<del>//</del>									}}			
43.40	5		CLAYEY SAND (SC): dense: dark brown: dry:	fine to	Ή,	1	13	27	44		12				PA		
	F		medium SAND ; (FILL).		H	Ė	13 13 14							181			
38.40	10										_	_		$  \langle   $			
00.40			SANDY lean CLAY (CL); dark brown; moist; so medium SAND; (FILL).	ome fine to	X	2	9 14 21	35	81		15			$\ \ $	PA		
	F		modium orivo , (i ill.).				21	4									
33.40	15	///	CLAYEY SAND (SC); very dense; dark brown;		-	3	16	51	72		8			$\  \ $	PA		
	F		mostly fine to medium SAND; little fines; (FILI	L).	H		16 26 25		12		-			╢╣	' '		
28 40	20										_	_		]{}			
28.40	20		SANDY lean CLAY (CL): very stiff: light reddict	h brown:	-X	4	5 4 8	12	100					][]	Perd at 20	ched groundwater encountere 0'	
	F		SANDY lean CLAY (CL); very stiff; light reddist some fine SAND; high plasticity fines; PP = 3	.0 tsf;			<u> </u> 8	4							" 2	•	
23.40	25	1//	(NATIVE). Light brown; dry.		$\forall$	5	12	44	100		21				PA,	PI	
	F	1//	Eight brown, dry.		H		12 18 26		100		-1			{{	' ',		
10.40	<u>,</u>	1//															
18.40	30		Poorly graded SAND (SP); very dense; light re brown; fine to medium SAND; trace mica.	ddish	X	6	9 24 34	58	100					]//			
	F		Brown, fine to medium SAIND, trace mica.				34	4									
13.40	35		Light brown; fine to coarse SAND.		$\forall$	7	17	80	100					{{			
	E						37 43							{			
8.40	40	: : :															
J.+U	<b>T</b>		Light olive brown; fine to medium SAND.		X	8	19 27 29	56	78		$\Box$						
	E	} :::					29	/									
3.40	45		Light grayish brown; moist.		$\forall$	9	21	40	94								
	E	<b> </b>				_	21 19 21										
-1.60	50				$\square$									]]}]			
- 1.00	- E	ا م اه	Well-graded SAND (SW); dense; dark grayish wet; trace GRAVEL; trace fines; micaceous.	brown;	$\mathbb{M}$	10	9 9 19	28	100					{			
	E	1	Bottom of borehole at 51.5 ft bgs		,	1	19	I									
-6.60	55	1															
		1	This Boring Record was developed in accorda	nce with													
11.60	60	1	the Caltrans Soil & Rock Logging, Classification Presentation Manual (2010) except as noted of	n, and n the Soil													
	E	1	or Rock Legend or below.														
	E	1															
16.60	65	1															
	þ	1															
	<u>70</u> 上																
																1	
			Department of Transportation	on			REPOR BORI			COR	D					HOLE ID <b>A-19-042</b>	
			Division of Engineering Serv			D	IST.	CC	DUN	TY	RC	UTE		STN		PROJECT ID	
		7	Geotechnical Services				<b>03</b> PROJE	_	R BI		<b>5</b> F NA		2	.5/4	.3	0H931	
			Office of Geotechnical Design	gn - North	า		SR 5	1 Ca	pita	I Cit	y C	orrid					
	(					В	RIDGI	E NUI	MBE	R			D BY <b>eve R</b>	۔ امری		DATE SHEET  9-5-19 <sub>0e 68</sub> 1 of 1	

48.07 ft	ELEVATION DATUM NAVD 88	TOTAL DEPTH OF BORING 70.0 ft
DRILLER'S NAME E. Santellan	HELPER'S NAME R. Ryon/M. Ageev	TOTAL DEPTH OF FILL 13.2 ft
		CONSULTANT COMPANY GEI Consultants, Inc.
DRILLING ROD TYPE AND 6" HSA, 94mm	DIAMETER	FIELD LOGGER M. Horse
CASING TYPE, DIAMETER Surface, 6-in., 15 ft	R, INSTALLATION DEPTH	FIELD LOG REVIEWER G. Bradner
		HAMMER EFFICIENCY 83%
		AFTER DRILLING (DATE-TIME)
	DRILLER'S NAME E. Santellan  DRILL RIG MAKE AND MC MARL M-10 (Gregg Ri DRILLING ROD TYPE AND 6" HSA, 94mm  CASING TYPE, DIAMETER Surface, 6-in., 15 ft HAMMER TYPE, MAKE/MC Marl, automatic, 140 lb GROUNDWATER READING	DRILLER'S NAME E. Santellan R. Ryon/M. Ageev  DRILL RIG MAKE AND MODEL MARL M-10 (Gregg Rig No. D-44)  DRILLING ROD TYPE AND DIAMETER 6" HSA, 94mm  CASING TYPE, DIAMETER, INSTALLATION DEPTH Surface, 6-in., 15 ft  HAMMER TYPE, MAKE/MODEL, WEIGHT/DROP Marl, automatic, 140 lbs / 30-inch drop

	, , , , , ,								.9					
Elevation, feet	Depth, feet	CLASSIFICATION OF MATERIALS (Description)	Sample Location	Sample Number	Recovery, %	Blows per 6 in. [Blows per ft]	N <sub>60</sub> (ASTM)	PP or TV, tsf		Liquid Limit				REMARKS
		Gravel Road Base.												
-	1 2	[LEVEE FILL] FAT CLAY (CH); very stiff; greenish black (5G 2.5/1); moist; 95% high plasticity, high dry strength, high toughness fines; 5% sand; 0% gravel.		1				3.0P						S01A_001_002B
	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	toughness fines; 5% sand; 0% gravei.		2										No Recovery; cobble removed
45-	3 4	1-foot thick Fat Clay with Sand (CH) lense; 5% gravel, max. 1/2 in.; 10% fine to medium sand; 85% high plasticity fines.	- 100	3	100									S03B_003_004P S03A_004_005P
_	5	SilTY CLAYEY SAND (SC-SM); dense; dark brown (7.5YR 3/4); moist; 75% fine to medium sand; 25% lov plasticity fines; 0% gravel.	, <u>                                    </u>	4	44	12 16	40					25	HD	S04A_005_007S
-	6 -					13								
- (ala)	7 -	[LEVEE FILL] Poorly Graded SAND with Silt (SP-SM); medium dense; olive brown (2.5Y 4/4); dry; 91% fine to medium sand; 9% fines; 0% gravel.		5	71	\[29]/			3			9		S05A_007_008P
6   40 —	]	1991 1980 1980		-		9								No Recovery; soft
-	9 -		X	6	0	9	26							material
	10 -	As above except moist.				\[19] <i>[</i>								S07A_011_011P Driller notes very soft material
	12 -			_	40									Driller notes very
- - - - - - - - - - - - - - - - - - -	13	Approximate bettem of Loves Fill 42 27		7	40									easy drilling
-	14	[Approximate bottom of Levee Fill 13.2].												
40 — 135 135 35 30 — 30 — 30 — 30 — 30 — 30 — 30 —	15	SANDY SILT (ML); loose; dark yellowish brown (10YR 3/6); moist; 50% fine sand; 50% low plasticity fines; 0% gravel.		8	50	3 3 4	10					50	HD	S08A_016_016S
-	17 -					[7]								No Recovery Very soft material;
30-	18 -													easy drilling
	19 -			9	0									
-	20													
		Final Report V	ers	ion	5/2	21/20	010	)						
DWR LEVEE UND SOIL LOG REVI:	WATERARISOURICES	Borehole Location: South Bank Crest  Coordinates: Northing: 1,976,188.21 Easting: Latitude: 38.58732 Longitud Levee Station or Milepost: 1200+59 Levee M	<u>6,7</u> <b>le:</b> <u>-</u>	121.44	3.27	crame	ento							RING 003B Sheet 1 of 4
STATE OF	Levee Segment Survey Method: GIS/LiDAR Coord. System: CA State Plane Zone II Channel / River Name / Feature: American River								Urban Levee Geotechnical Evaluations Program Engineering Support Services					



Urban Levee Geotechnical Evaluations Program Engineering Support Services

						1	1					 		Item 4
Elevation, feet	Depth, feet	Material Graphics	CLASSIFICATION OF MATERIALS (Description)	Sample Location	Sample Number	Recovery, %	Blows per 6 in. [Blows per ft]	N <sub>60</sub> (ASTM)	PP or TV, tsf	Water Content, %	Liquid Limit			REMARKS
_	- 20 - - 21 -		SANDY SILT (ML); as above except medium dense.	X	10	0	5 6 6	17						No Recovery Rock stuck in hole
_	22 - 23 -		SANDY SILT (ML); medium dense; very dark brown (7.5YR 2.5/3); moist; 65% low plasticity fines; 35% fine to medium sand; 0% gravel.	X	11	0	\[12] 7 8 11							No Recovery Sandy Silt observed in cuttings
25—	24 -			M	12	0	[19] 5 4	15						No Recovery Driller notes rock still present in hole
_	- 25 - 26 -		Poorly Graded SAND with Silt (SP-SM); medium dense; dark brown (7.5YR 3/4); moist; 91% fine to medium sand; 9% low plasticity fines; 0% gravel; predominantly fine sand.		13 14	100	7 [11] 7					9		S13A_025_025P 2.25-inch cobble fragment on top of sample
	27 -				15	44	10 10 [20] 5	19		11			SG	S14Å_025_027M S15A_027_028S
20-	28 - 29 -	-			16	42	5 9 [14]							S16A_028_029P
_	- - 30 - 31 -		SILTY CLAYEY SAND (SC-SM); medium dense; dark brown (7.5YR 3/4); moist; 77% fine sand; 23% low plasticity fines; 0% gravel.		17	56	7 5 11	22				23	HD	S17A_030_032S
_	32 -		patient, mos, so grave.				\[16]							S18A_032_033P
15—	33 - 34 -				18	50								
_	- 35 <del>-</del> 36 -	<i>2/2/2</i> -	SILTY SAND (SM); dense; dark yellowish brown (10YR 3/6); moist; 80% fine to medium sand; 20% fines; 0% gravel.		19	56	9 12 13	35		12		20		S19A_035_037S
-	37 - 38 -	- 1					[25]							Box 1 Representative S20A_038_038P
10-	39 -				20	79								
-	- 40 - - 41 -		As above except medium dense.		21	61	9 11 11	30						S21A_040_042P
5— —	42 - 43 - 44 -	- 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	As above except very dark greenish gray (5G 3/1).		22	45	\[22]							S22A_042_043P
	- <b>45</b> -		Final Report Ve	ers.	ion	5/2	21/2	010	)					



DWR LEVEE UNU SOIL LOG REV1; AMERICAN RIVER LEVEE BORINGS 6-16-2010.GPJ; DWR OFFICIAL LIBRARY 032210.GLB; 6/16/10

Borehole Location: South Bank Crest County: Sacramento Coordinates: Northing: 1,976,188.21 Easting: 6,719,198.27 Latitude: 38.58732 Longitude: -121.44887 Levee Station or Milepost: 1200+59 Levee Mile: 3.79

Levee Segment \_

Coord. System: CA State Plane Zone II Survey Method: GIS/LiDAR Coord
Channel / River Name / Feature: American River

LOG OF BORING WCSBAR\_003B

Sheet 2 of 4

Urban Levee Geotechnical Evaluations Program Engineering Support Services

Levee Mile: 3.79

Coord. System: CA State Plane Zone II

DWR LEVEE UNU SOIL LOG REV1; AMERICAN RIVER LEVEE BORINGS 6-16-2010.GPJ; DWR OFFICIAL LIBRARY 032210.GLB; 6/16/10

Levee Station or Milepost: 1200+59

Channel / River Name / Feature: American River

Survey Method: GIS/LiDAR

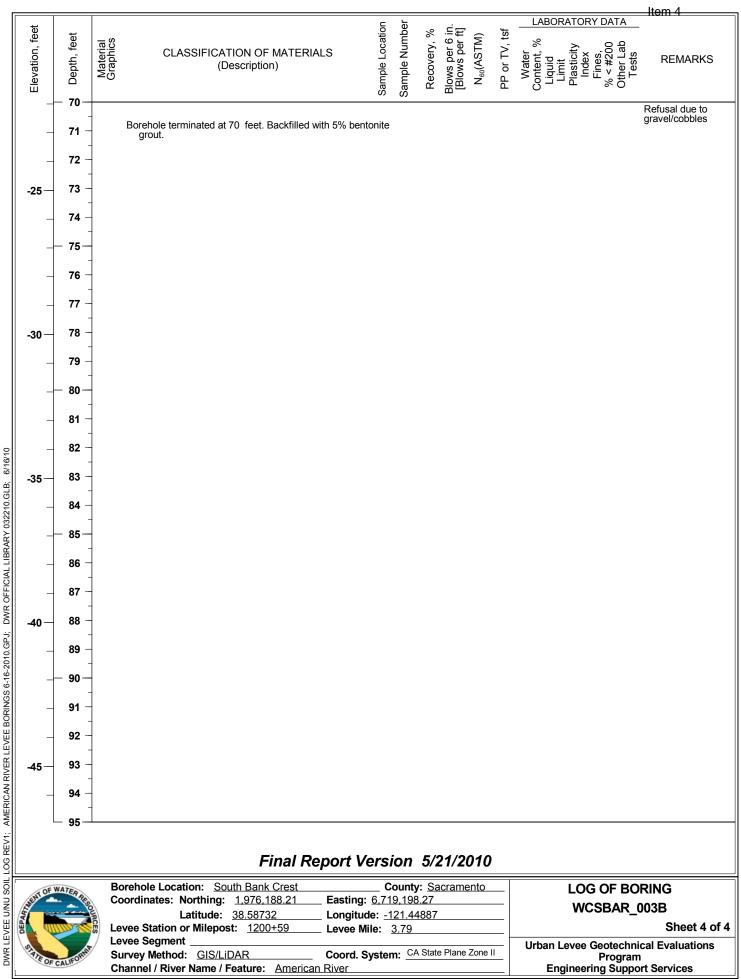
Levee Segment

**Urban Levee Geotechnical Evaluations** 

**Program** 

**Engineering Support Services** 

Sheet 3 of 4



## Memorandum

To: Madhwesh Raghavendrachar Office of Bridge Design North Structure Design Branch 11 At: Mark Okimura Date: November 26, 2019

File: American River
Br. No. 24-0003
03-Sac-51-PM 2.6
EA 03-3F0700
Project ID: 03-1200-0054

From: Department of Transportation
Engineering Service Center MS #9

Structure Hydraulics and Hydrology

Subject: Revised Draft Final Hydraulic Report

Attached is the revised Draft Final Hydraulic Report for the proposed deck replacement and widening for the American River Bridge. If you have any questions please call me at (916) 227-0444 or my mobile at (916) 224-9640.

Sincerely,

Neal Alie, P.E.

Hydrology/Hydraulics Engineer

Structure Hydraulics

American River Bridge Br. No. 24-0003 03-Sac-51-PM 2.61 EA 03-3F0700 Project ID: 03-1200-0054

State of California – Department of Transportation Division of Engineering Services Structure Design Services

Structure Hydraulics and Hydrology

DRAFT FINAL HYDRAULIC REPORT

American River Bridge

Located in Sacramento County Bride No. 24-0003

03-Sac-51-PM 2.61

EA 03-3F0700 EFIS: 03 1200 0054

November 26, 2019

		B10(F30(A)(B30)(B9)		
WRITTEN BY:			REVIEWED BY:	
Neal Alie			Ronald McGaugh	

This report has been prepared under my direction as the professional engineer in responsible charge of the work, in accordance with the provisions of the Professional Engineers Act of the State of California

The Professional Engineer's (P.E.) seal and signature will be included on the Final Hydraulic Report. **See Note on the following page.** 

REGISTERED ENGINEER

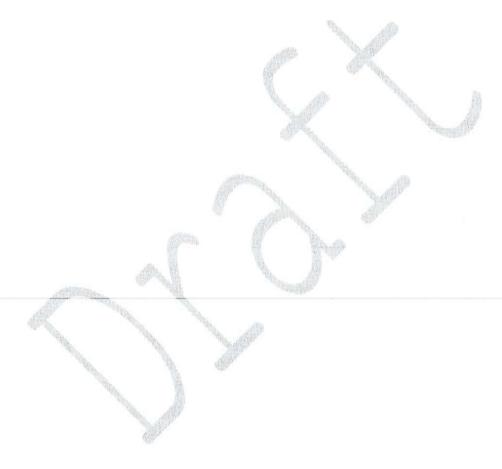
C 56398 Exp: 07/15/21

REGISTRATION NUMBER

03-Sac-51-PM 2.61 EA 03-3F0700

Project ID: 03-1200-0054

**Note:** This is a Draft Final Hydraulic Report which has been completed based on the preferred design alternative and other current information. The information reported in this study is considered valid (checked). However, any changes to the currently proposed bridge design details and/or other study assumptions may require changes to the hydraulic/scour analyses and report; therefore, the information provided in this report is considered "draft" and subject to revision. The Final Hydraulic Report will include the Professional Engineer's (P.E.) seal and signature and will be delivered when all bridge design details have been finalized for Final Structure Plans, Specifications, and Estimates (SPS&E).



03-Sac-51-PM 2.61 EA 03-3F0700 Item 4

Project ID: 03-1200-0054

## **Table of Contents**

1.0	General	Page 5
2.0	Drainage Basin	Page 6
3.0	Discharge	Page 8
4.0	Stage, Velocity and Waterway	Page 8
4.1	Existing Condition	Page 9
4.2	Proposed Variant B and C Condition	Page 10
5.0	Streambed and Scour	Page 11
5.1	Scour History	Page 11
5.2	Current Scour Evaluation	Page 12
6.0	Drift	Page 13
7.0	Bank Protection	Page 13
8.0	Hydrologic Summary for Design Engineer	Page 13
9.0	Scour Data Table	_

American River Bridge Br. No. 24-0003 03-Sac-51-PM 2.61 EA 03-3F0700 Project ID: 03-1200-0054

#### Hydrology/Hydraulic Report

#### 1.0 General

Structure Design in coordination with the District is proposing to replace the existing deck of the American River Bridge, Br. No. 24-0003, due to spalling and severe cracks. An intermediate widening is also proposed to facilitate the deck replacement while keeping all lanes open to traffic. Further future widening in addition to the proposed intermediate widening is proposed as part of a larger corridor project (03-0H931). The following two variants have been proposed:

Variant B- Deck replacement with the intermediate widening plus the substructure for the ultimate widening. (Preferred Variant).

Variant C- Deck replacement with the ultimate widening.

The new supports for the widening will match the existing support locations with pile caps with driven piles. The environmental work window in the river and flood plain is 5 months from May to September.

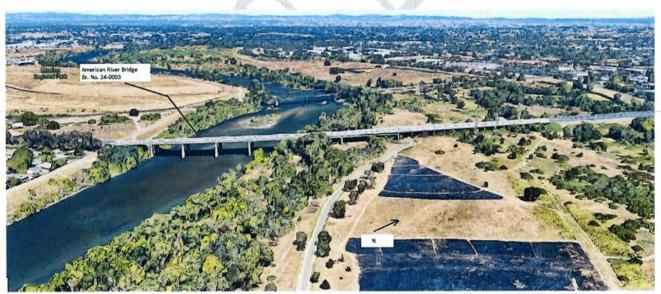


Photo 1 - Aerial view of the American River Bridge, Br. No. 24-0003

The existing American River Bridge is a 25-span, 1890-foot-long, 107.6-foot-wide structure built in 1954, widened in 1961, strengthened in 1988 and seismically retrofitted in 1997. The structure is a

Project ID: 03-1200-0054

simple span steel welded and riveted girder on RC hollow piers and RC 5-column bents and RC open end seated abutments, all founded on steel piles.

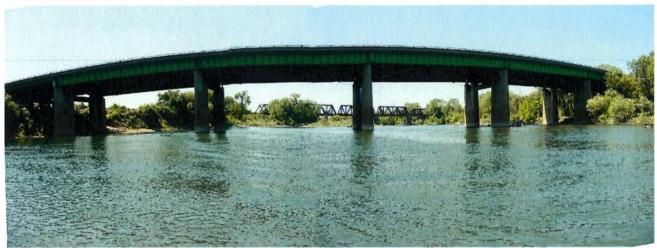


Photo 2 - American River Bridge, Br. No. 24-0003

This report makes extensive reference to the (1) Caltrans Bridge Maintenance Reports, (2) General plans and profiles submitted by structures, (3) Caltrans As-Built Plans (4) Previous Hydrology/Hydraulics Reports (5) FEMA Study, 07/19/2018, (6) FHWA Hydraulic Engineering Circular, (HEC-23), "Bridge Scour and Stream Instability Countermeasures", (7) Stability Rating Memo, 06/11/2002.

#### All Elevations used in this report are based on the NAVD 88 Datum.

#### 2.0 Drainage Basin

The American River drains a watershed of approximately 1900 square miles of the Tahoe and El Dorado National Forests, including the Granite Chief Wilderness and Desolation Wilderness. The river flows west from the peaks of the northern Sierra Nevada west of Lake Tahoe. Its streams gradually converge into the South, Middle and North Forks of the American River draining into Folsom Dam.

Although it was it was originally authorized by Congress in 1944 as flood control unit, Folsom Dam was reauthorized in 1949 as a multipurpose facility to also store water for irrigation, domestic, municipal and industrial use, hydropower generation, recreation, water quality and maintenance of flows stipulated to protect fish. Folsom Lake features roughly 10,000 surface acres of water when full and has 75 miles of shoreline. It extends about 15 miles up the North Fork American River and about 10 ½ miles up the South Fork.

Project ID: 03-1200-0054

During a 24-hour period, the releases of water from Folsom Dam can vary greatly to meet changing demands for water and power. Nimbus Dam, 7 miles downstream from Folsom Dam, stores these releases and re-regulates them to a steady flow downstream in the American River and allows Folsom Dam releases and power generation to fluctuate with daily power demands. Nimbus Dam forms Lake Natoma located in the town of Folsom. The Lower American River has levees on its north and south banks for about 13 miles from the Sacramento River to Carmichael on the north end. Portions of the floodplain have been acquired by either the City or County of Sacramento and is managed cooperatively as the American River Parkway.

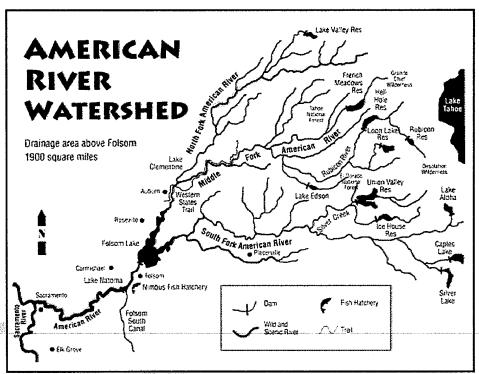


Figure 1- American River Watershed

The Lower American River begins at Folsom Dam and flows approximately 30 miles to its confluence with the Sacramento River near downtown Sacramento. The Lower American River Watershed has a number of contributing streams including Coon Creek, Markham Ravine, Auburn Ravine, pleasant Grove Creek, Curry Creek, Dry Creek, Cordova Creek (aka Clifton's Drain), and Arcade Creek. Most of these creeks enter the floodplain drainage systems of the Natomas Cross Canal and Natomas East Main Drainage Canal in southern Sutter and northern Sacramento Counties. The Natomas Cross Canal drains into the Sacramento River just south of the Feather River, and the Natomas East Main Drainage Canal drains into the Sacramento River just to the north of the American River.

The Lower American River watershed elevations range from approximately 400 feet at Folsom Dam

American River Bridge Br. No. 24-0003 03-Sac-51-PM 2.61 EA 03-3F0700 Project ID: 03-1200-0054

to approximately 23 feet at the confluence with the Sacramento River. The channel slope at the bridge site is approximately 0.0003. Average annual precipitation based on the Oregon Climate Service Prism Program (Annual normal from 1981 to 2010) is about 23 inches.

The project is located in a FEMA Special Flood Hazard Area (SFHA) designated as a Zone AE, where the Base Flood Elevations have been determined.

#### 3.0 Discharge

The American River levees were originally intended to convey a release from Folsom Dam of 115,000 cfs. During several major storm events since the construction of Folsom Dam, flows have equaled or exceeded the design capacity and caused significant erosion at the levees.

In the 1955 flood event, the peak release form Folsom Dam was 115,000 cfs. Soon after this flood event, the flood magnitude was factored into the hydrology of Folsom Dam operations, which led to the level of protection provided by Folsom Dam being considerably lowered.

In the 1964 flood event, Folsom Dam was again forced to release 115,000 cfs which was the first time the complete American River levee system was tested. This 1964 flood event showed considerable stress on the levee system but no major levee failures.

In the 1986 flood event, Folsom Dam was forced to release 130,000 cfs to avoid a dam failure. The peak flow was passed without any levee failure, but two locations were almost breached. One of the sites upstream from the Capital City Freeway experienced significant erosion and if the discharge was sustained any longer, the levee would have likely failed.

In 1997 Folsom Lake experienced a peak inflow of 255,000 cfs and was able to control it by releasing 115,000 cfs. Significant erosion occurred at five different sites along the American River which required immediate repair.

The objective release from Folsom Dam is currently under review as part of the Folsom dam Reoperations Study and the Joint Federal Project which is currently constructing improvements to the dam for a release of 160,000 cfs.

According to the FEMA Report dated July 19, 2018 the 100-year discharge is 180,000 cfs at Nimbus Dam. For the purpose of this project the FEMA 100-year discharge of **180,000 cfs** will be used.

#### 4.0 Stage, Velocity and Waterway

The U.S. Army Corps of Engineers Surface Water Modeling System (SMS) program was used to

EA 03-3F0700 Project ID: 03-1200-0054

perform a two-dimensional hydraulic analysis to calculate the water surface elevations and velocity for the existing structure and for the proposed widening.

The General Plans submitted by Structure Design was referenced to acquire the planned deck elevation height. The proposed freeboard is measured from the water surface elevation to the lowest chord of the soffit of the structure.

The parameters used to model the existing and proposed widening for the American River Bridge includes, the 100-year discharge of 180,000 cfs, a manning's roughness coefficient of 0.033 and a gradient of 0.0052 ft/ft at the bridge. The model results are as follows:

#### 4.1 Existing Condition

Discharge (cfs)	Minimum Soffit Elevation (ft)	Water Surface Elevation (ft)	Average Channel Velocity (fps)	Available Freeboard (ft)
100 -Year Discharge 180,000	46.30	41.14	6.86	5.14



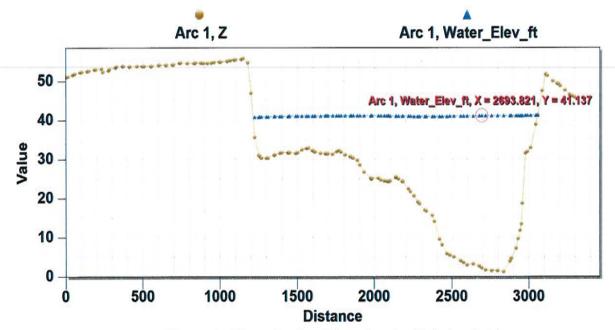


Figure 2- Water Surface Elevation for Existing Bridge

EA 03-3F0700 Project ID: 03-1200-0054

## 4.2 Proposed Variant B and C Condition

	S. CT.	Water	Avg.		∆ Existing to Proposed			
Discharge (cfs)	Soffit Elevation (ft)	Surface Elevation (ft)	Channel Velocity (fps)	Available Freeboard (ft)	Δ Water Surface Elevation (ft)	Δ Avg. Channel Velocity (fps)		
100 -Year Discharge 180,000	43.20 (for ultimate widening)	41.20	6.80	2.0	0.06	-0.06		

The proposed widening will slightly increase the water surface elevation and slightly decrease the velocity for the 100-year discharge. There is adequate freeboard for the 100-year discharge.



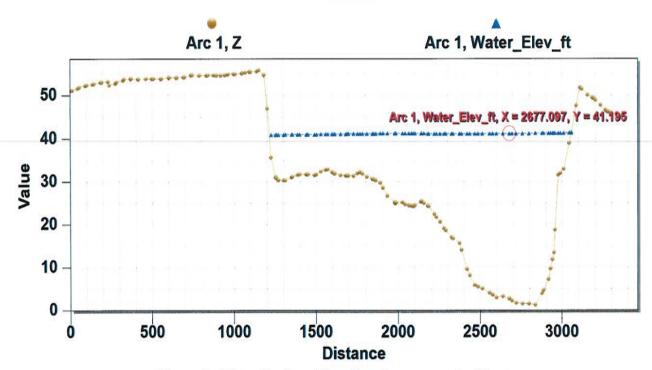


Figure 3- Water Surface Elevation for proposed widening.

Project ID: 03-1200-0054

#### 5.0 Streambed and Scour

#### 5.1 Scour History

According to the Caltrans Bridge Maintenance Records this bridge has a history of degradation, and local pier scour with various levels of footing exposure at Piers 4, 5, 6 and 7 with Pier 4 being the worst.

In June 2002 a detailed scour analysis was completed with the following results:

The channel had degraded 8.11 feet between 1954 and 2002 from a thalweg elevation of 6.74 feet to elevation -1.37 feet. The rate of degradation was 0.17 feet per year with a 20-year potential degradation of 3.4 feet for the remaining life of the bridge.

The local pier scour was calculated to be 9.4 feet for a total scour of 12.8 feet. This initiated a request for a Stability Analysis by the Structure Ratings Branch. According to a memo dated June 11, 2002 from Structure Ratings, the bridge was determined to be stable under the maximum scour and stream flow conditions. However, it was recommended that Pier 4 should be monitored for any further pile exposure.

The Bridge's scour potential was assessed in accordance with FHWA Technical Advisory T5140.23, "Evaluating Scour at Bridges", and within current Caltrans guidelines. The bridge was determined to be not scour critical, and the item 113 code "Vulnerability to scour", was changed to 5, "Bridge Foundations determined to be stable for calculated scour conditions; scour within limits of footing or piles."

An underwater inspection was completed on 07/10/2012. The pile caps at Pier 4 through 7 were exposed from 2.6 to 5.9 feet. The worst exposure was found at the southeast corner of the left column of Pier 4 with 5.9 feet of exposure. It appeared the scour had not changed significantly since 2002 but should be monitored in case it worsened.

The most recent underwater inspection was completed in 9/12/17 with the following results:

The left pile caps at Piers 4 and 5 are undermined to a maximum height of 1.6 feet along the upstream nose. The undermining has exposed (4) steel piles at each pier. The right pile cap at Pier 4 is undermined by 2.6 feet along the upstream nose. Based on the last underwater inspection performed in 2012, the scour remains stable and essentially unchanged.

Project ID: 03-1200-0054

#### 5.2 Current Scour Evaluation

The FHWA Hydraulic Engineering Circular, (HEC-18), "Evaluating Scour at Bridges" was used to calculate the potential scour for the existing bridge. The scour evaluation requires an assessment of (1) Channel Bed Degradation, (2) Contraction Scour and (3) Local Pier Scour including the effects of debris and hydraulic skew.

No contraction scour was noted at this location, and a 20-year potential degradation of 3.4 feet for the remaining life of the bridge was used.

A maximum discharge of 180,000 cfs was used to evaluate the potential local abutment and pier scour for the proposed widening of the structure with the following results:

Bridge Item	Pier Scour	Degradation	Total Scour	Total Scour
	Depth (ft)	Depth (ft)	Depth (ft)	Elev. (ft)
		N. A		
Abutment 1	2.00	3.40	5.40	40.23
Pier 2	3.79	3.40	7.19	22.51
Pier 3	8.58	3.40	11.98	-8.20
Pier 4	9.77	3.40	13.17	-18.14
Pier 5	9.90	3.40	13.30	-18.77
Pier 6	14.49	3.40	17.89	-16.49
Pier 7	8.87	3.40	12.27	-7.67
Pier 8	7.83	3.40	11.23	3.63
Pier 9	7.03	3.40	10.43	10.65
Pier 10	6.89	3.40	10.29	12.07
Pier 11	7.00	3.40	10.40	10.94
Pier 12	6.76	3.40	10.16	11.84
Pier 13	4.03	0.00	4.03	22.97
Pier 14	3.97	0.00	3.97	23.76
Pier 15	3,95	0.00	3.95	23.97
Pier 16	3.94	0.00	3.94	24.15
Pier 17	3.97	0.00	3.97	23.80
Pier 18	3.96	0.00	3.96	23.94
Pier 19	3.98	0.00	3.98	23.66
Pier 20	3.90	0.00	3.90	24.59
Pier 21	3.85	0.00	3.85	23.23
Pier 22	3.84	0.00	3.84	25.34
Pier 23	3.85	0.00	3.85	23.24
Pier 24	3.87	0.00	3.87	22.92

Pier 25	3.24	0.00	3.24	23.78
Abutment 26	2.00	0.00	2.00	46.83

Structure Hydraulics recommends that all new foundations associated with the proposed widening should be designed assuming no ground support (lateral or vertical) as a result of soil loss due to the possible future scour calculated above.

#### 6.0 Drift

There is a moderate potential of drift at the American River Bridge. According to the Bridge Maintenance Records there has been a history of drift including small to medium trees and branches. The existing structure and the proposed widening should have adequate freeboard to pass a moderate amount of drift. Structure Hydraulics recommends the removal of any drift build up on a consistent basis, especially after major storm events.

#### 7.0 Bank Protection

The average velocity has been provided in this report to assist the District Hydraulic Engineers in the design of bank protection if necessary.

### 8.0 Hydrologic and Scour Summary for Design Engineer

· ·	HYDROLOGIC SUI	MMARY <b>Br. No.</b>	24-0003					
Drainage Area: 1875 sqmi								
	Design Flood	Base Flood	Overtopping Flood/Flood of Record					
Frequency	N/A	N/A	N/A					
Discharge	180,0000 cfs	N/A	N/A					
Water Surface Elevation at Bridge	41.25 ft	N/A	N/A					

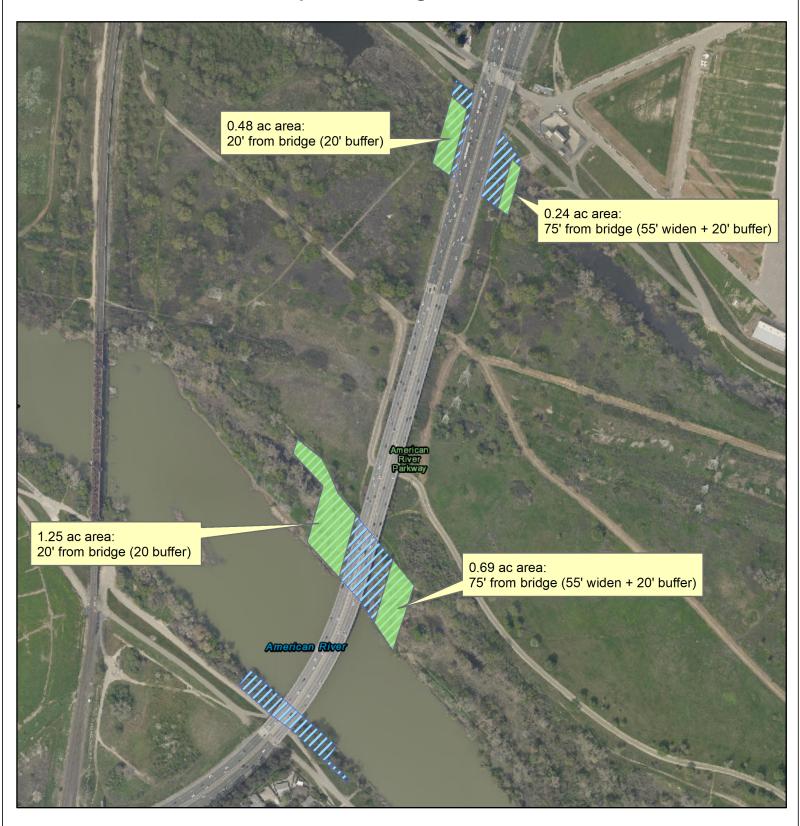
Flood plain data are based upon information available when the plans were prepared and are shown to meet federal requirements. The accuracy of said information is not warranted by the State and interested or affected parties should make their own investigation.

American River Bridge Br. No. 24-0003 03-Sac-51-PM 2.61 EA 03-3F0700 Project ID: 03-1200-0054

## 9.0 Scour Data Table

C	Long Term (Degradation and Contraction)	Short Term (Local)
Support No.	Scour Elevation (ft)	Scour Depth (ft)
		• • • • • • • • • • • • • • • • • • • •
Abutment 1	45.60	2.00
Pier 2	26.30	3.79
Pier 3	0.380	8.58
Pier 4	-8.37	9.77
Pier 5	-8.87	9.90
Pier 6	-2.00	14.49
Pier 7	1.20	8.87
Pier 8	9.52	7.83
Pier 9	17.68	7.03
Pier 10	18.96	6.89
Pier 11	17.94	7.00
Pier 12	18.60	6.76
Pier 13	27.00*	4.03
Pier 14	27.73*	3.97
Pier 15	27.92*	3.95
Pier 16	28.09*	3.94
Pier 17	27.77*	3.97
Pier 18	27.90*	3.96
Pier 19	27.64*	3.98
Pier 20	28.49*	3.90
Pier 21	27.08*	3.85
Pier 22	29.18*	3.84
Pier 23	27.09*	3.85
Pier 24	26.79*	3.87
Pier 25	27.02*	3.24
Abutment 26	45.65*	2.00

<sup>\*</sup>Although there is no anticipated degradation or contraction scour, the existing approximate ground elevation is noted.



## Legend

Planting Areas (2.66 ac)
Const. Impacts (5.21 ac)

Map of Proposed Riparian Planting Areas American River Bridge Project (EA: 03-3F070) SAC-51: PM-2.0-3.5, Sacramento, CA 11/20/20



300 Feet

300 150 0

#### **Riparian Planting Plan Summary**

#### SAC-51 Bridge Project (EA: 03-3F070)

Construction access for the proposed SAC-51 Bridge Deck Replacement Project will result in 5.21 ac of impacts to riparian habitat. Caltrans is required under conditions of the project 1602 permit (California Department of Fish and Wildlife) to mitigate for the loss of riparian vegetation cleared for construction access. Caltrans proposes to plant a 'Great Valley Riparian' planting on-site to compensate for project impacts. The proposed planting consists of native California riparian tree species common to the Central Valley planted at thirty (30) foot spacing. Proposed tree Species include Boxelder (*Acer negundo*), California sycamore (*Plantanus racemosa*), Valley oak (*Quercus lobata*), Fremont cottonwood (*Populus freemontii*), Interior live oak (*Quercus wislizeni*), Oregon white ash (*Fraxinus latifolia*) and Western Redbud (*Cercis occidentalis*). Caltrans has identified a 2.66 ac tree planting area (shown on map) within the temporary impact area.

- Tree planting is to replace existing trees removed for construction access.
- No shrubs will be planted to avoid creating low lying, dense vegetation capable of disrupting water flow.
- Planting proposed in floodplain between levees.
- No planting proposed on levees or within twenty (20) feet of toe of levee slopes.
- No planting proposed under bridges or within twenty (20) feet of bridges.

## Memorandum

Making Conservation a California Way of Life

TO: MR. MADHWESH RAGHAVENDRACHAR

**Branch Chief** 

Bridge Design North and Central, Branch 11

Structure Design

File: 03-SAC-51-PM2.651/2.97

November 27, 2019

Project ID: 0312000054

EA: 03-3F070

Date:

Division of Engineering Services

Attention: Mr. Mark Okimura

AMERICAN RIVER BRIDGE #24-0003
Widen and Deck Rehabilitation

From: DEPARTMENT OF TRANSPORTATION

Division of engineering services

Geotechnical Services

Office of Geotechnical Design - North

Design Branch D

## Subject: PRELIMINARY FOUNDATION REPORT FOR AMERICAN RIVER BRIDGE (WIDEN AND DECK REHABILITATION)

#### **Scope of Work**

The Office of Geotechnical Design North has prepared a Preliminary Foundation Report (PFR) for the proposed American River Bridge (Widen and Deck Rehabilitation). In a request letter dated July 7, 2017, Structure Design, Office of Bridge Design Central, Bridge Design Branch 11 (BDC11) requested a Preliminary Foundation Report (PFR) for the proposed American River Bridge (Widen and Deck Rehabilitation). This PFR supersedes all previously generated Structure Preliminary Geotechnical Reports for this structure. The following recommendations are based on the 1954 and 2019 subsurface investigations performed at the site and the design information provided by BDC11.

With regards to the current foundation recommendations, all elevations referenced within this report and shown on the recent Log of Test Boring sheets are based on the NAVD 1988 vertical datum, unless otherwise noted.

#### **Project Description**

The American River Bridge (Br. No. 24-0003) is located in the city of Sacramento. It was built in 1954 and widen in 1966. The structure consists of 25 spans, steel girder supported on HP 10x42 piles. The proposed project will add one travel lane on each side and a bike lane on the right side of bridge. The bridge widening will

AMERICAN RIVER BRIDGE EA: 03-3F070 Proi. ID: 0312000054

consist of a steel reinforced concrete deck on steel girder supported on seat type abutments.

#### Field Investigation and Field Testing Program

The 1954 As-built LOTBs show the subsurface investigation consisted of three auger borings, one 1-inch closed sampler driven boring and nine 1-inch sampler borings with a minimum 25 feet and maximum depth of 75 feet (Elev. – 44.5 feet).

The 2019 subsurface investigation consisted of 2 auger and 11 mud rotary borings with a maximum explored depth of 201 feet (Elev. -185.8 feet).

#### **Laboratory Testing Program**

The 2019 laboratory testing consisted of corrosion, particle size analysis and Atterberg limits tests. Corrosion test results were available only during the preparation of this PFR.

#### Site Geology and Subsurface Conditions

#### Regional and Local Geology

The project site is located within the Sacramento Valley region of the Great Valley geomorphic province of California. The Great Valley province is an asymmetrical synclinal trough that extends roughly 400 miles north to south and varies up to 50 miles in width separating the Sierra Nevada Mountains on the east from the Coast Range on the west. The surface of the Great Valley is comprised of up to several thousand feet of Quaternary aged, unconsolidated, marine and non-marine alluvial deposited sediments (Geology of California Second Edition, Norris and Webb, 1990).

According to the Geologic Map of the Sacramento Quadrangle, California (C.W. Jennings and D.L. Wagner, 1981), the site is underlain by Quaternary levee and channel deposits (Qa). The levee and channel deposits include the active river and stream channels and their man-made and natural levees as well as adjacent alluvial fans.

AMERICAN RIVER BRIDGE EA: 03-3F070 Proj. ID: 0312000054

#### Subsurface Conditions

The summary of the project subsurface conditions is based on the subsurface investigation which was conducted in 2019. The project site predominately consists of alluvial deposits. These alluvial deposits generally consist of interbedded layers of gravels, sand, silty sand, sandy silts, silts, and clays. Gravels and some cobbles were predominately encountered within the upper layers of the river channel. The granular layers within the alluvial deposits range in densities from very loose to very dense and the fine layers (silts and clays) range from very stiff to hard. The subsurface material generally increases in density as the depth of the boring increases. The total depth of the deepest boring (RW-19-028) was 216.5 feet below the roadway/bridge surface or elevation -152.8 feet. Bedrock was not encountered in any of the borings. For a more in depth descriptions of the subsurface materials encountered, please see the LOTB sheets (will be sent once finalized) RW-19-026 through RW-19-038 that were completed for this report.

#### **Groundwater**

The existing bridge structure spans American River. During the 2019 subsurface investigation, the stream surface water was at about Elevation 10.0 feet. During the drilling operations, groundwater was first encountered from elevation 9.0 to 13.0 feet. No final groundwater readings were conducted at the end of the drilling operations.

Structure Hydraulics has provided a Draft Final Hydraulic Report dated September 18, 2018. The report presents design groundwater estimated at elevation 39.1 feet for the 100-yr event. Groundwater elevations are subject to seasonal fluctuations and may occur higher or lower depending on the conditions and time of construction. For more details, please refer to the LOTB sheets.

#### "AS-BUILT" FOUNDATION DATA

The American River Bridge is supported on driven steel H-Piles 10x42. Geotechnical Services conducted pile resistance analysis taking into account the design scour presented in the Draft Final Hydraulics Report. The As-built foundation data information and estimated pile resistances are presented below in Table 1.

AMERICAN RIVER BRIDGE EA: 03-3F070 Proj. ID: 0312000054

Table 1 – "As-Built" Foundation Information

Table	Cutoff	Pile Tip	Nominal
Support #	Elevation <sup>1</sup>	Elevation <sup>1</sup>	Resistance
' '	(feet)	(feet)	Kips
1	40.25	-30.00	180
2	24.00	-28.00	180
3	-5.00	-27.00*	95
4	-5.00	-27.00*	85
5	-5.00	-27.00*	85
6	-5.00	-27.00*	90
7	-5.00	-27.00*	95
8	-5.00	-27.00*	95
9	10.00	-27.00*	150
10	10.00	-27.00*	170
11	10.00	-27.00*	130
12	10.00	-27.00	130
13	20.00	-27.00	180
14	20.00	-25.00	180
15	20.00	-26.00	180
16	20.00	-26.00	180
17	20.00	-23.00	180
18	20.00	-18.00	150
19	20.00	-17.00	150
20	20.00	-19.00	150
21	20.00	-19.00	150
22	20.00	-19.00	150
23	20.00	-18.00	150
24	20.00	-19.00	150
25	20.00	-17.00	150
26	46.00	-17.00	180

Note: 1 NGVD 1929 Datum. \* Assumed Elevation.

#### **Scour Potential**

The Draft Final Hydraulic Report stated that American River Bridge has a potential for local scour. The scour data presented in the Hydraulics report is shown in Table 2 below.

AMERICAN RIVER BRIDGE EA: 03-3F070 Proj. ID: 0312000054

Table 2 – Scour Data American River

Idbi	Long Term Scour	Short Term
Support #	Elevation (ft)	Scour
зоррон и	Degradation and Contraction	(Local) Depth (ft)
1	45.60	2.00
2	26.30	3.79
3	0.38	8.58
4	-8.37	9.77
5	-8.87	9.90
6	-2.00	14.49
7	1.20	8.87
8	9.52	7.83
9	17.68	7.03
10	18.96	6.89
11	17.94	7.00
12	18.60	6.76
13	27.00	4.03
14	27.73	3.97
15	27.92	3.95
16	28.09	3.94
17	27.77	3.97
18	27.90	3.96
19	27.64	3.98
20	28.49	3.90
21	27.08	3.85
22	29.18	3.84
23	27.09	3.85
24	26.79	3.87
25	27.02	3.24
26	45.65	2.00

Please refer to the draft final hydraulics report for more specific information.

AMERICAN RIVER BRIDGE EA: 03-3F070 Proj. ID: 0312000054

#### Corrosion

Corrosion test results are shown below in Table 3. The tested soil samples were taken from various soil borings. Test results indicate the soil sample is considered **non-corrosive** by current Caltrans standards. See Appendix I for more detail information.

Table 3 – Corrosion Test Summary

Location	SIC Number	рН	Minimum Resistivity (Ohm-cm)	Sulfate Content (ppm)	Chloride Content (ppm)
Water	CR20190498	5.98	30326	4	4
RW-19-026 85' -120'	CR20190493	7.26	1781	N/A	N/A
RW-19-029 35' - 60'	CR20190494	6.99	4196	N/A	N/A
RW-19-031 45' - 100'	CR20190495	7.03	4083	N/A	N/A
RW-19-034 0' - 30'	CR20190496	7.68	5655	N/A	N/A
RW-19-034 30' - 80'	CR20190497	7.15	5296	N/A	N/A

Note: Caltrans currently defines a corrosive environment as an area where the soil has either a chloride concentration of 500 ppm or greater, a sulfate concentration of 1500 ppm or greater, or has a pH of 5.5 or less. With the exception of MSE walls, soil and water are not tested for chlorides and sulfates if the minimum resistivity is greater than 1,100 ohm-cm.

### Preliminary Seismic Design Information and Recommendations

The bridge site may be subject to strong ground motions from nearby earthquake sources during the design life of the bridge. Based on available subsurface information and Standard Penetration Test correlations for determining shear wave velocity, the average shear wave velocity (V<sub>530</sub>) for the upper 100 feet of soil is estimated to be 853 feet/sec (260 m/s). Per the Caltrans Seismic Design Criteria (SDC V.2.0), "Soil Profile Classification", the site should be classified "Class S2 Soil".

AMERICAN RIVER BRIDGE EA: 03-3F070 Proi. ID: 0312000054

The Design Response Spectrum was determined using the Caltrans ARS Online web tool V3.0. The Design Spectrum is the upper envelope of the probabilistic response spectrum, but not less than the Minimum Spectrum for California. The Design Response Spectrum is based on the probabilistic approach. Adjustments for site conditions and near fault effects were implemented when applicable. See Appendix II for more detail information.

Using the USGS Unified Hazard Tool (Dynamic: Conterminous U.S. 2014, V4.2.0), with a shear wave velocity of 260 m/s (closest to calculated site shear wave velocity), the probabilistic fault scenario for the site was determined to have a magnitude (M) of 6.67 (at zero period) and a mean source to site distance (R) of approximately 57.7 miles (at period of 1 second). The peak ground acceleration (PGA) is estimated to be 0.24g.

#### Fault Rupture

The potential for surface fault rupture at the site is low as there are no known faults Holocene or younger in age that fall within 1000 feet of the proposed structure and the proposed structure does not fall within an Alquist-Priolo fault zone. A fault rupture hazard analysis per MTD 20-10 is not required.

#### Liquefaction

Laboratory test results were not available at the time this PFR was prepared. A preliminary liquefaction analysis for the project site was performed according to Youd, et al (2001) Liquefaction Resistance of Soils, using soil properties and groundwater information from the borings and a probabilistic earthquake magnitude and PGA from the USGS Unified Hazard Tool. The amount of seismic settlement due to strong ground shaking does not exist. However, localized liquefaction was encountered on soil borings RW-19-033 and RW-19-034 near Bents 23 and 24. The preliminary analysis showed from 2 to 3 inches of seismic induced settlement. Final Seismic Design Recommendations will include an evaluation of the liquefaction potential at the site.

### <u>Lateral Spreading Evaluation</u>

Based on the preliminary liquefaction analysis, a lateral spreading analysis is not needed. Final seismic design recommendations will be provided in the final report.

AMERICAN RIVER BRIDGE EA: 03-3F070 Proj. ID: 0312000054

#### **Foundation Recommendations**

The following recommendations are for the proposed bridge widening and deck rehabilitation of the American River Bridge (Br. #24-0003), as shown on the General Plan dated October 20, 2017. The following foundation types may be used as foundation support: Driven Open-End Steel Pipe and CISS Piles are the preferred pile type at all support locations for this site. The preference to pipe piles is the ability to handle relatively high driving stresses, and on the ability to mitigate hard driving resistance (prior to reaching the specified pile tip elevation). Driven steel "H" piles may be considered as an alternative pile type at all support locations.

CIDH, Driven Concrete and Close-End piles are not feasible for support due to the high groundwater elevation and the very dense gravel layer at shallow elevation.

Class 200 Alternative "W" piles may be used as foundation support for the proposed bridge widening. Tables 4 and 5 present the foundation information provided by the structure designer.

Table 4 – Foundation Design Data – Right Side

Support	Foundation Type Considered	Estimate of Max Factored Compression Load (Kips)
Abut 1	Class 200 H-Pile or Alt. "W"	280 per pile
ADULI	Class 200 H-Hile Of All. W	2200 per Abutment
Bent 2	Class 200 Alternative "W"	280 per pile
Derii Z	Class 200 Allemative W	2000 per Column
Pier 3-11	Class 200 Alternative "W"	280 per pile
FIEL 3-11	Class 200 Allemative W	8200 per Pier
Ponts 10 05	Class 200 Alternative "W"	280 per pile
Bents 12-25	Class 200 Alternative "W"	2000 per Column
Abut 26	Class 200 H-Pile or Alt. "W"	280 per pile
ADUI 26	Ciass 200 n-rile of All. W	2200 per Abutment

Note: Max factored loads are estimated based on Strength Limit State.

AMERICAN RIVER BRIDGE EA: 03-3F070 Proj. ID: 0312000054

Table 5 – Foundation Design Data – Left Side

Support	Foundation Type Considered	Estimate of Max Factored Compression Load (Kips)
Abut 1	Class 200 H-Pile or Alt. "W"	280 per pile
ADULI	Class 200 H-i lie of Ali. W	1600 per Abutment
Bent 2	Class 200 Alternative "W"	280 per pile
beni z	Class 200 Allemanive W	1700 per Column
Pier 3-11	Class 200 Alternative "W"	280 per pile
FIEL 3-11	Class 200 Allemative W	6400 per Pier
Bents 12-25	Class 200 Alternative "W"	280 per pile
Deriis 12-25	Class 200 Allemative W	1700 per Column
Abut 26	Class 200 H-Pile or Alt. "W"	280 per pile
ADUI 26	Ciass 200 n-rile of All. W	1600 per Abutment

Note: Max factored loads are estimated based on Strength Limit State.

#### Abutments, Bents and Piers

At Abutment, Bent and Pier locations Class 200 Alternative "W" piles are recommended for support. The preliminary foundation recommendations are listed in Tables 6 and 7, below.

AMERICAN RIVER BRIDGE EA: 03-3F070 Proj. ID: 0312000054

Table 6 – Foundation Design Recommendations

	Tuble 6 - FOU	ilaalioli D	coigii k														
Support	Pile Type	Finished Grade Elev. (ft)	Cut- off Elev <sup>1</sup> (ft)	Cap Size (ft)		Cap Size (ft)		Size (ft)		Cap Size (ft)		Cap Size (ft)		Cap Size (ft)		Permissible Settlement <sup>1</sup> (in)	Number of Piles
1	Class 200 Alt. "W"	*	40.25	*	*	1	*										
2	Class 200 Alt. "W"	*	24.00	*	*	1	*										
3	Class 200 Alt. "W"	*	-5.00	*	*	1	*										
4	Class 200 Alt. "W"	*	-5.00	*	*	1	*										
5	Class 200 Alt. "W"	*	-5.00	*	*	1	*										
6	Class 200 Alt. "W"	*	-5.00	*	*	1	*										
7	Class 200 Alt. "W"	*	-5.00	*	*	1	*										
8	Class 200 Alt. "W"	*	-5.00	*	*	1	*										
9	Class 200 Alt. "W"	*	10.00	*	*	1	*										
10	Class 200 Alt. "W"	*	10.00	*	*	1	*										
11	Class 200 Alt. "W"	*	10.00	*	*	1	*										
12	Class 200 Alt. "W"	*	10.00	*	*	1	*										
13	Class 200 Alt. "W"	*	20.00	*	*	1	*										
14	Class 200 Alt. "W"	*	20.00	*	*	1	*										
15	Class 200 Alt. "W"	*	20.00	*	*	1	*										
16	Class 200 Alt. "W"	*	20.00	*	*	1	*										
17	Class 200 Alt. "W"	*	20.00	*	*	1	*										
18	Class 200 Alt. "W"	*	20.00	*	*	1	*										
19	Class 200 Alt. "W"	*	20.00	*	*	1	*										
20	Class 200 Alt. "W"	*	20.00	*	*	1	*										
21	Class 200 Alt. "W"	*	20.00	*	*	1	*										
22	Class 200 Alt. "W"	*	20.00	*	*	1	*										
23	Class 200 Alt. "W"	*	20.00	*	*	1	*										
24	Class 200 Alt. "W"	*	20.00	*	*	1	*										
25	Class 200 Alt. "W"	*	20.00	*	*	1	*										
26	Class 200 Alt. "W"	*	46.00	*	*	1	*										

Note: \* Unknown information. 1 Assumed.

AMERICAN RIVER BRIDGE EA: 03-3F070 Proj. ID: 0312000054

Table 7 – Preliminary Foundation Design Recommendations

Tuble	2 / – Preliminary Foun	ualion be		luulions
			Nominal Resistance	
Support	TIP IVNA I FIRVI		per pile (Kips)	Preliminary Pile Tip
Location	riie Type		Strength	Elev.
		(ft)	Limit State	(ft)
			Compression	
			$\phi = 0.7$	
Abut 1	Class 200 Alt. "W"	40.25	400	-14.0
Bent 2	Class 200 Alt. "W"	24.00	400	-64.0
Pier 3	Class 200 Alt. "W"	-5.00	400	-58.0
Pier 4	Class 200 Alt. "W"	-5.00	400	-55.0
Pier 5	Class 200 Alt. "W"	-5.00	400	-50.0
Pier 6	Class 200 Alt. "W"	-5.00	400	-40.0
Pier 7	Class 200 Alt. "W"	-5.00	400	-40.0
Pier 8	Class 200 Alt. "W"	-5.00	400	-40.0
Pier 9	Class 200 Alt. "W"	10.00	400	-40.0
Pier 10	Class 200 Alt. "W"	10.00	400	-40.0
Pier 11	Class 200 Alt. "W"	10.00	400	-40.0
Bent 12	Class 200 Alt. "W"	10.00	400	-40.0
Bent 13	Class 200 Alt. "W"	20.00	400	-40.0
Bent 14	Class 200 Alt. "W"	20.00	400	-40.0
Bent 15	Class 200 Alt. "W"	20.00	400	-40.0
Bent 16	Class 200 Alt. "W"	20.00	400	-40.0
Bent 17	Class 200 Alt. "W"	20.00	400	-40.0
Bent 18	Class 200 Alt. "W"	20.00	400	-53.0
Bent 19	Class 200 Alt. "W"	20.00	400	-53.0
Bent 20	Class 200 Alt. "W"	20.00	400	-53.0
Bent 21	Class 200 Alt. "W"	20.00	400	-53.0
Bent 22	Class 200 Alt. "W"	20.00	400	-53.0
Bent 23	Class 200 Alt. "W"	20.00	400	-53.0
Bent 24	Class 200 Alt. "W"	20.00	400	-53.0
Bent 25	Class 200 Alt. "W"	20.00	400	-53.0
Abut 26	Class 200 Alt. "W"	46.00	400	-10.0

Note: 1 Estimated cut-off elevation as existing piles.

AMERICAN RIVER BRIDGE EA: 03-3F070 Proj. ID: 0312000054

This Preliminary Foundation Report is based on specific project information regarding structure type and location that have been provided by the Office of Bridge Design Central, Bridge Design Branch 11. Once the project plans are available, the Office of Geotechnical Design North, Design Branch D should review the information to determine if this PFR is still applicable. Any questions regarding the above recommendations should be directed to the attention of Shawn Wei, (916) 227-1079 or Fernando De Haro, (916) 227-1069, at the Office of Geotechnical Design North, Branch D.

Prepared by:

Prepared by:

PROFESS/ONAL ENGINEER

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No.8164

Reviewed by:

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Senior Transportation Engineer
Office of Geotechnical Design-North
Design Branch D

cc: Clark Peri – District 3 (Project Manager)
Steve Culley – District 3 (District Materials Engineer)
Ruth Fernandes – Structures Office Engineer
Geotechnical Archive

Appendix I: Laboratory Test Results

Appendix II: ARS Curve

AMERICAN RIVER BRIDGE EA: 03-3F070 Proj. ID: 0312000054

#### **APPENDIX I**

LABORATORY TEST RESULTS

SAMPLE FROM: SAMPLE FROM SAMPLE FROM: SAMPLE FROM: Results sent to: FERNANDO DE HARO SAMPLE FROM: Dist/Co/Rte/PM: 03 / SAC /051/ / 2.61 PM EFIS: CORROSION CR20190495 CR20190494 CR20190493 CR20190497 CR20190496 CR20190498 EΑ 0312000054 03-3F070 968985D 968985C 968985E 968985F 968985A 968985B TL101# RW-19-034 RW-19-034 RW-19-026 RW-19-031 RW-19-029 CORROSION TEST SUMMARY REPORT SAMPLE OF WATER SOIL SOIL SOIL SOIL SOIL 30 45 35 85 Bridge Name AMERICAN RIVER DEPTH 0 0 Ê Bridge # 120 100 80 30 60 0 RESISTIVITY MINIMUM 30326 24-0003 ohm-cm 5655 1781 5296 4083 4196 7.15 7.68 7.03 6.99 7.26 5.98 PH. Materials Engineering and Testing Services CONTENT<sup>2</sup> CHLORIDE 4 Division of Engineering Services CONTENTS SULFATE Reported by Michael Mifkovic Report Date: 10/18/2019 Corrosion Branch IS SAMPLE S 8 NO S NO S

This site is not corrosive to foundation elements (see note below).

chloride concentration is 500 ppm or greater, sulfate concentration is 1500 ppm or greater. Resistivity is not considered for Structural Elements. MSE backfill shall conform to the requirements of section 47-2.02C Structure Backfill in the 2015 Standard Specifications. Note: For Structural Elements, the Department considers a site corrosive if one or more of the following conditions exist: pH is 5.5 or less,

1CT 643, 2CT 422, 3CT 417

CR20190493 - CR20190498

AMERICAN RIVER BRIDGE EA: 03-3F070 Proj. ID: 0312000054

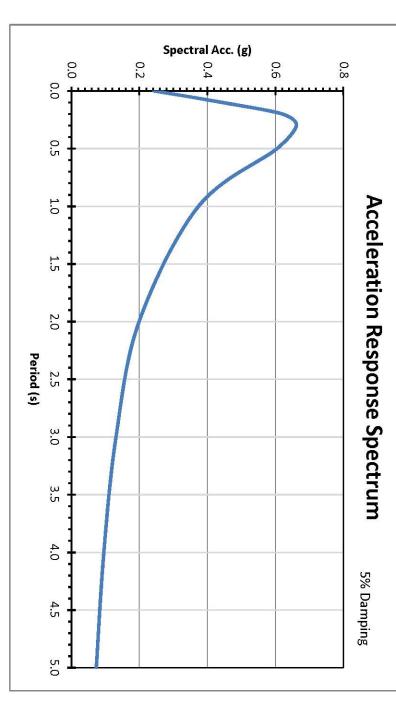
**APPENDIX II** 

**ARS CURVE** 

Period (	Presiding.
$(\mathbf{s})$ Sa $(\mathbf{g})$	1811 7 1181
	l

					5.0	4.0	3.0	2.0	1.0	0.5	0.3	0.2	0.1	0.0	Period (s)
					0.073	0.095	0.131	0.199	0.374	0.605	0.662	0.620	0.443	0.242	<b>Sa</b> (g)





Probabilistic Data (Conterminous - Dynamic Model) with a 975 return period. The Design ARS was developed using the ARS Online Version 3.0 webtool based on the 2014 USGS

Seismic Loading Table (per MTD 1-47, Attachment 1)

Magnitude:  $M_{max} =$ 

0.24 g6.7 Soil Profile  $(V_{s30})$ =

853 ft/s

Proj. ID: 0312000054

EA: 03-3F0700

#### PROJECT DESCRIPTION



The American River Bridge (Widen and Deck Replacement) project proposes to remove and replace the existing concrete deck and steel girder strengthening post-tensioning systems on the American River Bridge (Br # 24-003) and widen the superstructure of the bridge to accommodate traffic during construction. It also proposes to construct the bridge substructure to accommodate the needed deck widening of State Route (SR) 51 and construct new multi-use facility to provide a levee to levee connection for bicyclists and pedestrians between the City of Sacramento bike network to the American River Bike Trail and the adjacent neighborhoods.

#### **PROJECT SCHEDULE**

Project Approval & Environmental Document	January 2021
Design Completed	December 2021
Advertise Project	March 2022
Begin Construction	July 2022
Complete Construction	December 2025

Milestone	Milestone Description	Milestone Date
M000	IDENTIFY NEED	08/05/2011
M010	APPROVE PID	06/29/2015
M015	PROGAM PROJECT	10/22/2015
M020	BEGIN ENVIRONMENTAL	09/01/2016
M040	BEGIN PROJECT	12/10/2015
M060	CIRC DPR & DED INTERNALLY	04/20/2020
M100	APPROVE DPR	10/12/2020
M120	CIRC DPR & DED EXTERNALLY	10/22/2020
M160	APPROVE FED	12/01/2020
M200	PA&ED	12/05/2020
M221	RECEIVE COMPLETE	01/23/2020
M224	R/W REQUESTS	02/27/2020
M225	REGULAR R/W	12/01/2020
M275	GENERAL PLANS	03/27/2020
M300	CIRCULATE PLANS IN DISTRICT	09/01/2021
M311	30% CONST REVIEW	12/01/2020
M313	60% CONST REVIEW	04/01/2021
M315	95% CONST REVIEW	09/17/2021
M377	PS&E TO DOE	12/01/2021
M378	DRAFT STRUCTURES PS&E	09/01/2021
M380	PROJ PS&E	09/01/2021
M410	R/W CERTIFICATION	01/21/2022
M430	DCR	01/14/2022
M460	READY TO LIST	01/28/2022
M470	FUND ALLOCATION	03/24/2022
M480	HQ ADVERTISE	03/07/2022
M490	BIDS OPEN	05/05/2022
M495	AWARD	06/06/2022
M500	APPROVE CONTRACT	07/01/2022
M600	CONTRACT ACCEPTANCE	12/01/2025
M700	FINAL REPORT	12/01/2026
M800	END PROJ	12/01/2027
M900	FINAL PROJ CLOSEOUT	12/01/2028

# **American River Flood Control District Water Forum Stakeholder Participation**

#### **Staff Report**

#### **Discussion:**

The Sacramento Water Forum was established to promote stainable management of the Sacramento Region's water supply and the aquatic habitat of the Lower American River. The Water Forum consists of a diverse group of agencies, businesses, and interest groups that work together to balance the co-equal goals of establishing water supply reliability and preserving the health of the ecosystem.

The Water Forum recently hosted a web meeting to reach out to potential participants in its Public Caucus. The training described the current effort underway for the Water Forum to update its 20-year plan in the form of the Water Forum Agreement and to list the specific task sand expectations of participants in the Public Caucus.

The Water Forum Agreement consists of 7 elements:

- 1. River Flow Standard
- 2. Habitat Management
- 3. Ground Water Management
- 4. Water Conservation
- Increased Surface Water Diversion
- 6. Dry Year Actions
- 7. Water Forum Successor Effort

The goals of the Public Caucus mainly include broadening participation into other areas of our region and community. Some specific areas to focus on include:

- 1. Social Equity and Diversity
- 2. Land Use and User Experience
- 3. Legacy of Stewardship

The group has a goal of updating the Water Forum Agreement over the next year and have the document ready to be ratified in mid-2022. The expectation of members in the Public Caucus would be to engage in monthly meetings and to review and contribute to work products and to present the document to their representative Boards for execution/endorsement.

The American River Flood Control District fits into the mix of participants since we are a steward of the lands adjacent to the American River Parkway. In this capacity the District has an impact on user experience of the Parkway and to a minor degree the habitat of the aquatic ecosystem. The District likely would not be participating in a large role in the development of the Water Forum Agreement but could be present in the discussions to provide information on flood control objectives. Although the Water Forum does not have a Flood Control component, the District could participate to stay connected to the progress of the group.

Water Forum staff indicated the time commitment to participate in the Public Caucus was likely to be between 2 to 6 hours each month at the evening work sessions. The Board may want to identify a Trustee to serve as the representative to the Public Caucus and name the General Manager as an alternate.

#### **Recommendation:**

The General Manager recommends that the District participate as a member of the Public Caucus in the Water Forum.

## General Manager's Meeting Summary February 2021

- **2/10: Water Forum coordination phone call.** I met with Jessica Law, the Executive Director of the Water Forum, via phone call to discuss the Water Forum and its Public Caucus. Ms. Law described the current effort to update the Water Forum Agreement and the ways the District could participate in the Public Caucus.
- 2/12: American River Flood Control District Board of Trustees meeting. The Board met in regular session. The agendized items included an encroachment permit application for a septic system replacement on Claremont Road, the Personnel Committee recommendation for selection of Personnel Legal Counsel, consideration of an effort to de-authorize the McClaren Drive levee segment, and a presentation from the Water Forum.
- **2/17: Sacramento County Local Hazard Mitigation Plan Web meeting.** I attended this meeting via teleconference with representatives from the County of Sacramento and numerous Special Districts to discuss the 2021 update to the Local Hazard Mitigation Plan.
- **2/23: Arcade Creek Seepage Discussion.** I met with staff from SAFCA, the U.S. Army Corps of Engineers, Mead & Hunt, and Kleinfelder to discuss the effort to correct a seepage problem on the Arcade Creek North Levee. The group discussed the seepage that was observed during the high-water events of 2017 and 2019 and steps taken to date to identify the source of the seepage. SAFCA tasked its consulting engineers with developing a strategy for more exploratory potholing and a water test to locate the waterside source of the seepage.
- **2/24: Water Forum 101 Web meeting.** I participated in this web meeting to learn about the Water Forum's mission and current effort to update the Water Forum Agreement. This meeting focused on the Public Caucus and its role in updating the Agreement.
- **2/25: ARFCD Public Outreach Committee meeting.** The Public Outreach Committee met to begin work on the Spring 2021 Newsletter.